



Validation mécanique des codes d'informatique graphique



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CNRS
Sorbonne-Université



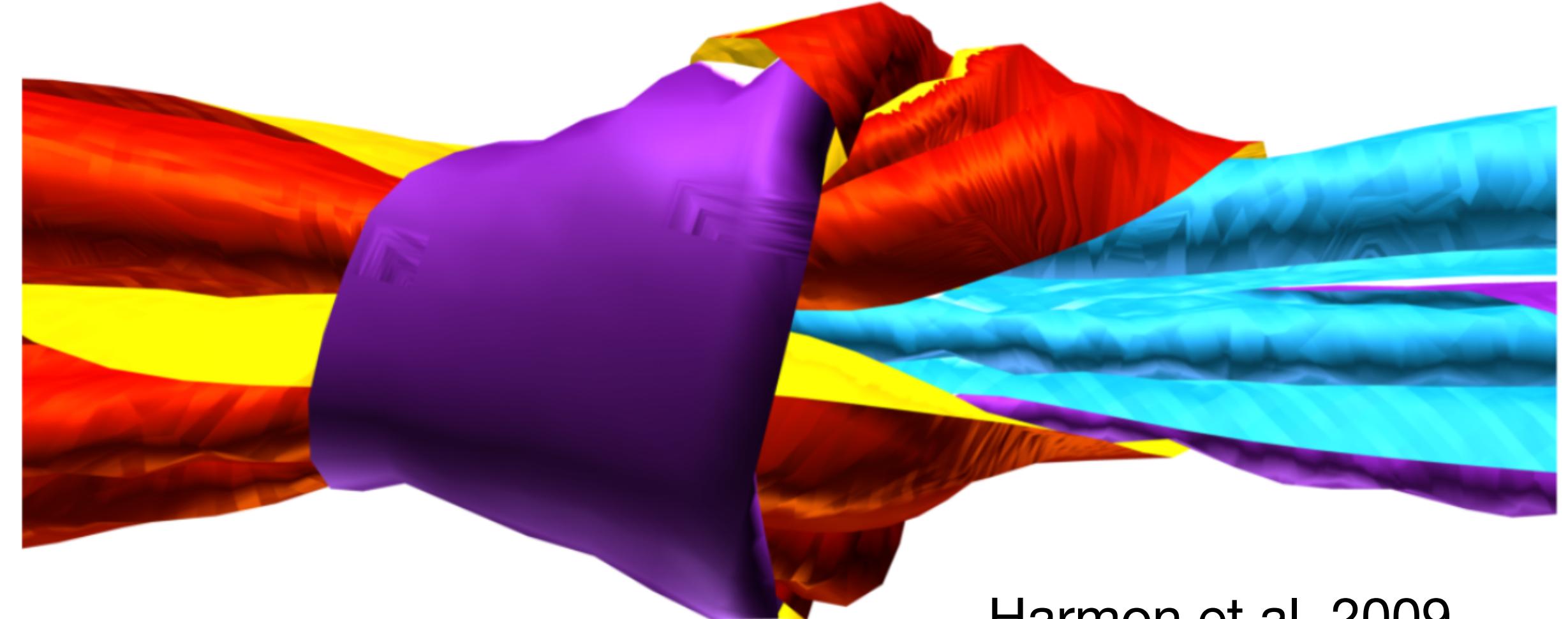
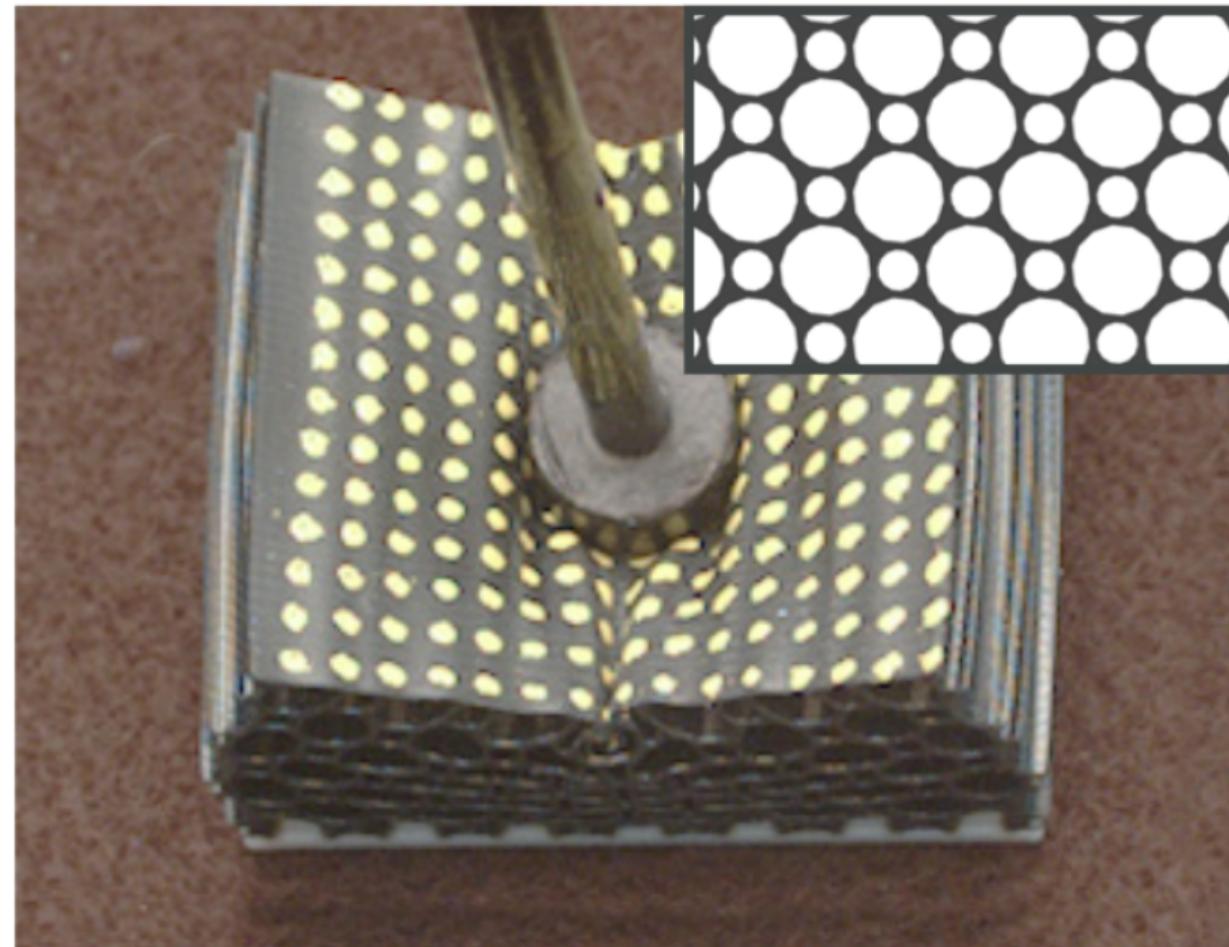
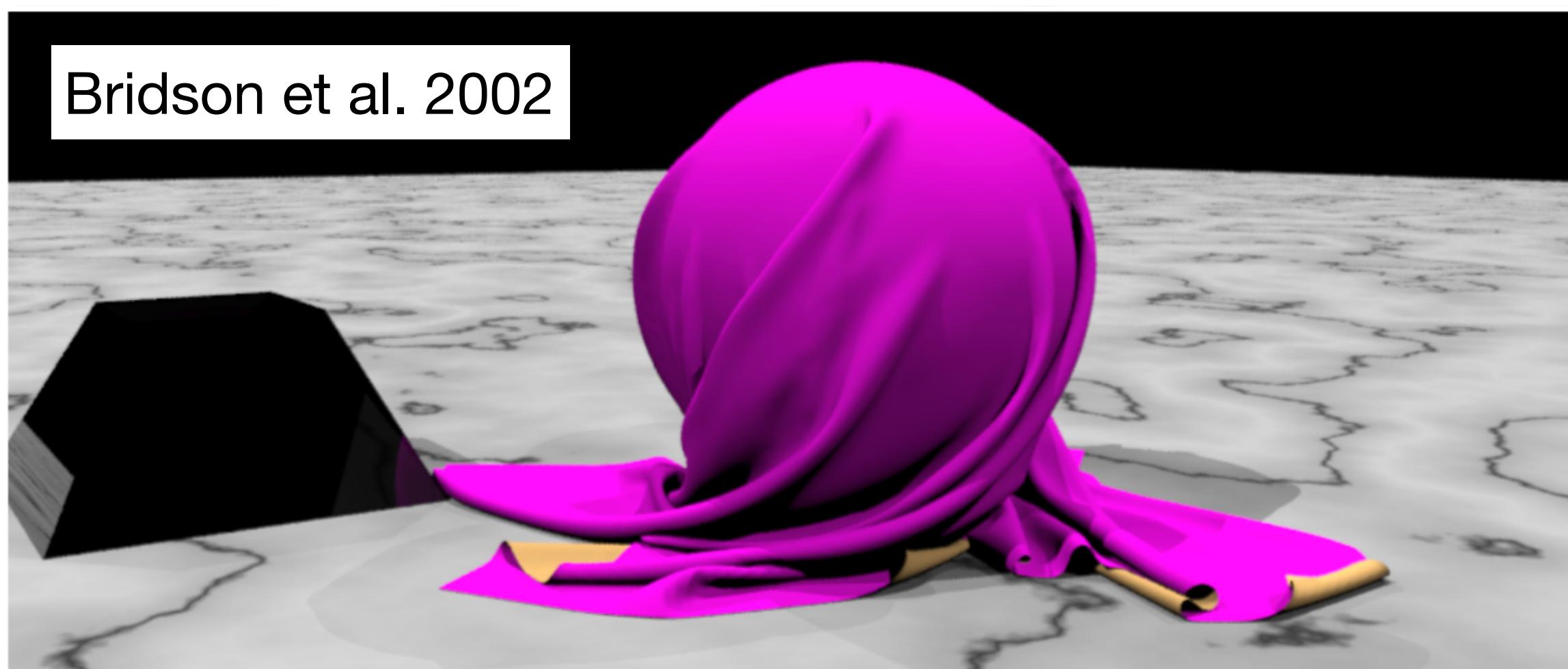
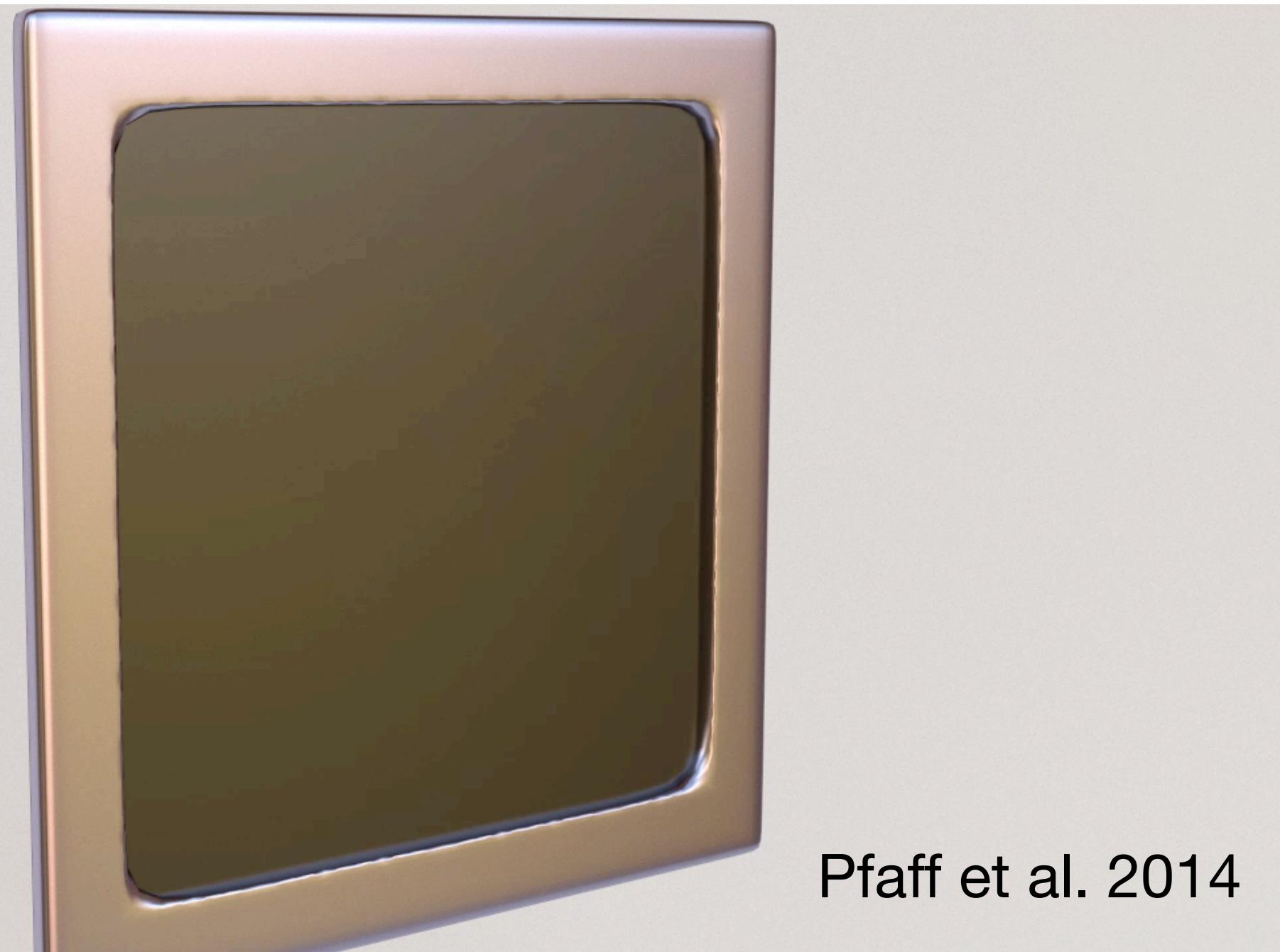
Motivation

Computer Graphics Simulators
are used in the
Animated Video Industry



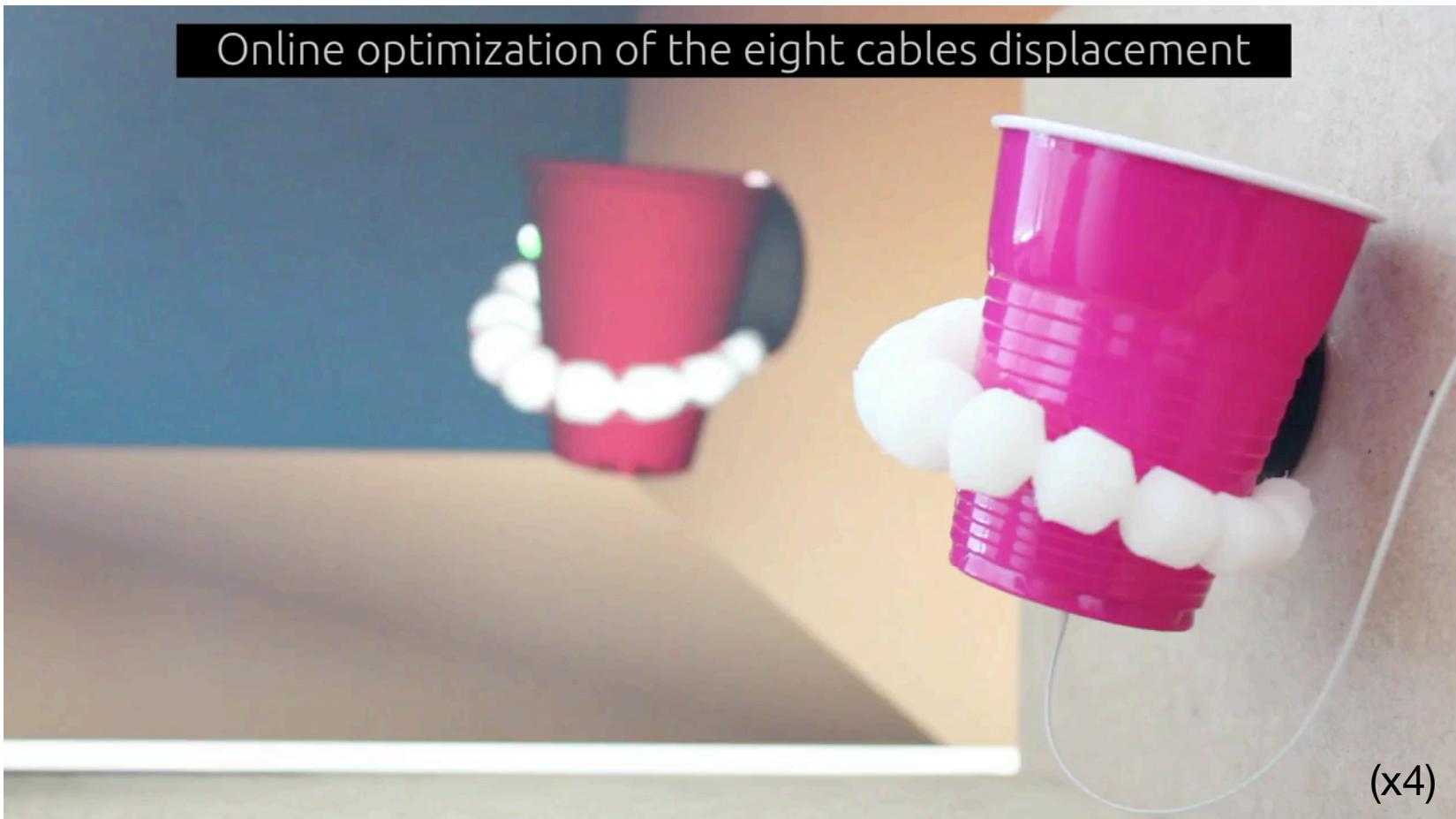
Buffet et al. SIGGRAPH, 2019

Impressive but qualitative scenarios



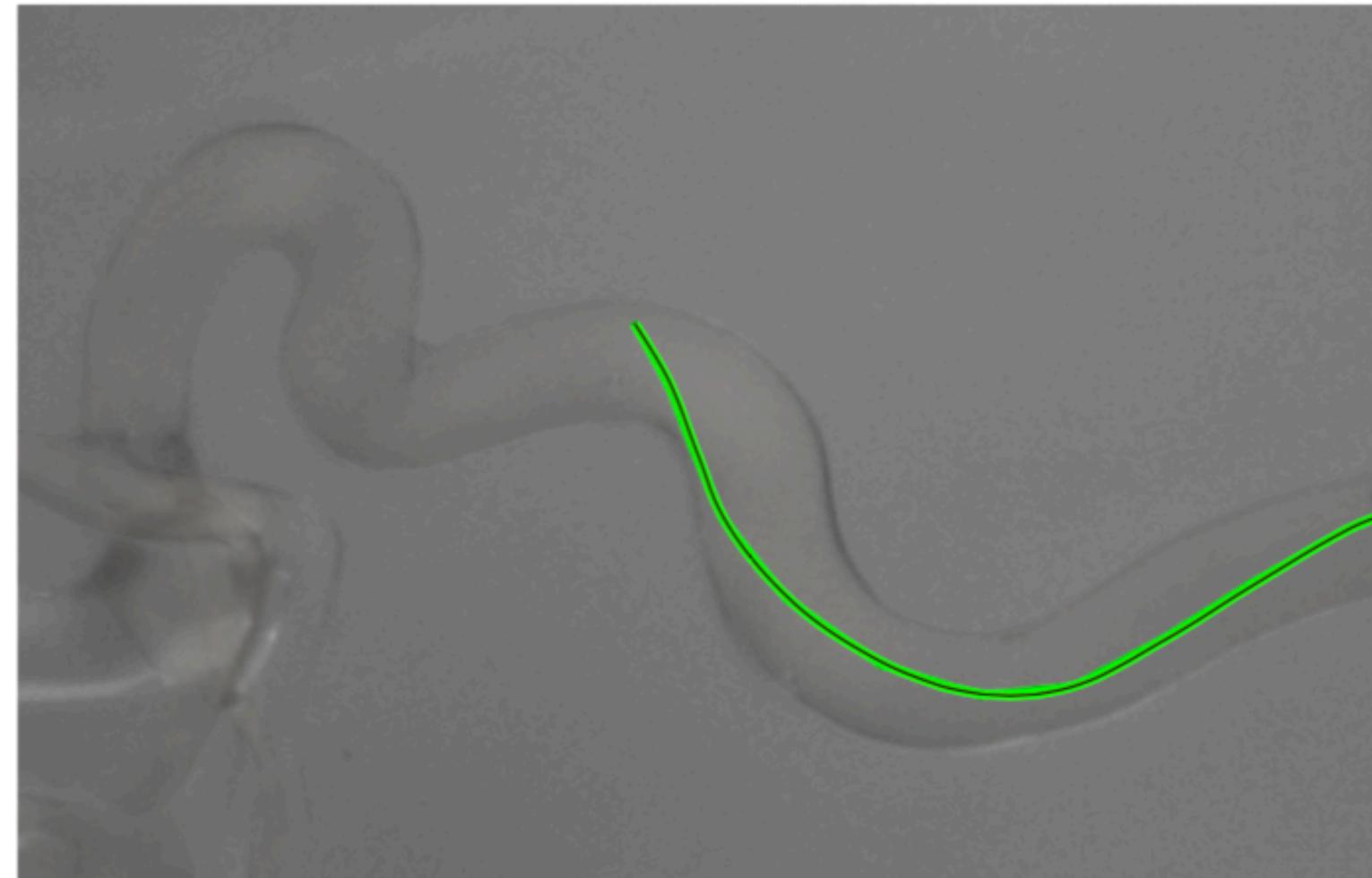
Engineering applications

Soft Robotics

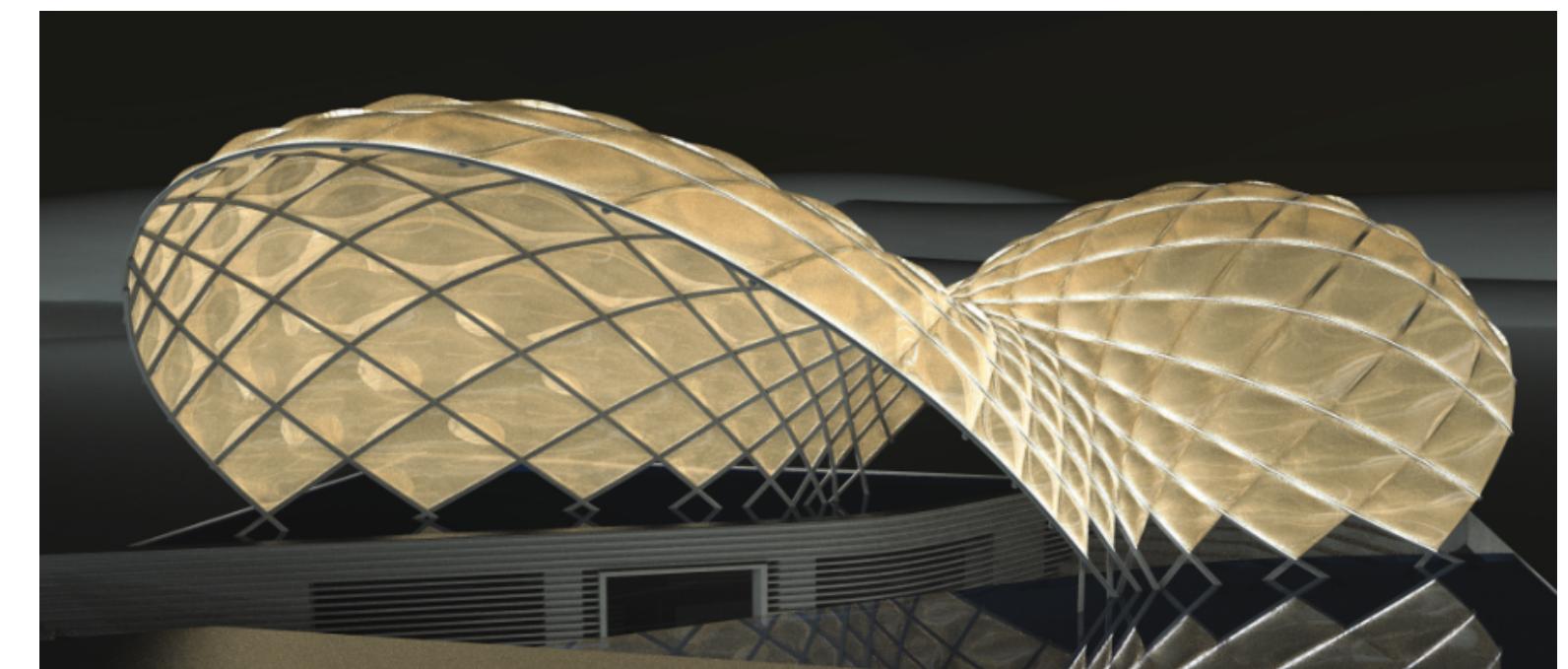
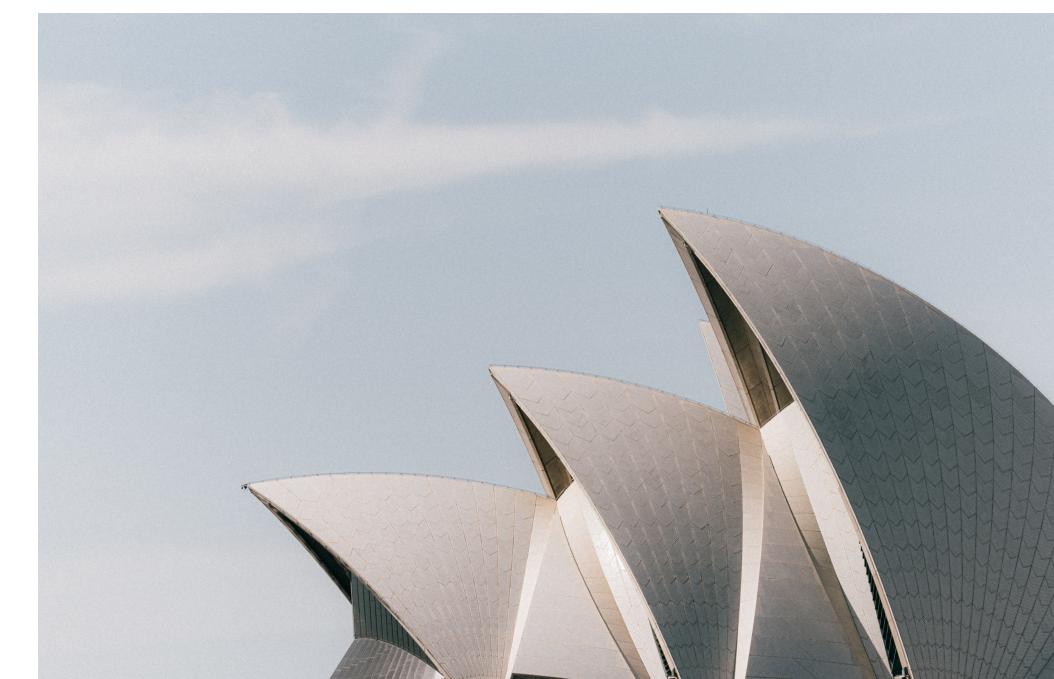


Coevoet et al. Robosoft, 2019

Medicine

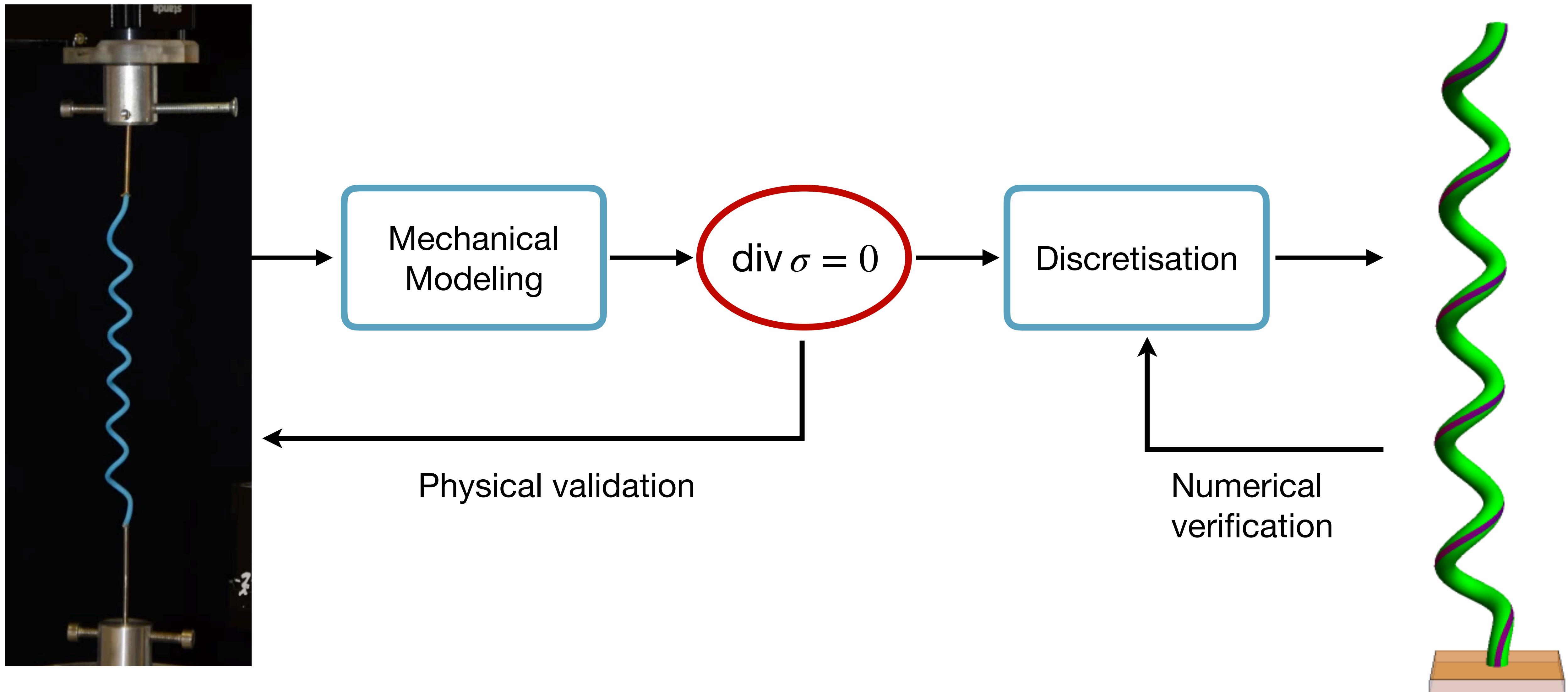


Architecture

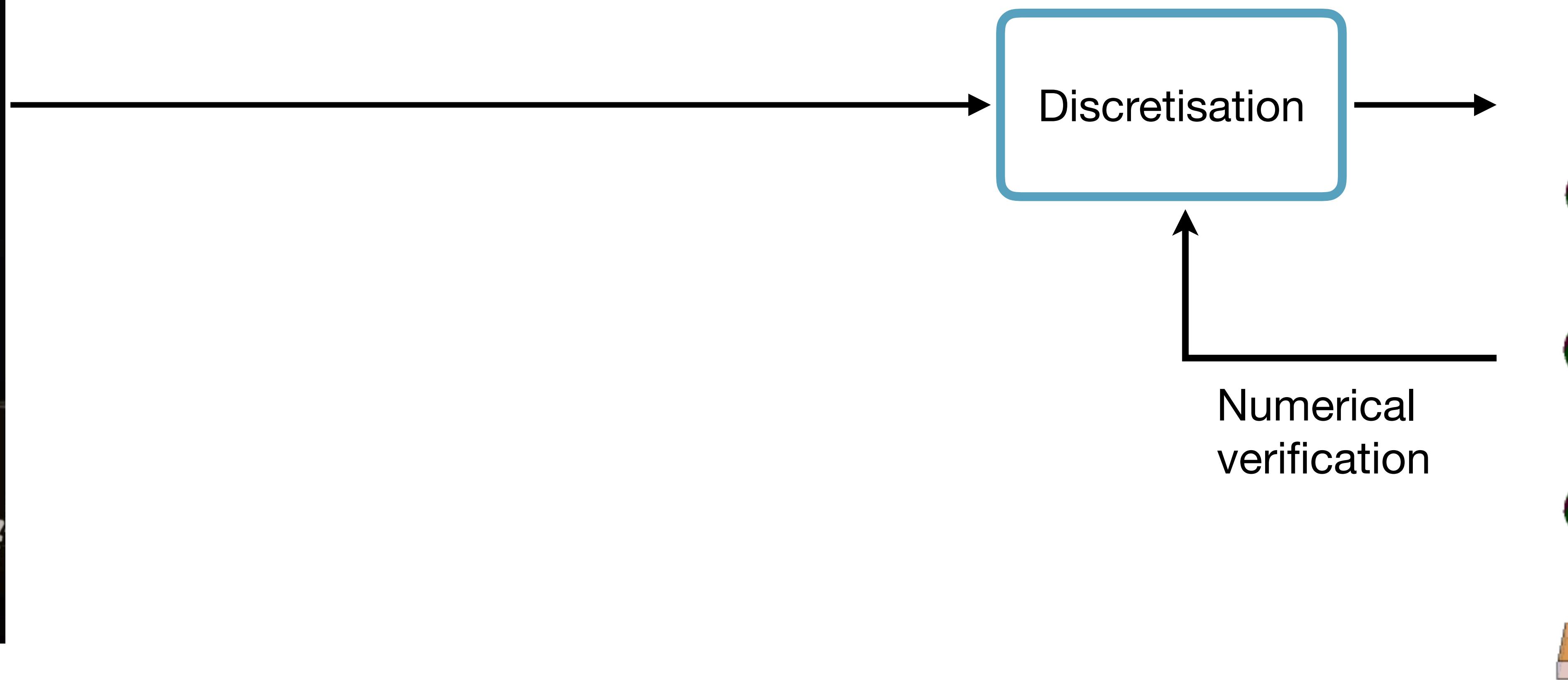
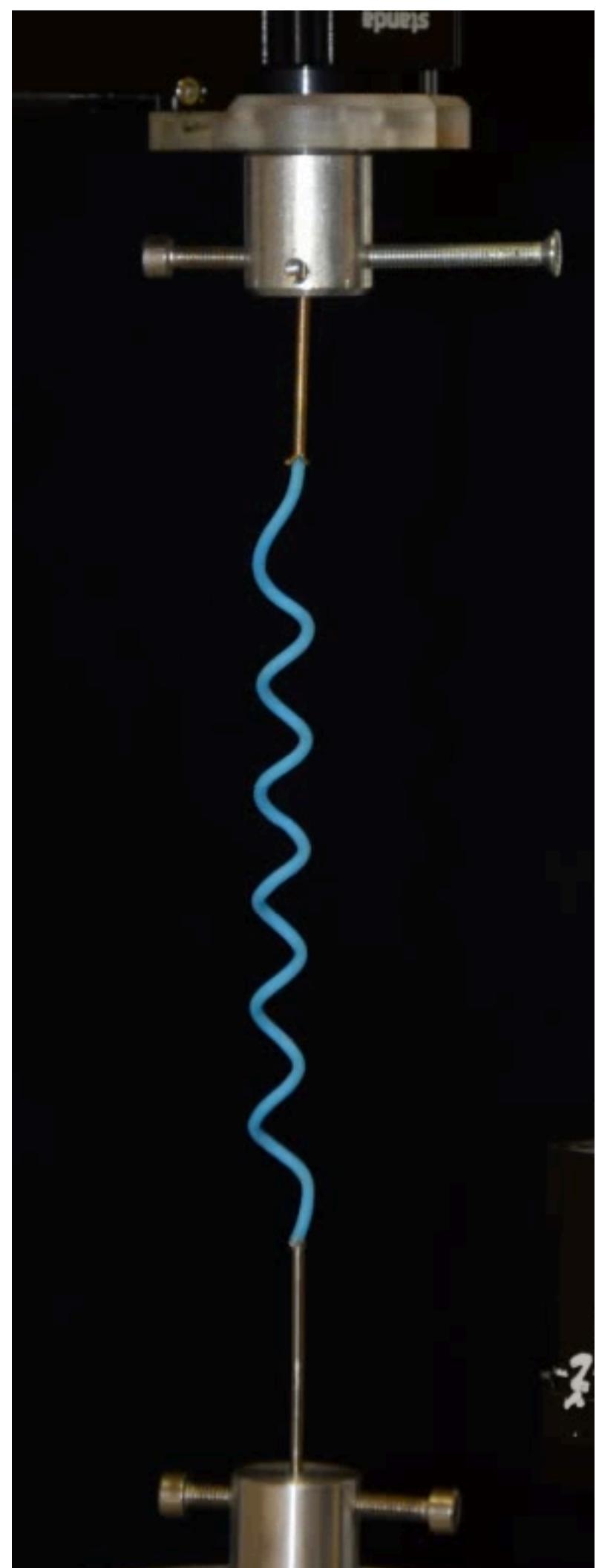


Panetta et al. Siggraph, 2019

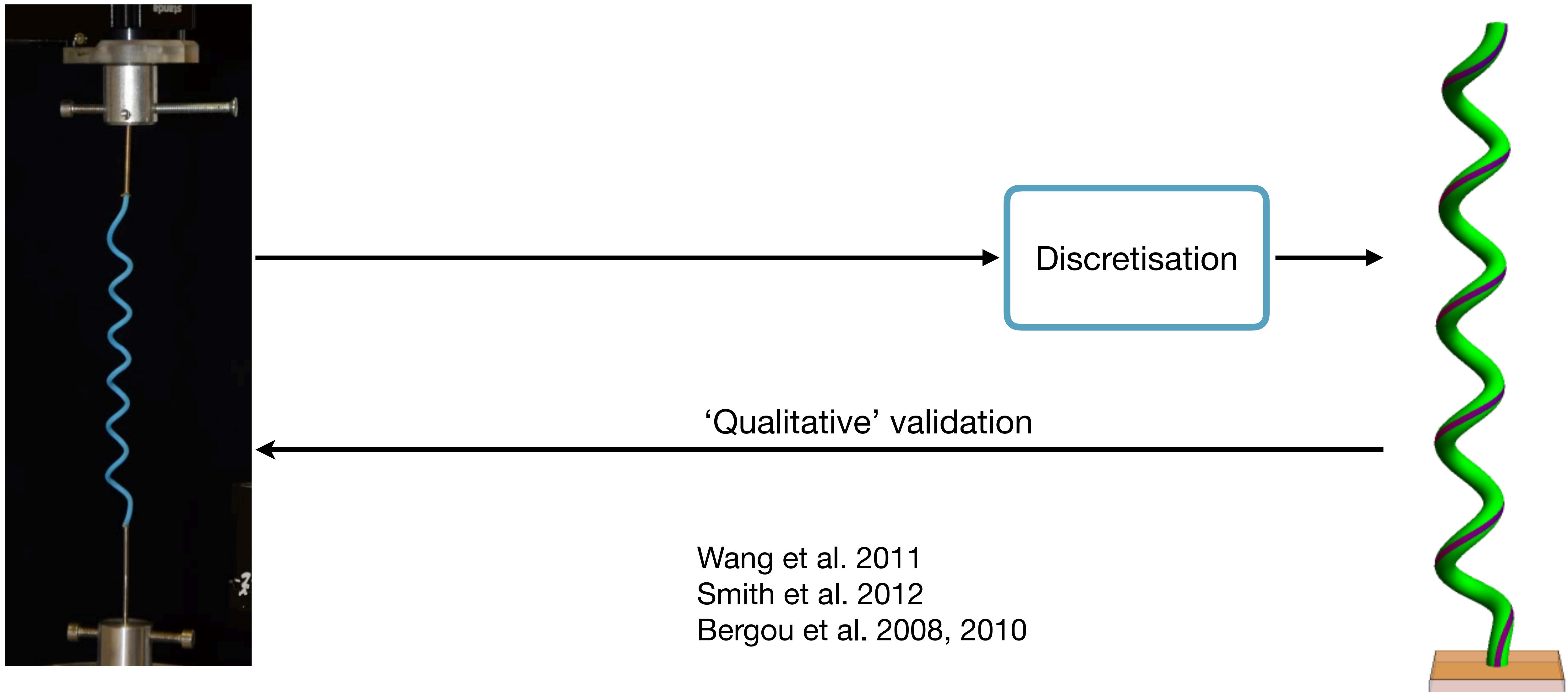
Traditional validation work flow



Work flow in Computer Graphics



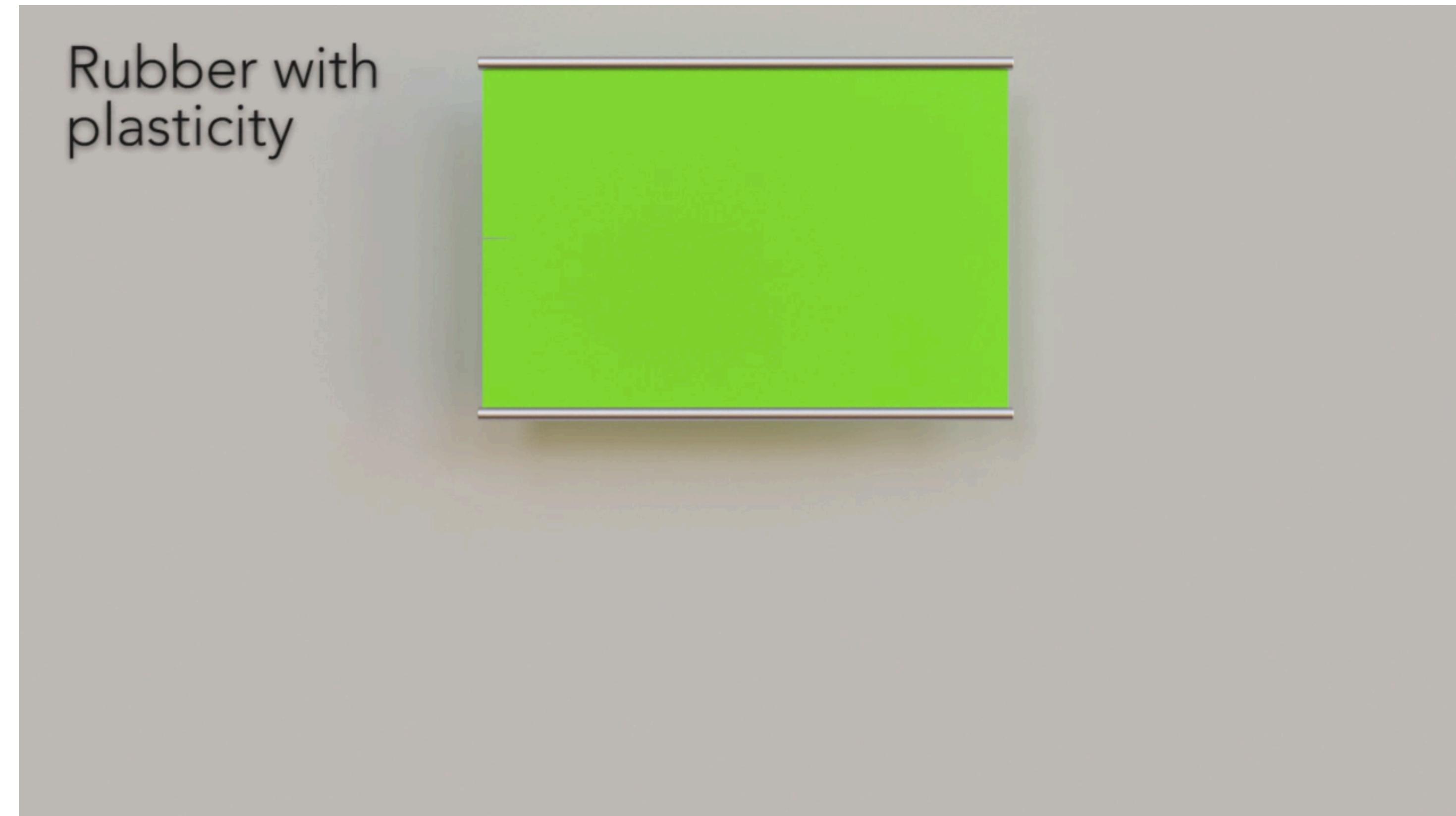
Work flow in Computer Graphics



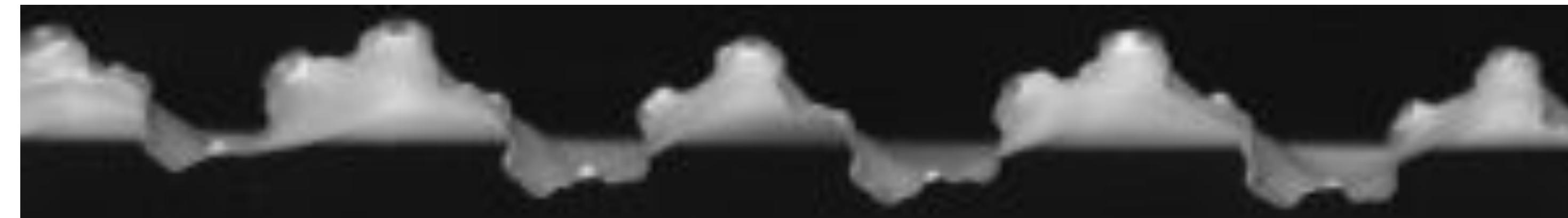
Taking advantage of numerical simulators ... for exploring complex physical systems

Pfaff et al.
ACM Transaction on Graphics
Vol. 33, No. 4 (2014)

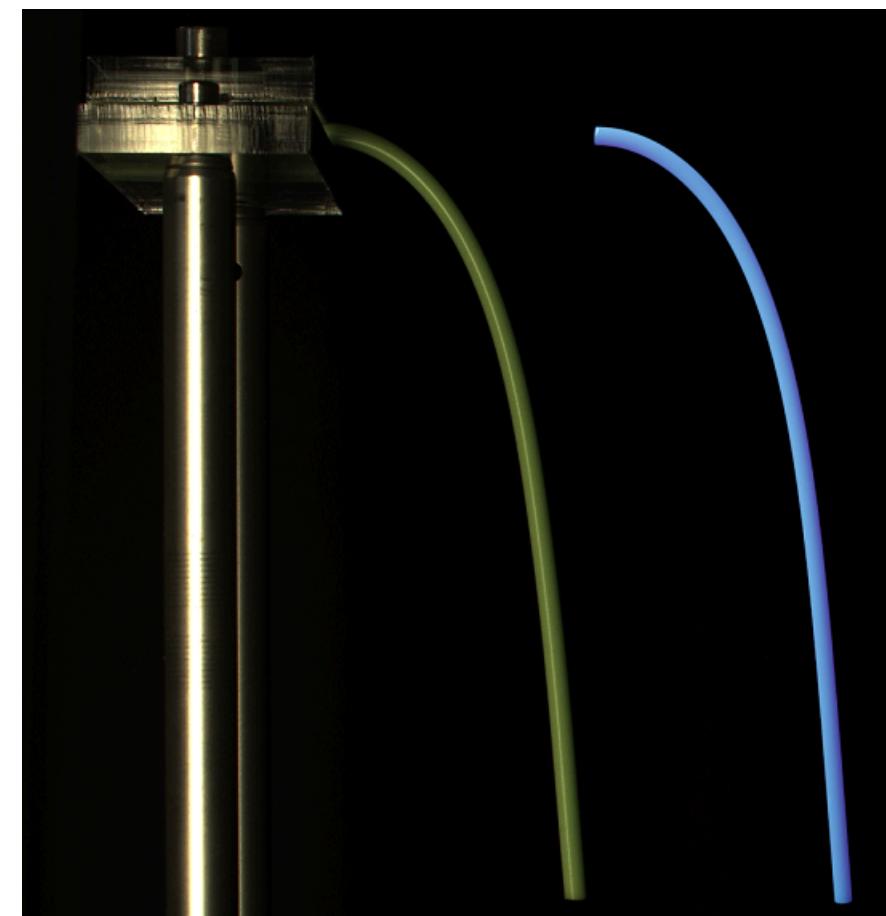
(numerics)



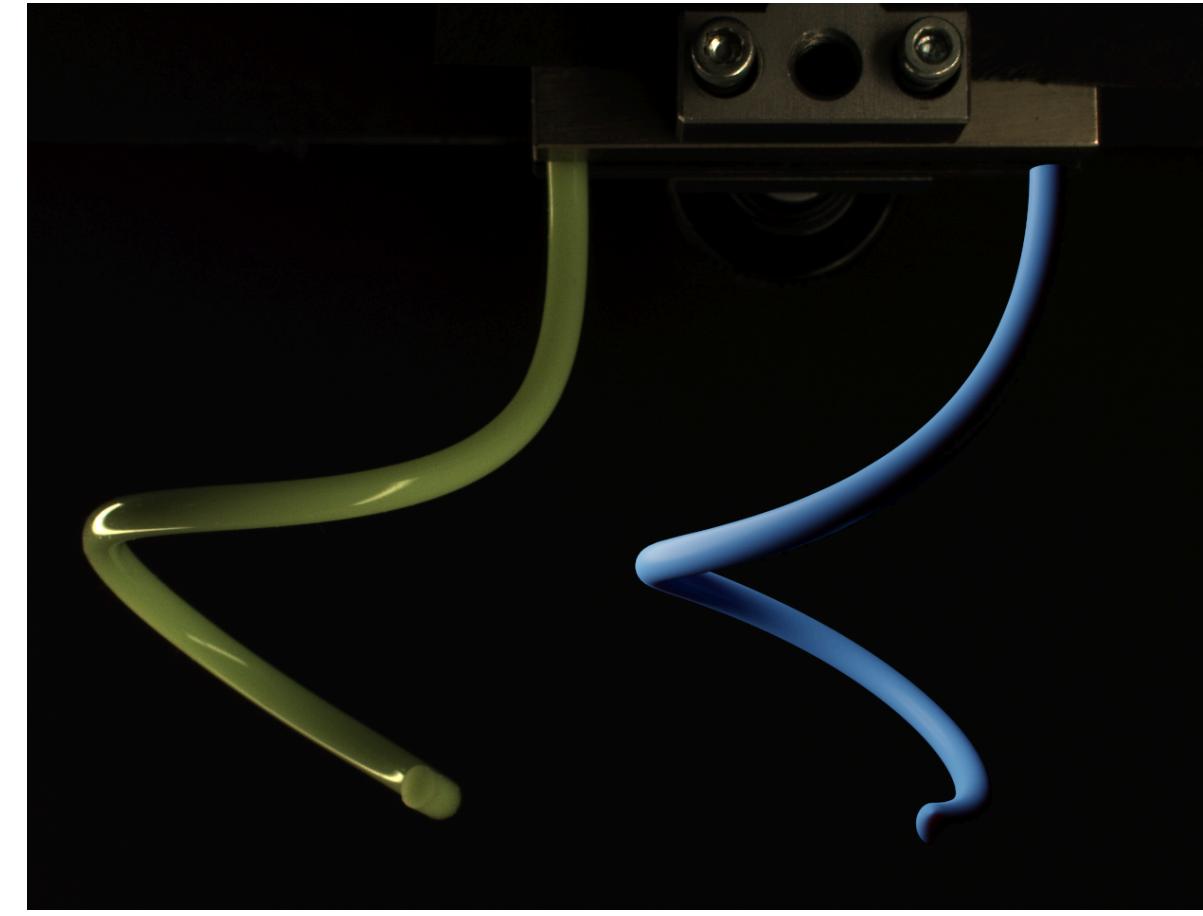
Sharon et al. Nature (2002)
(Physics experiments)



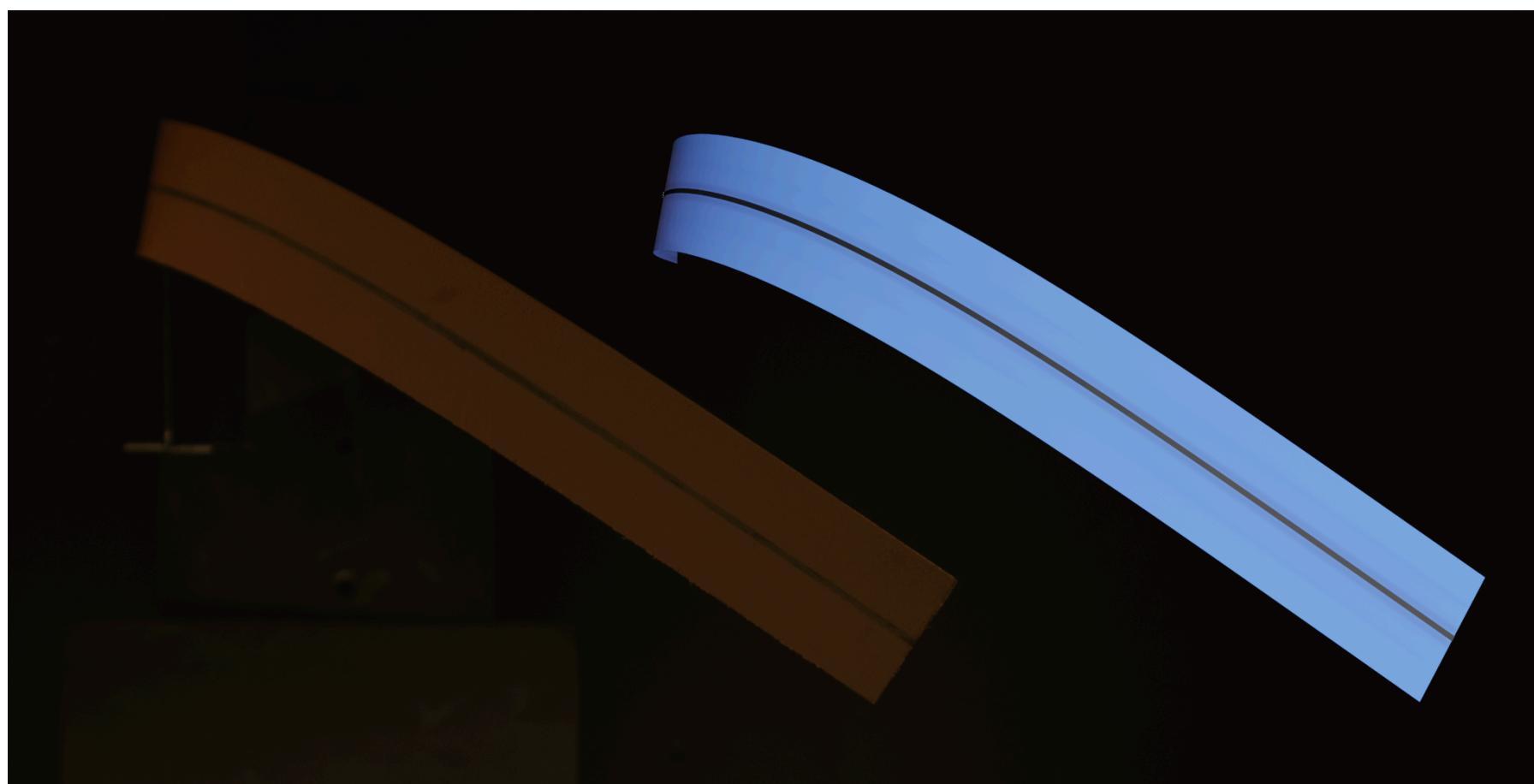
The 4 tests



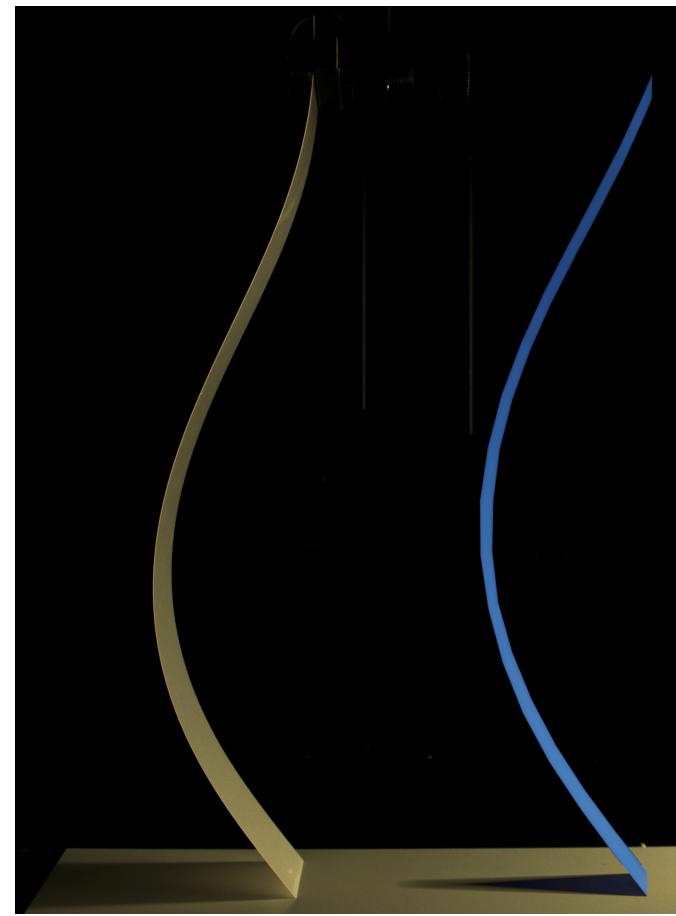
Cantilever



Bend-Twist



Lateral Buckling

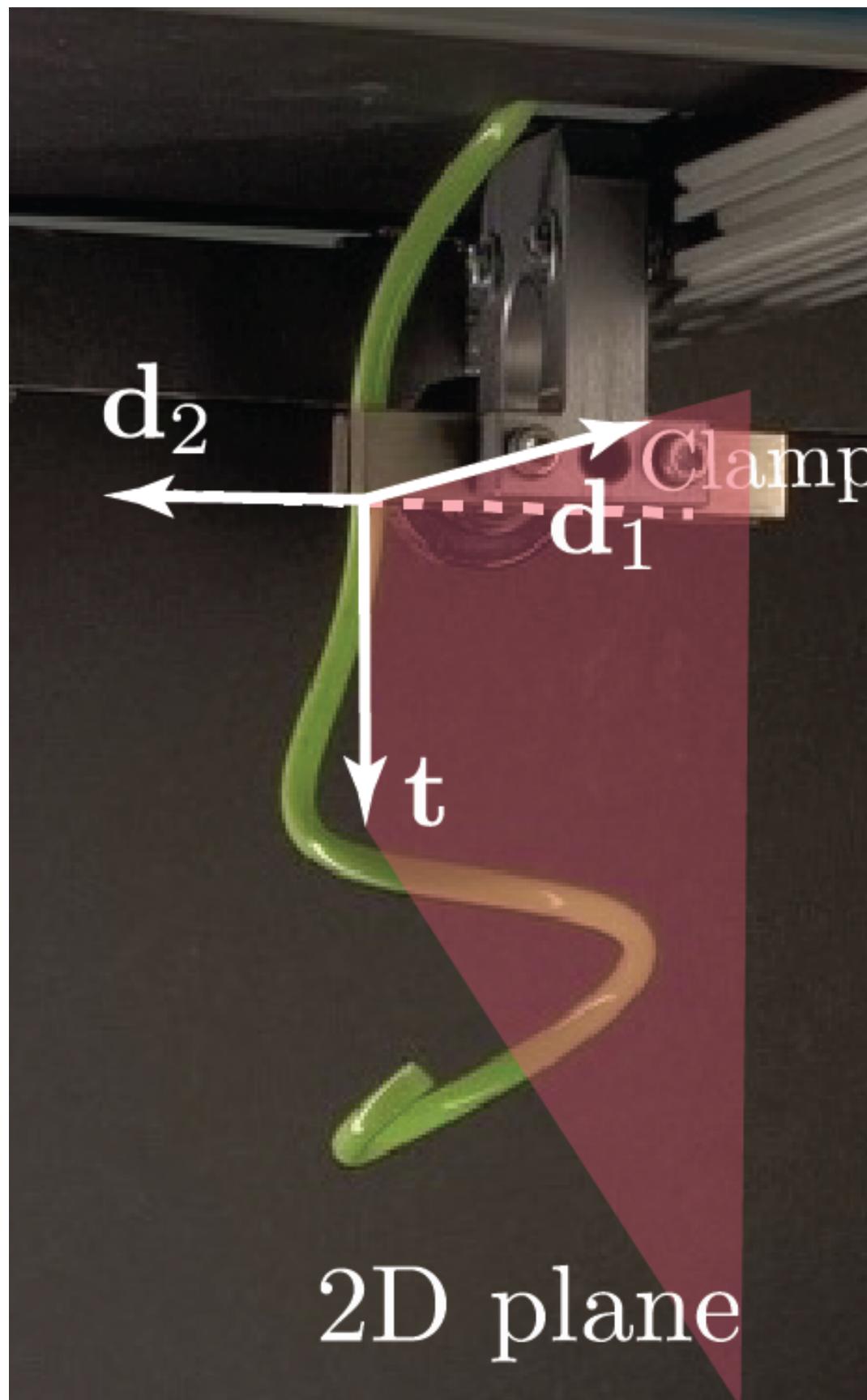


Stick-Slip

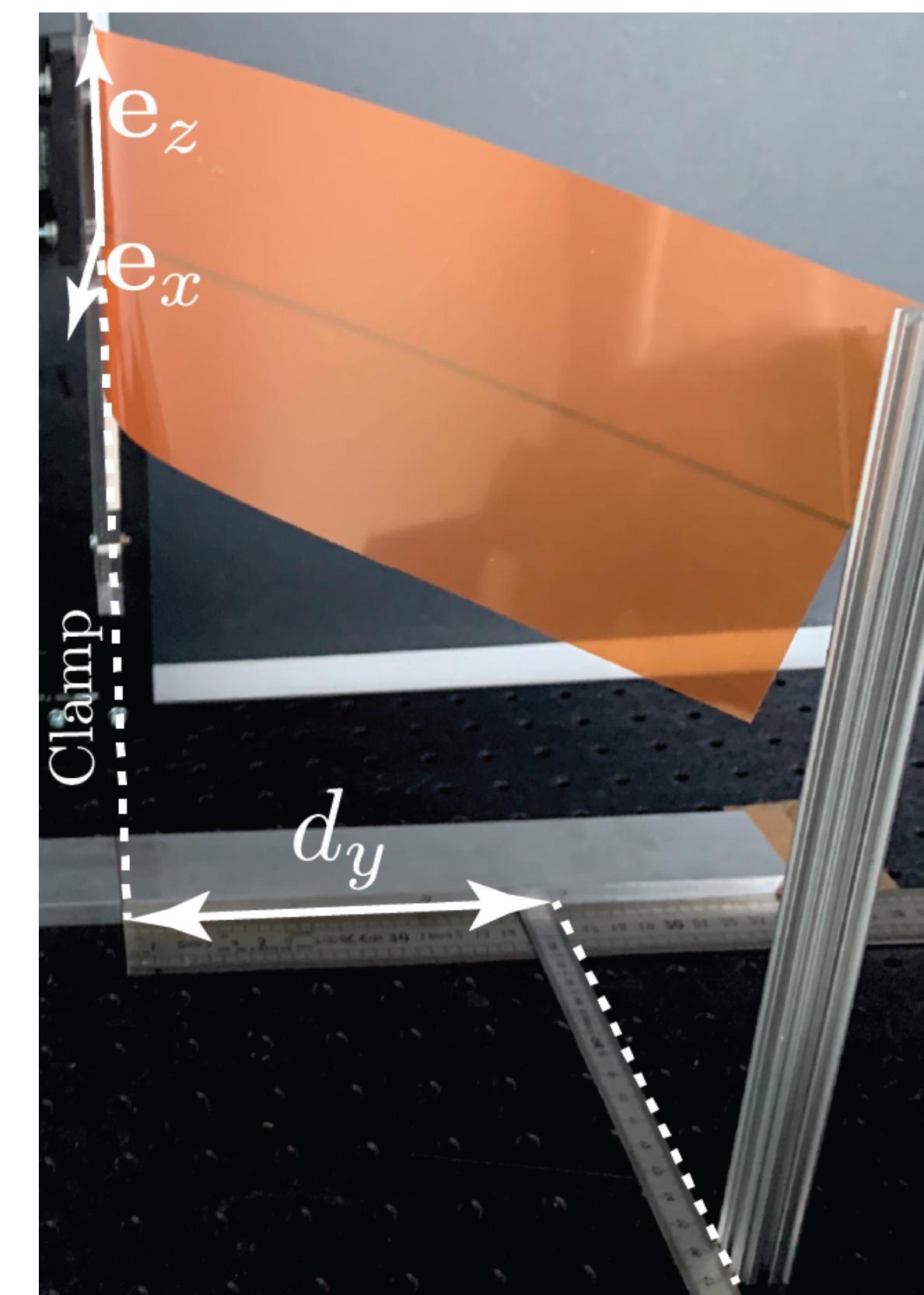
Experimental setups



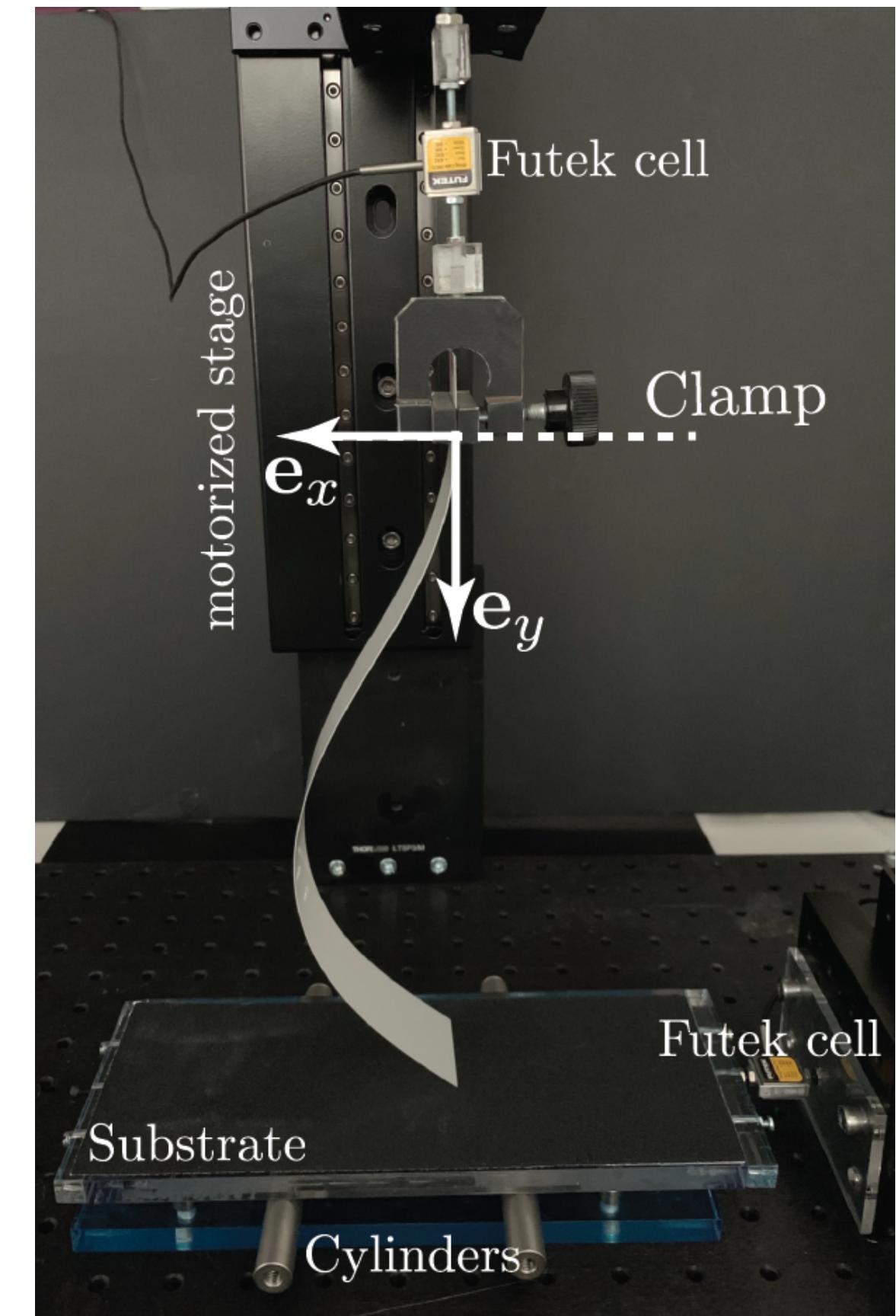
Cantilever



Bend-Twist

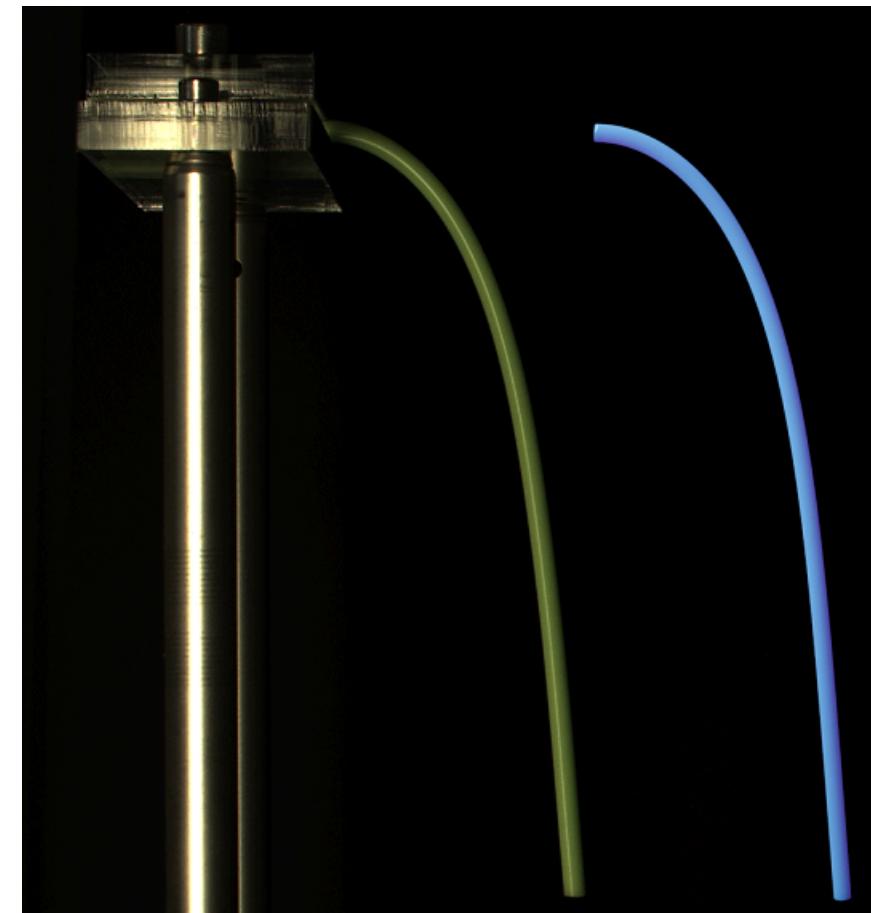


Lateral Buckling



Stick-Slip

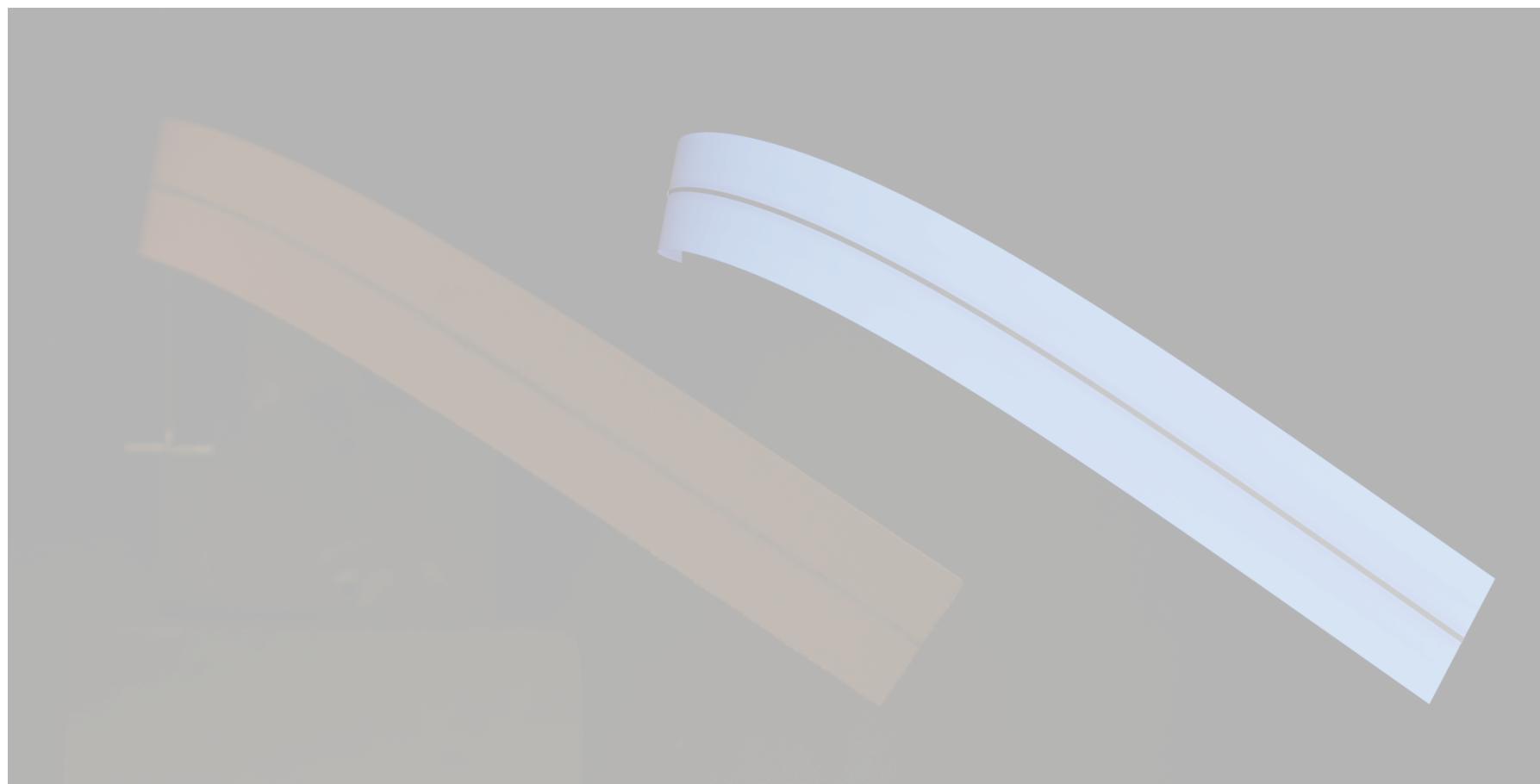
The 4 tests



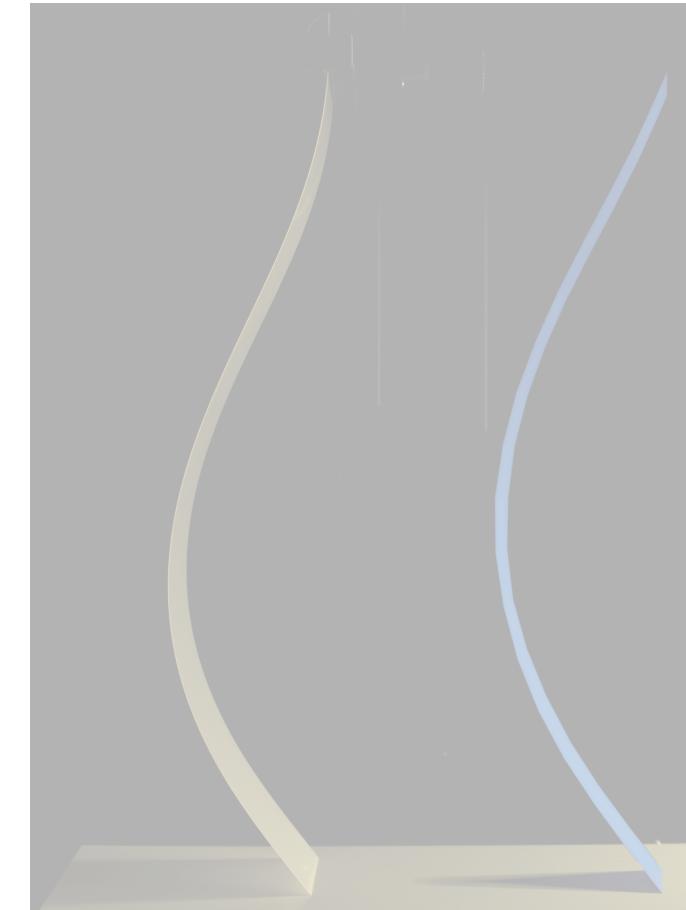
Cantilever



Bend-Twist



Lateral Buckling



Stick-Slip

Cantilever test



Well-known in Engineering and Computer Graphics
(here, finite rotations)

Bending rigidity EI
Length L
Weight Mg

The Magic behind non-dimensionalization

SI Units

here: statics, and
no electric charges

M Kg Sec Amp.

M Kg 2 units, which can be chosen *arbitrarily*

Length Force

Our Units (adim units)

We choose

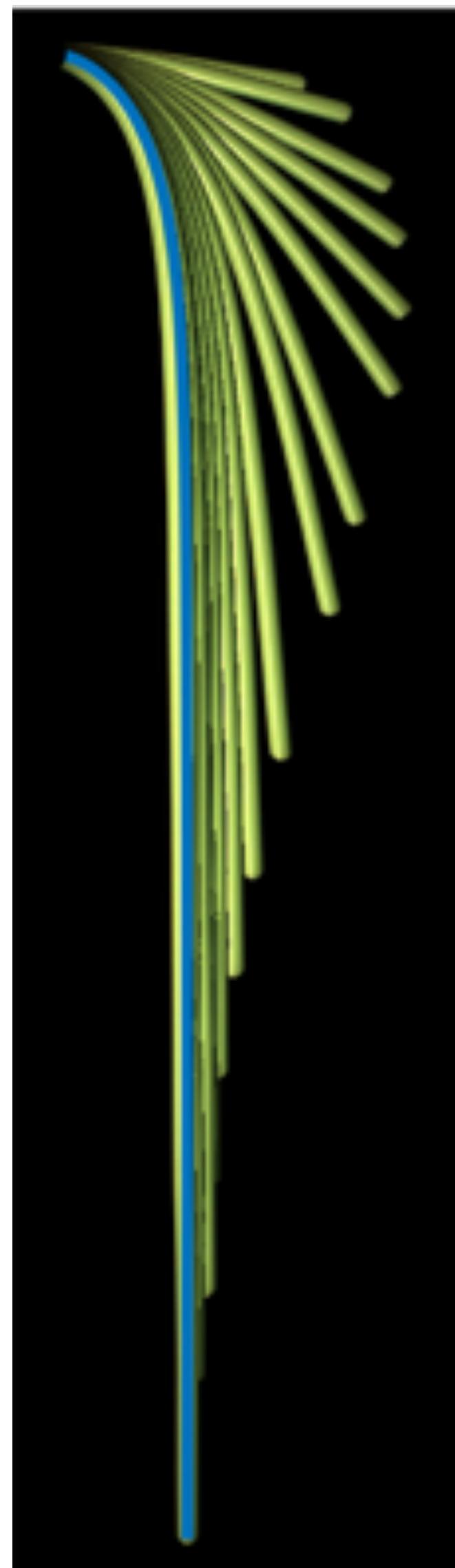
L EI/L²

Equiv. to
formally write

L=1 EI=1

no loss of generality!

Cantilever test



Well-known in Engineering and Computer Graphics
(here, finite rotations)

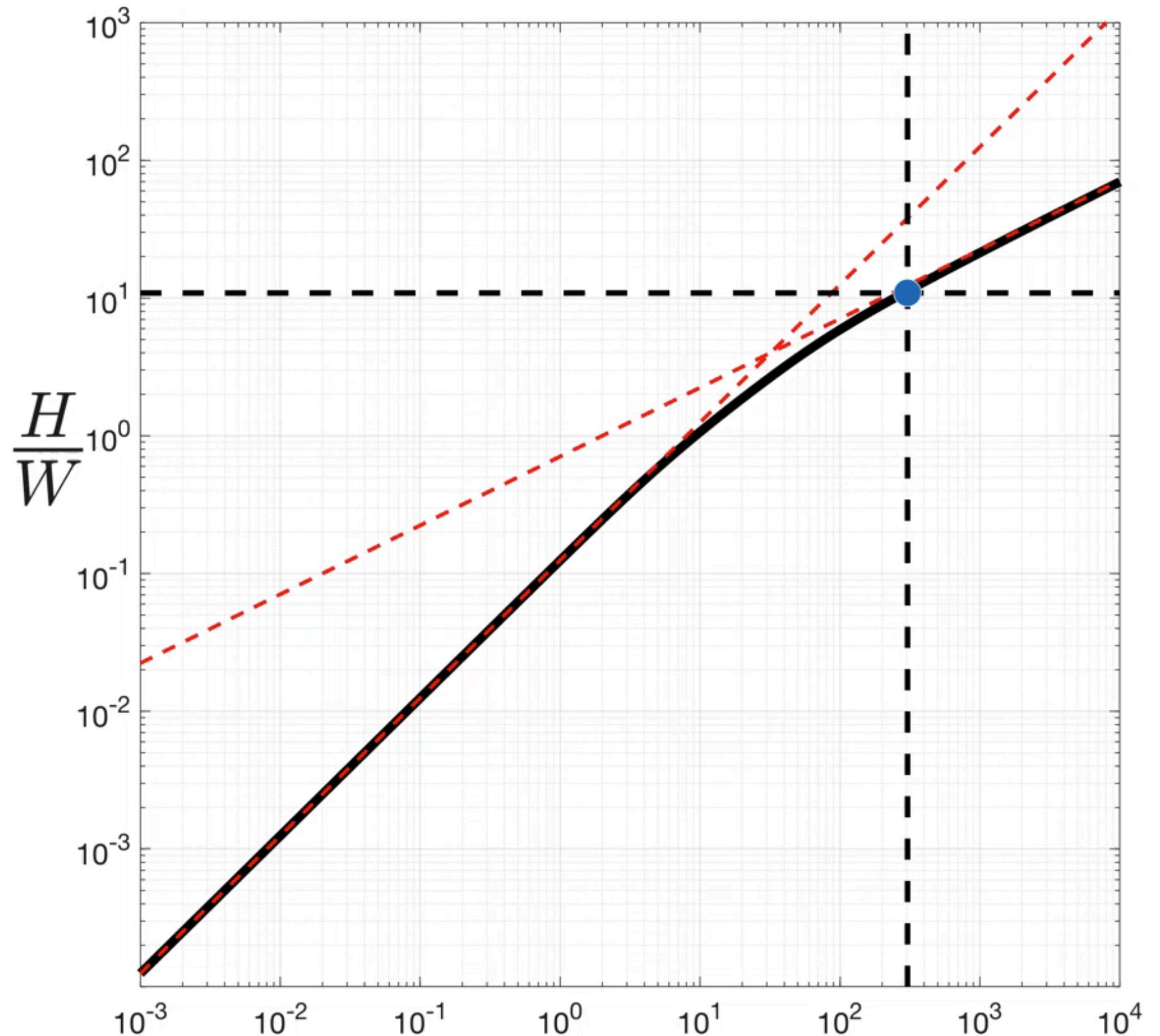
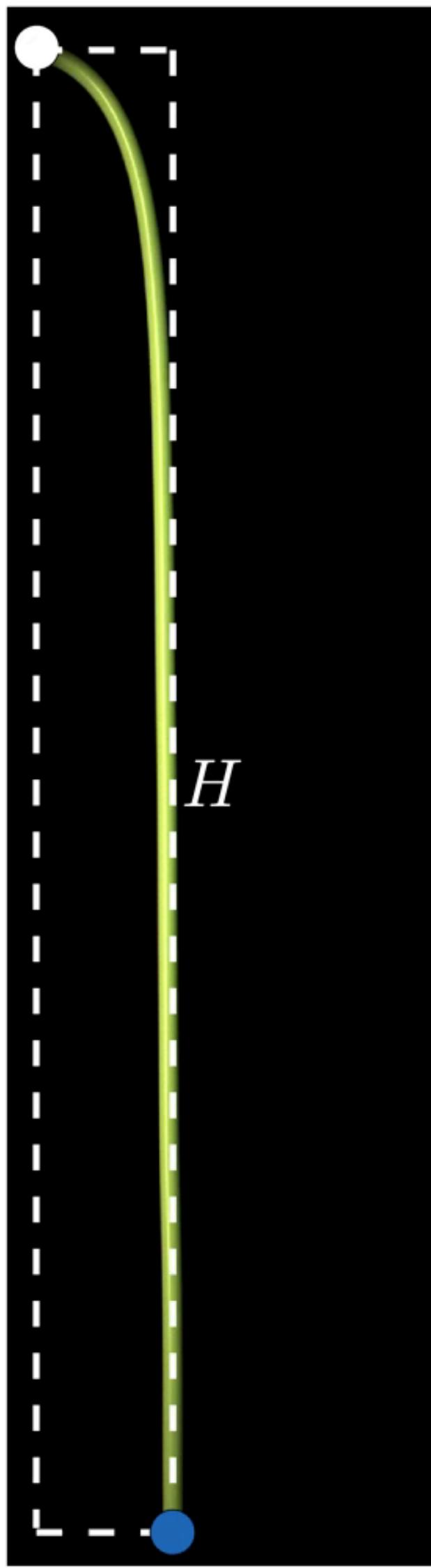
Bending rigidity EI

Length L

Weight Mg

Adim weight: $\Gamma = \frac{MgL^2}{EI}$

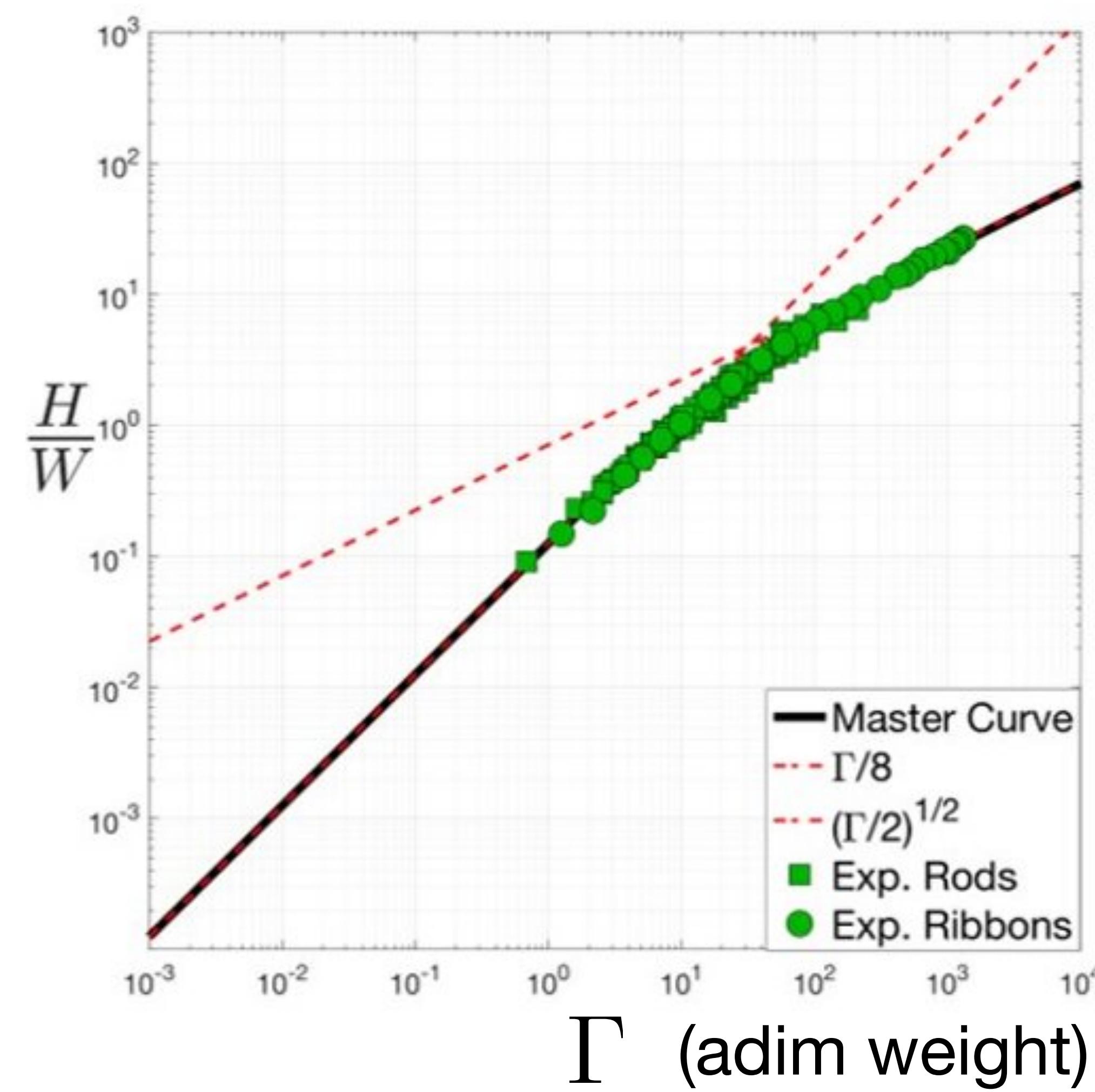
Cantilever test – experimental validation



$$\Gamma = \frac{MgL^2}{EI} \quad (\text{adim weight})$$



Cantilever test – experimental validation



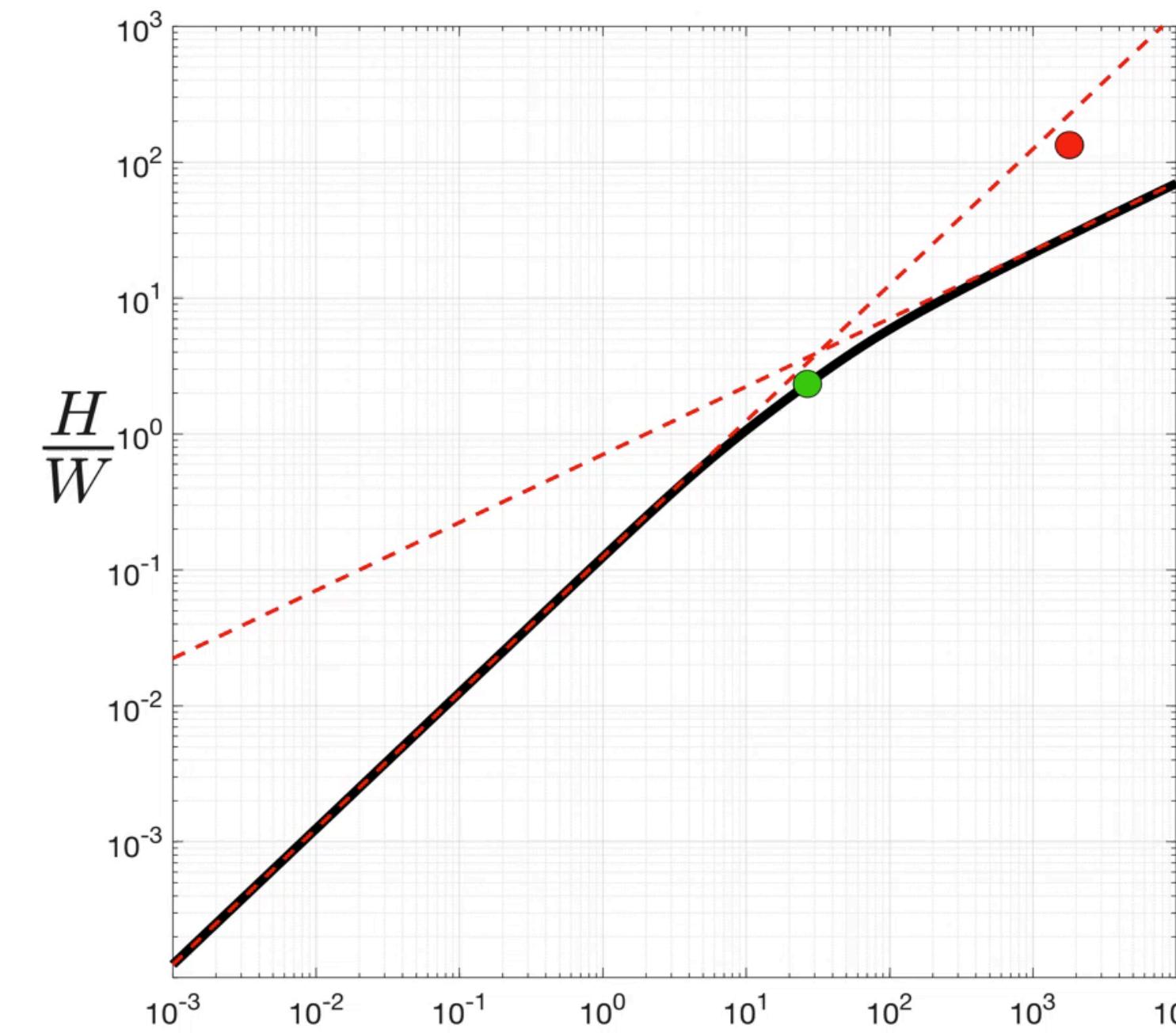
Results

methodology

the simulator output must match the master curve
over a range of physical parameters

\Rightarrow OK or KO

OK



KO

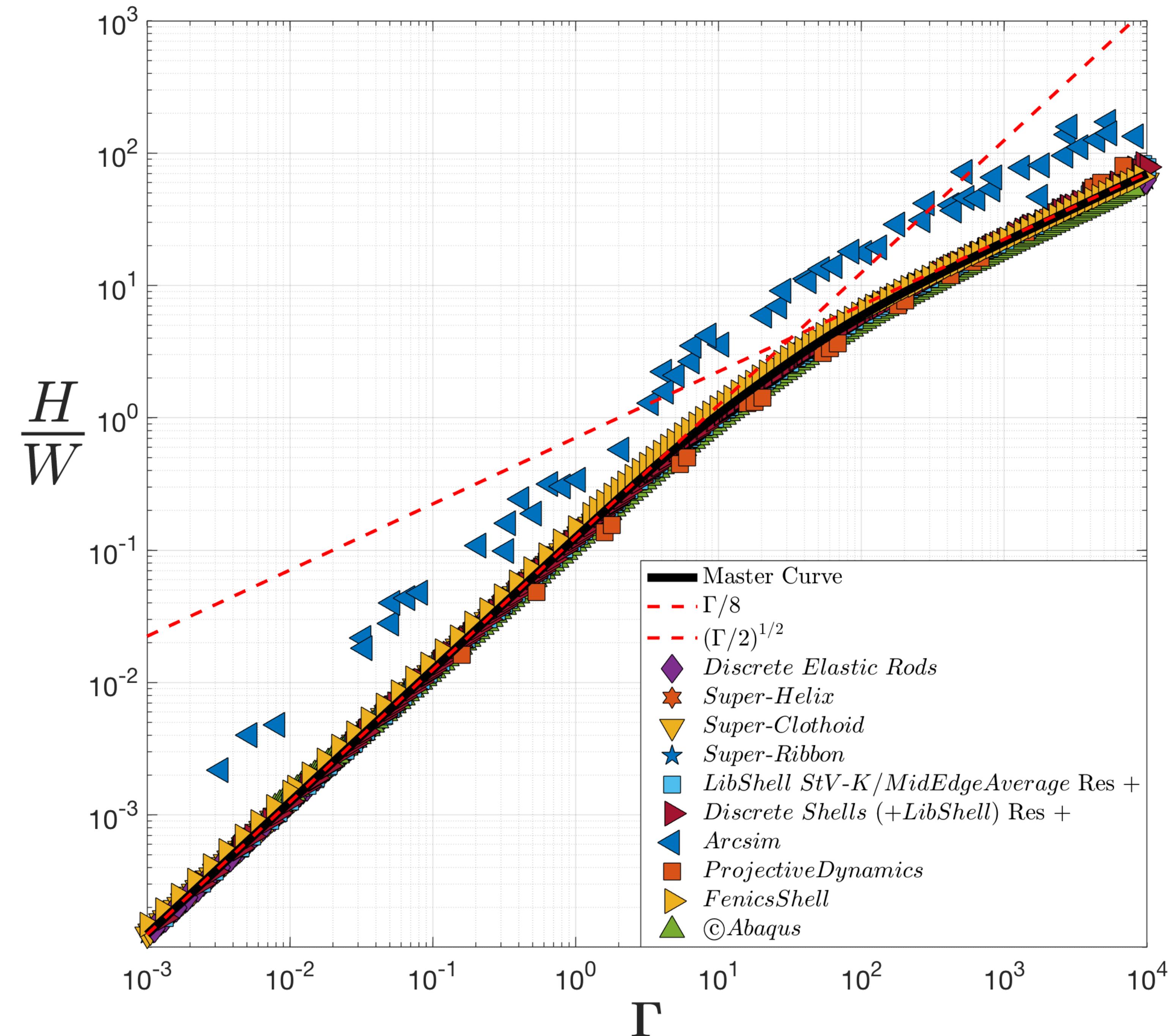
Results

Cantilever test

| Tested Code | Cantilever | Bend-Twist | Lateral Buckling | Stick-Slip |
|--|----------------------------|---------------|----------------------------|---------------------------------------|
| Rod | | | | |
| DISCRETE ELASTIC ROD [Bergou et al. 2010] | OK (300 elts) | OK (200 elts) | - | - |
| SUPER-HELIX [Bertails et al. 2006] | OK (50 elts) | OK (30 elts) | - | - |
| SUPER-CLOTHOID [Casati and Bertails-Descoubes 2013] | OK (20 elts) | OK (25 elts) | - | - |
| Ribbon | | | | |
| SUPER-RIBBON [Charrondière et al. 2020] | OK (20 elts) | - | KO | - |
| Plate | | | | |
| LIBSHELL [Chen et al. 2018] | OK (Res 0) | - | OK (Res +) | - |
| DISCRETE SHELL (+ LIBSHELL) [Grinspun et al. 2003] | OK (Res +) | - | KO | - |
| ARCSIM [Narain et al. 2012] | KO | - | X | - |
| DISCRETE SHELL + ARCSIM (tentative fix of ARCSIM) | KO | - | X | - |
| PROJECTIVE DYNAMICS [Bouaziz et al. 2014] (fit) | KO | - | X | - |
| Contact & friction | | | | |
| VISCOUS FRICTION (+ SUPER-HELIX 2D) | - | - | - | KO |
| So-BOGUS [Daviet et al. 2011] (+ SUPER-HELIX 2D) | - | - | - | OK ($dt=0.5$ ms, $tol = 10^{-13}$ N) |
| ARGUS (\approx ARCSIM + So-BOGUS) [Li et al. 2018] | - | - | - | KO |
| ARGUS NON ADAPTIVE (fix of ARGUS) | - | - | - | OK ($dt=0.5$ ms, $tol = 10^{-13}$ N) |
| BRIDSON-HARMON [Bridson et al. 2002; Harmon et al. 2008] (+ ARCSIM) | - | - | - | KO |
| PROJECTIVE FRICTION [Ly et al. 2020] | - | - | - | KO |
| Reference codes in Mechanical Engineering | | | | |
| FENICSHELL [Hale et al. 2018] | OK (Res 0, $P_{2,3}$ elts) | - | OK (Res 0, $P_{2,3}$ elts) | - |
| ©ABAQUS | OK (200 P_2 elts) | KO | KO | OK ($dt=9\ \mu s$) |

Results

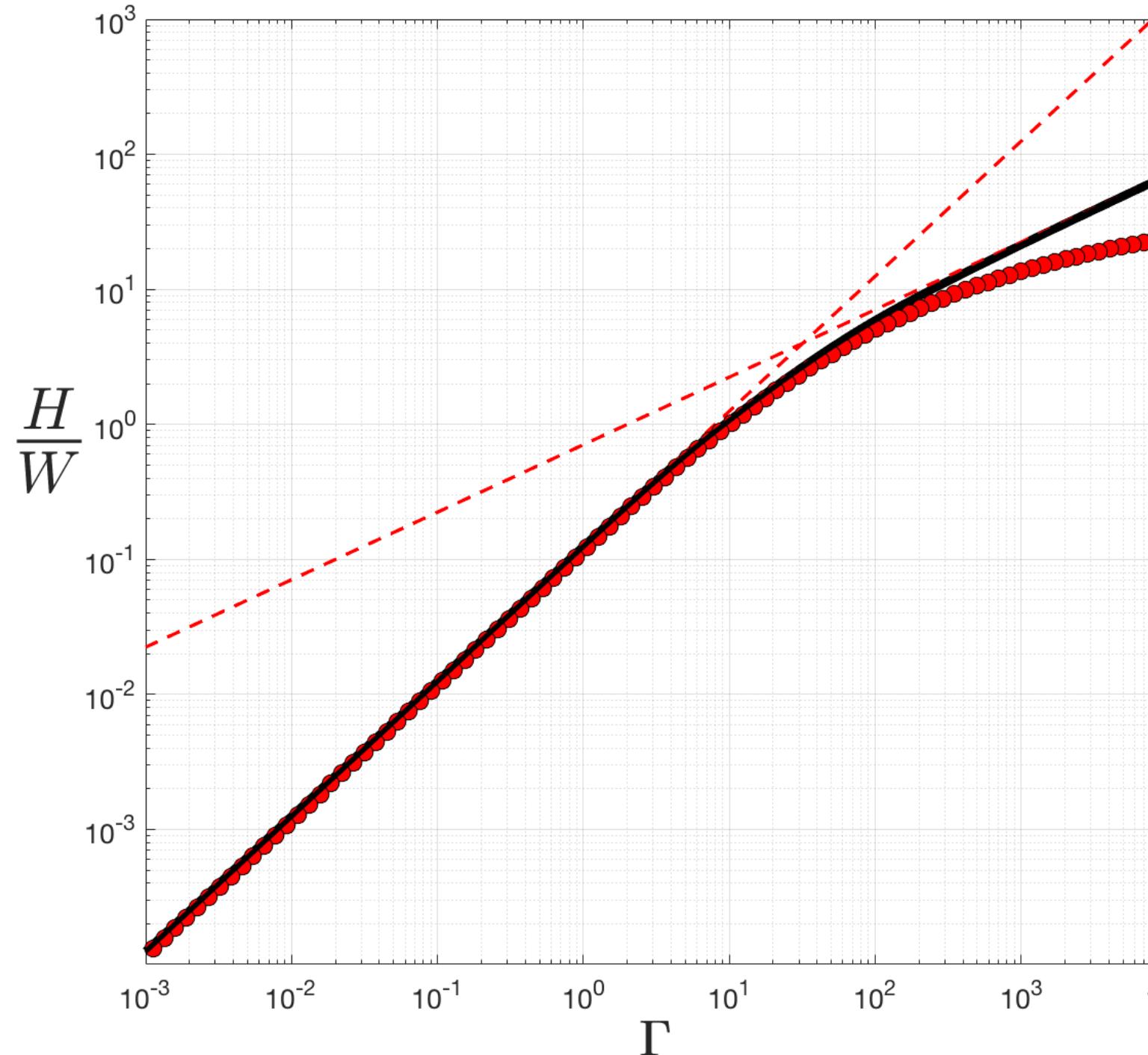
Cantilever test



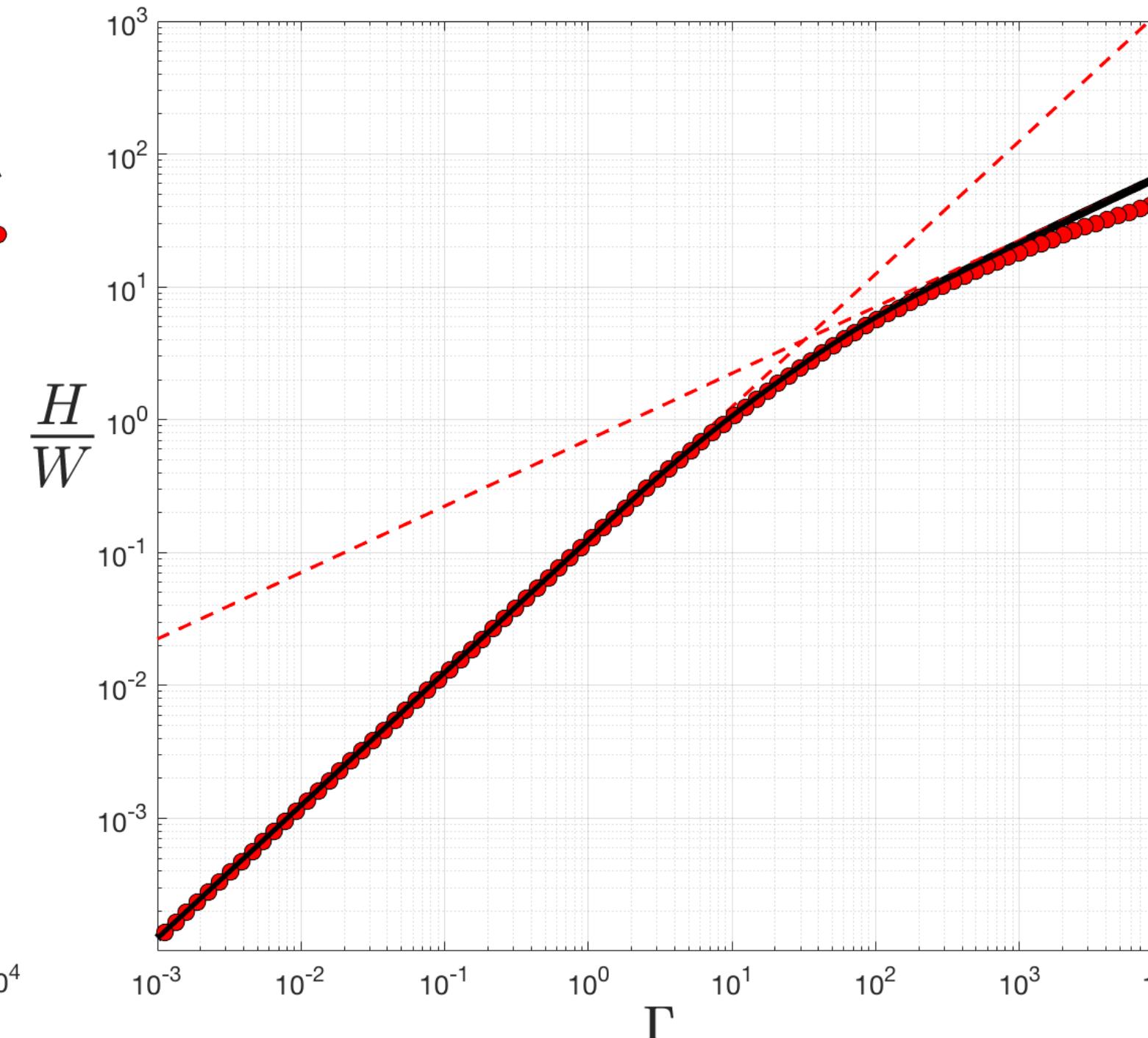
Results

Cantilever test: High values of Γ

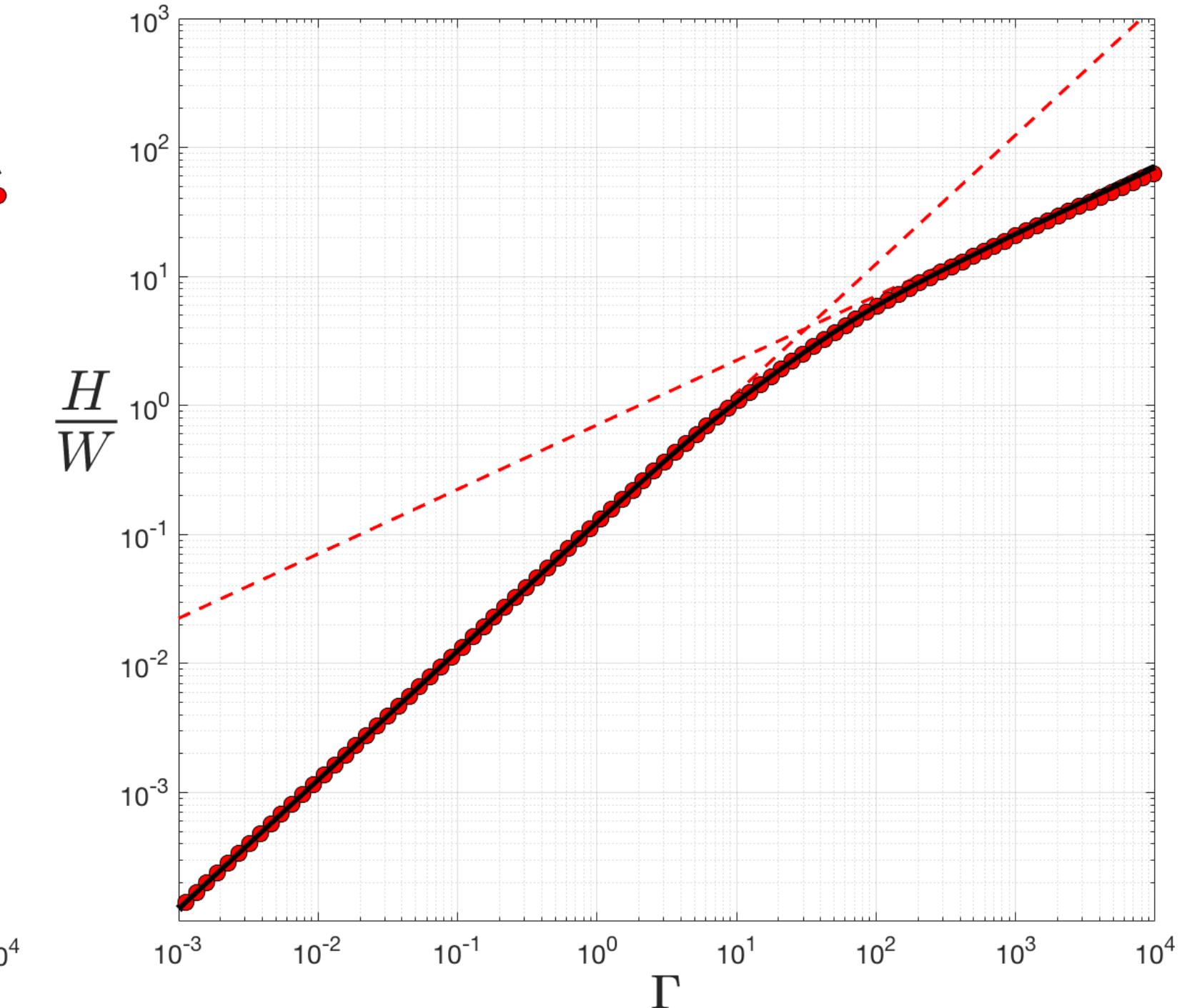
OK



30 elements



80 elements



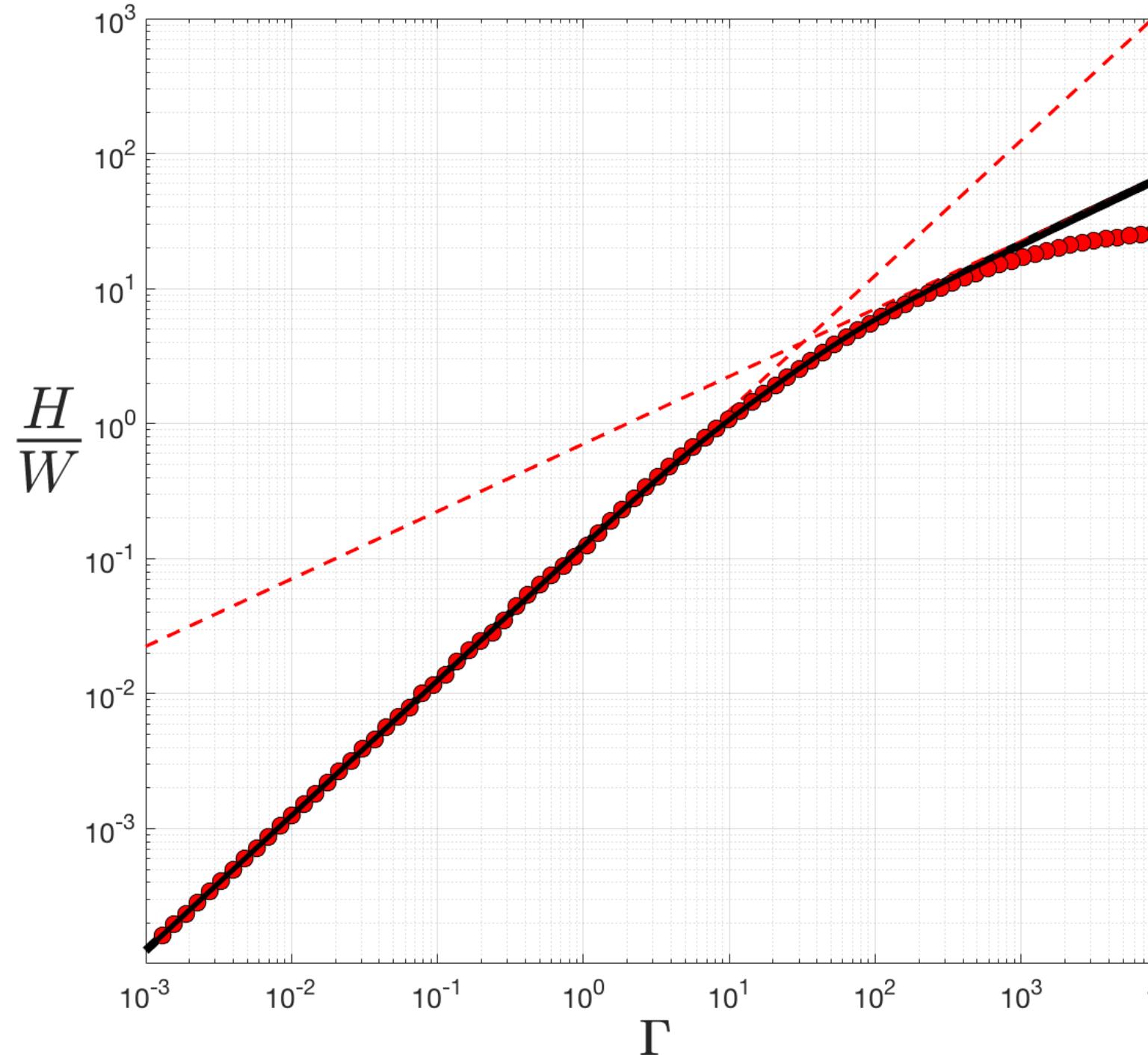
300 elements

Discrete Elastic Rod [M. Bergou et al. ACM Transactions on Graphics, 27 #3 (2008), 1–12]

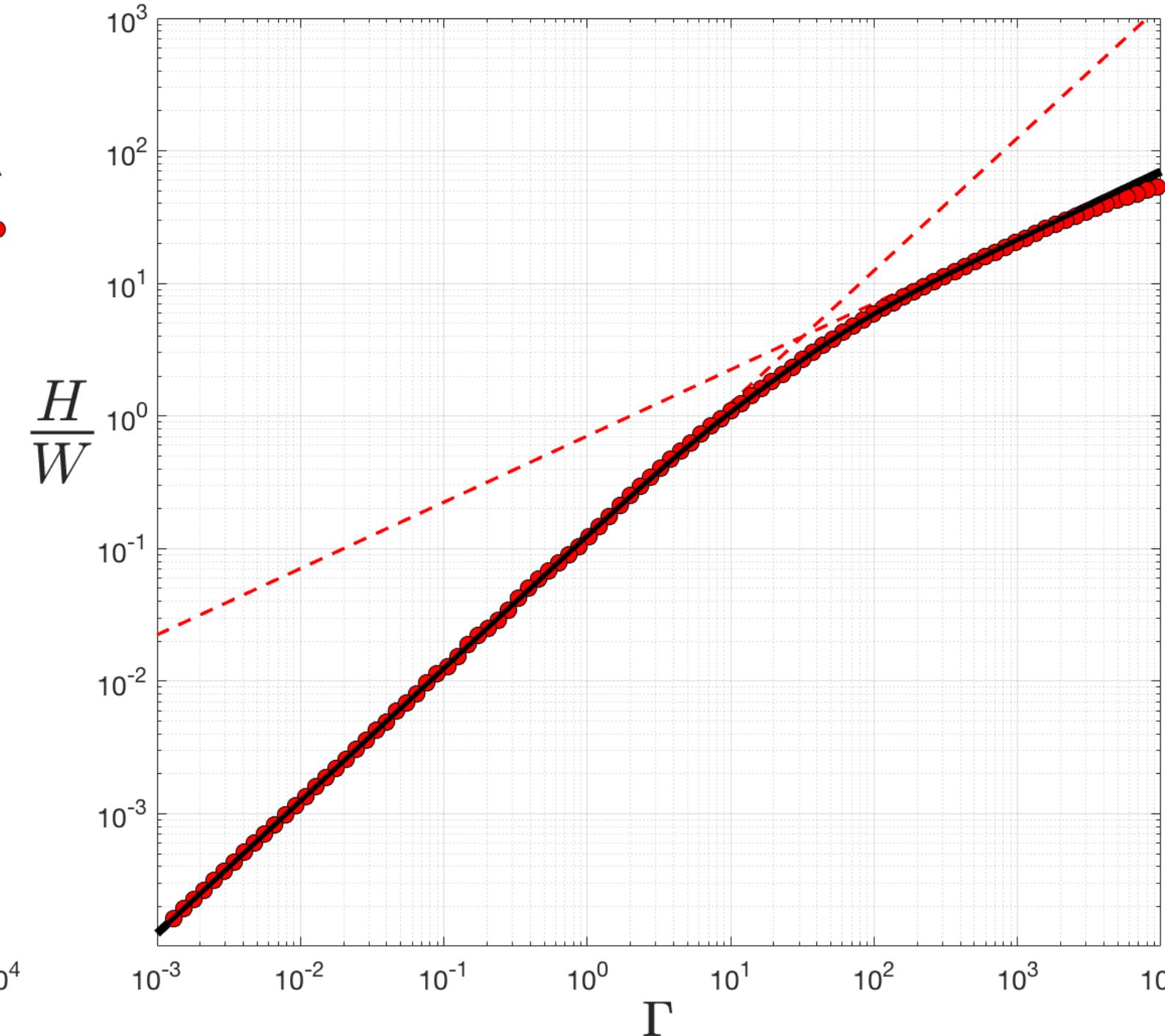
Results

Cantilever test: High values of Γ

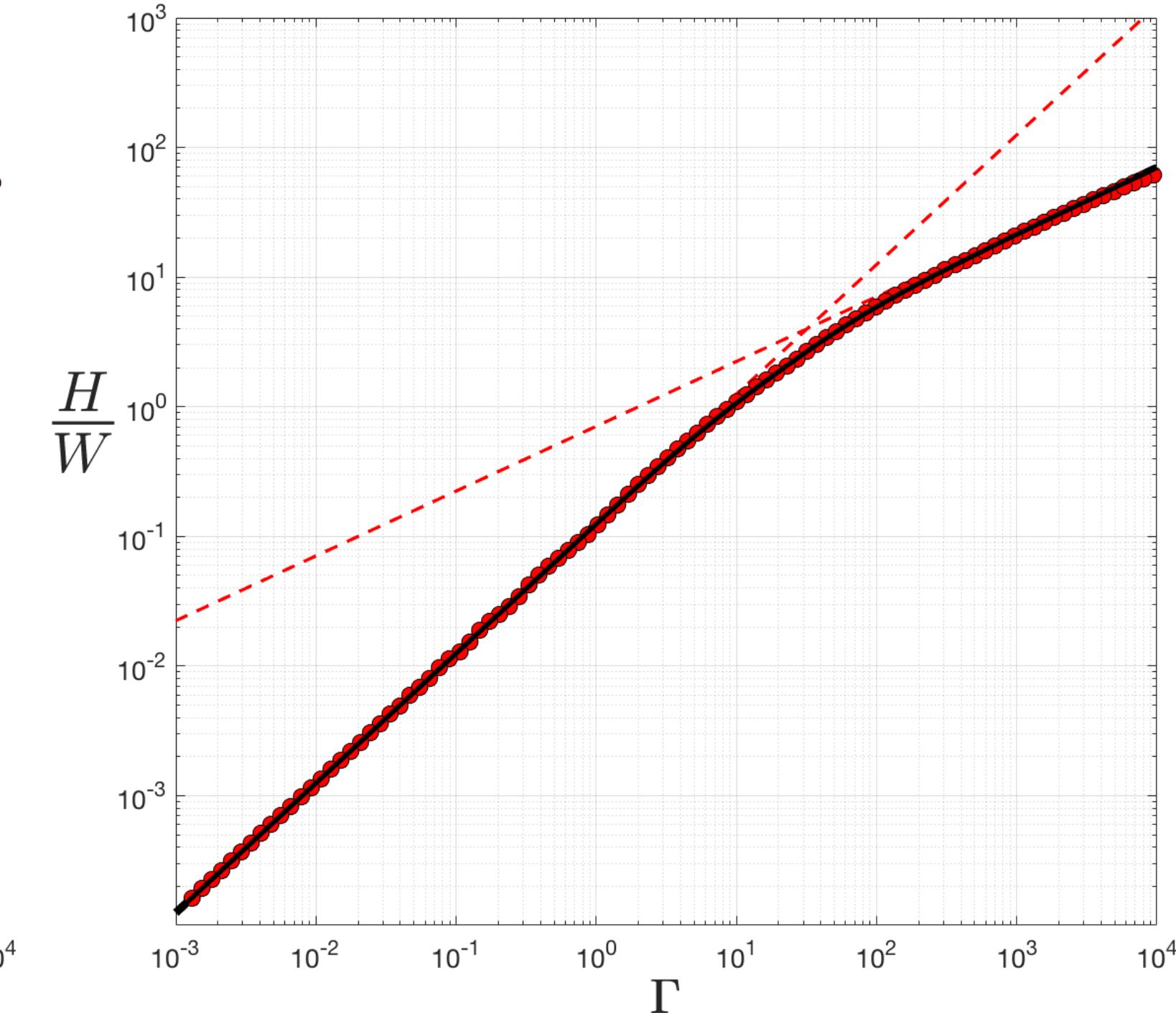
OK



10 elements



30 elements



50 elements

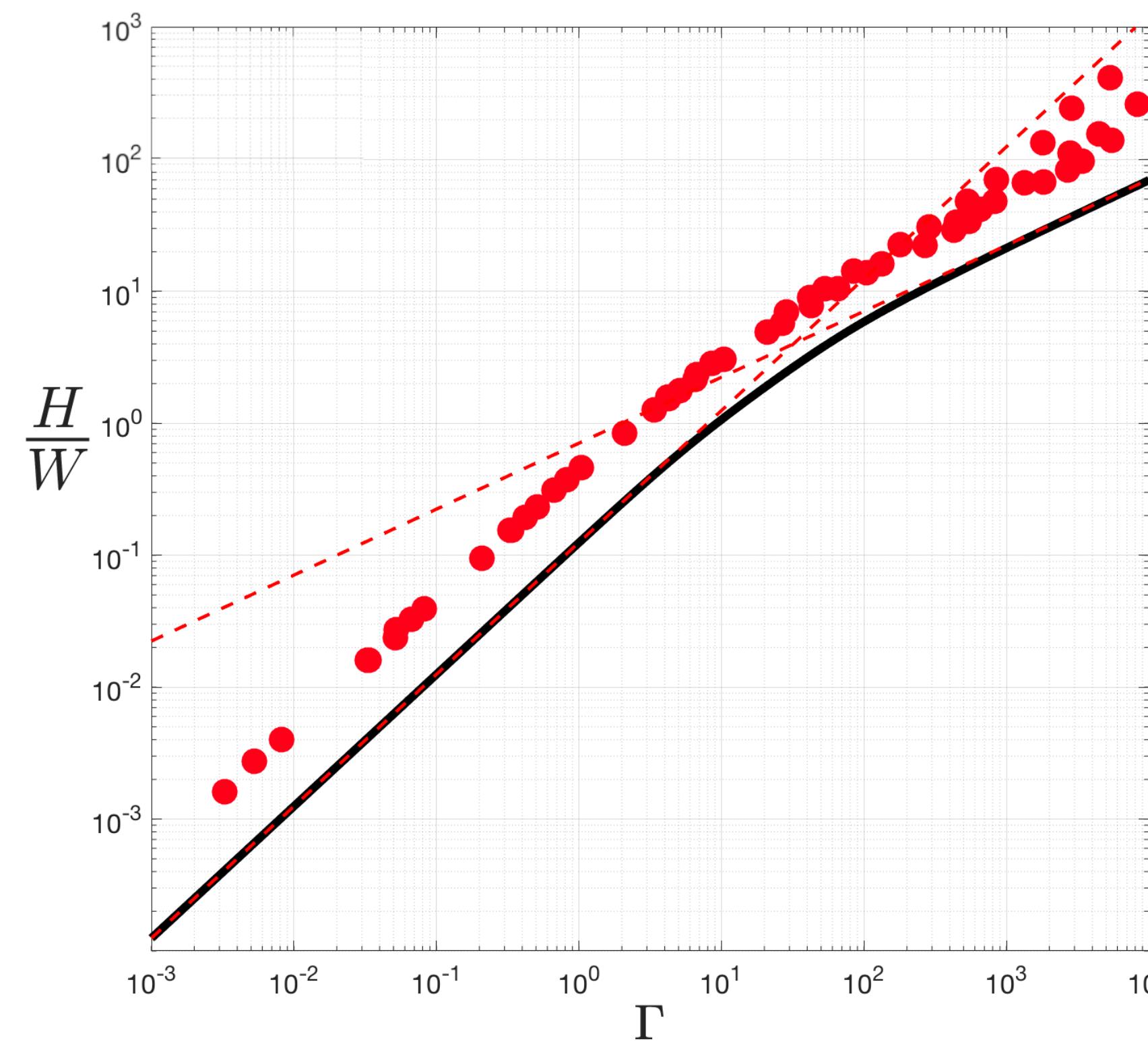
Super-Helix [F. Bertails et al. ACM Transactions on Graphics 25 #3 (2006) 1180–1187]

Results

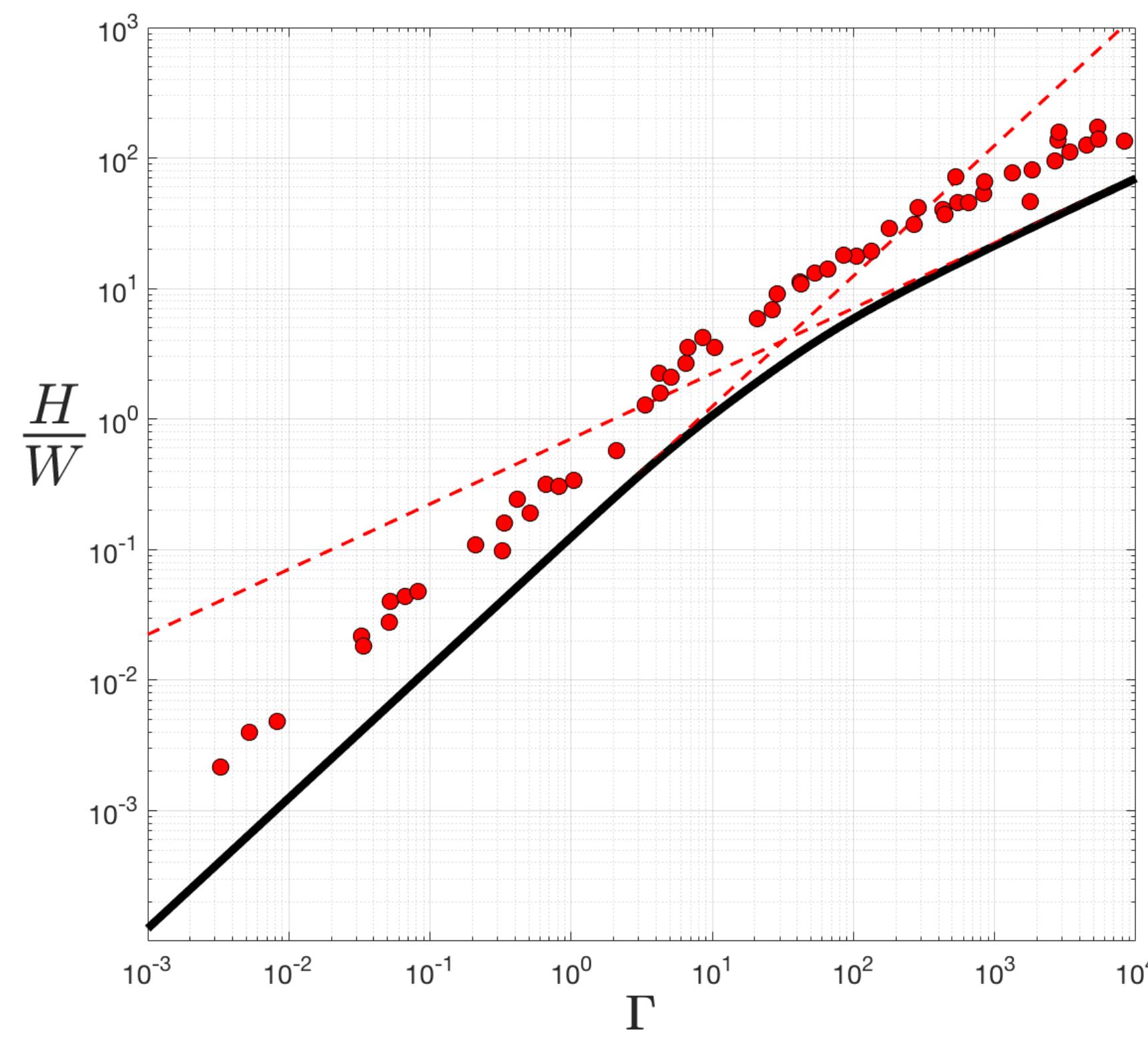
Cantilever test: ArcSim

Narain et al. ACM Transactions on Graphics (2012)

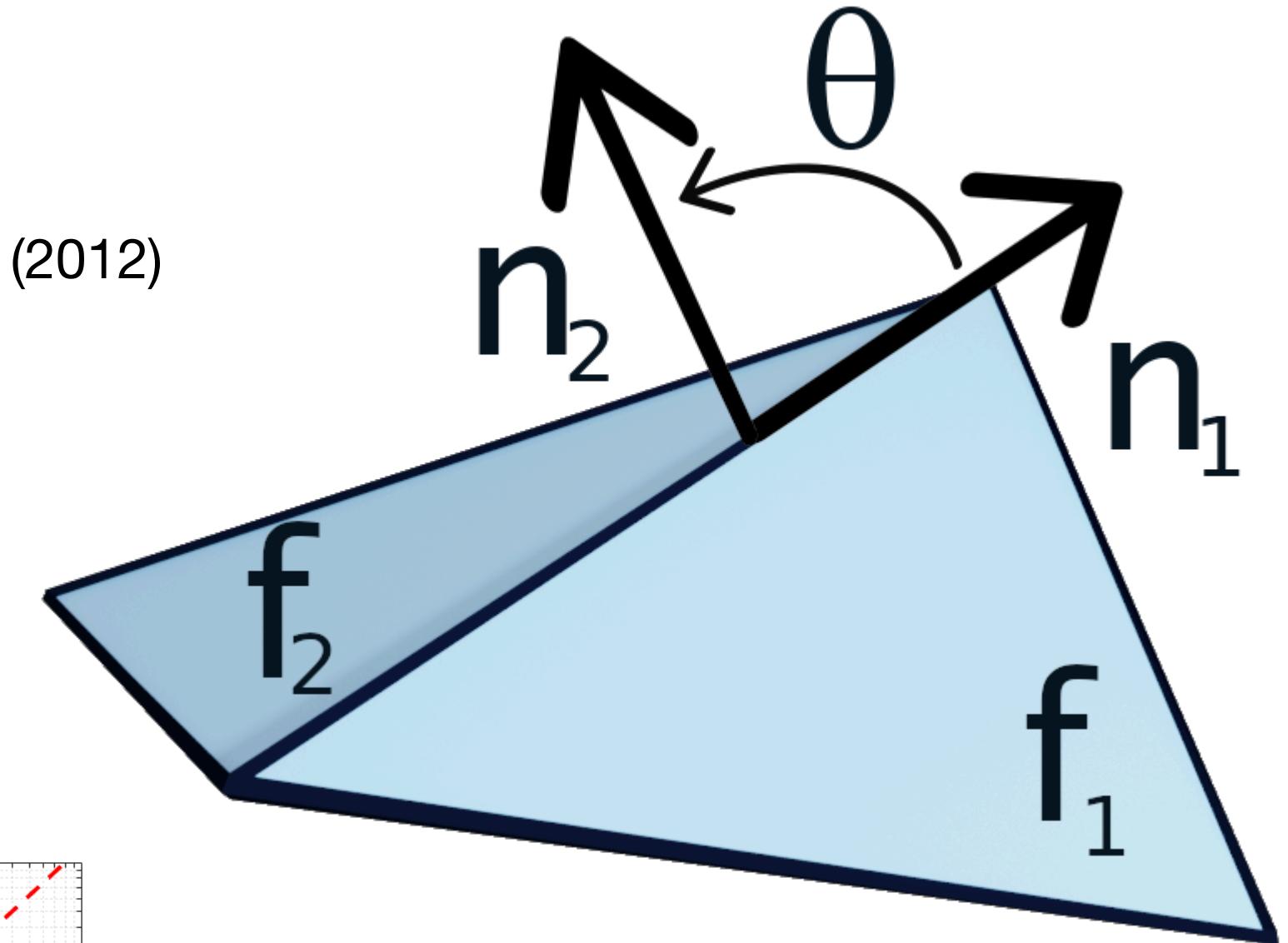
based on a discrete bending energy:



No remeshing



Adaptive remeshing



Shifted
and
scattered
KO

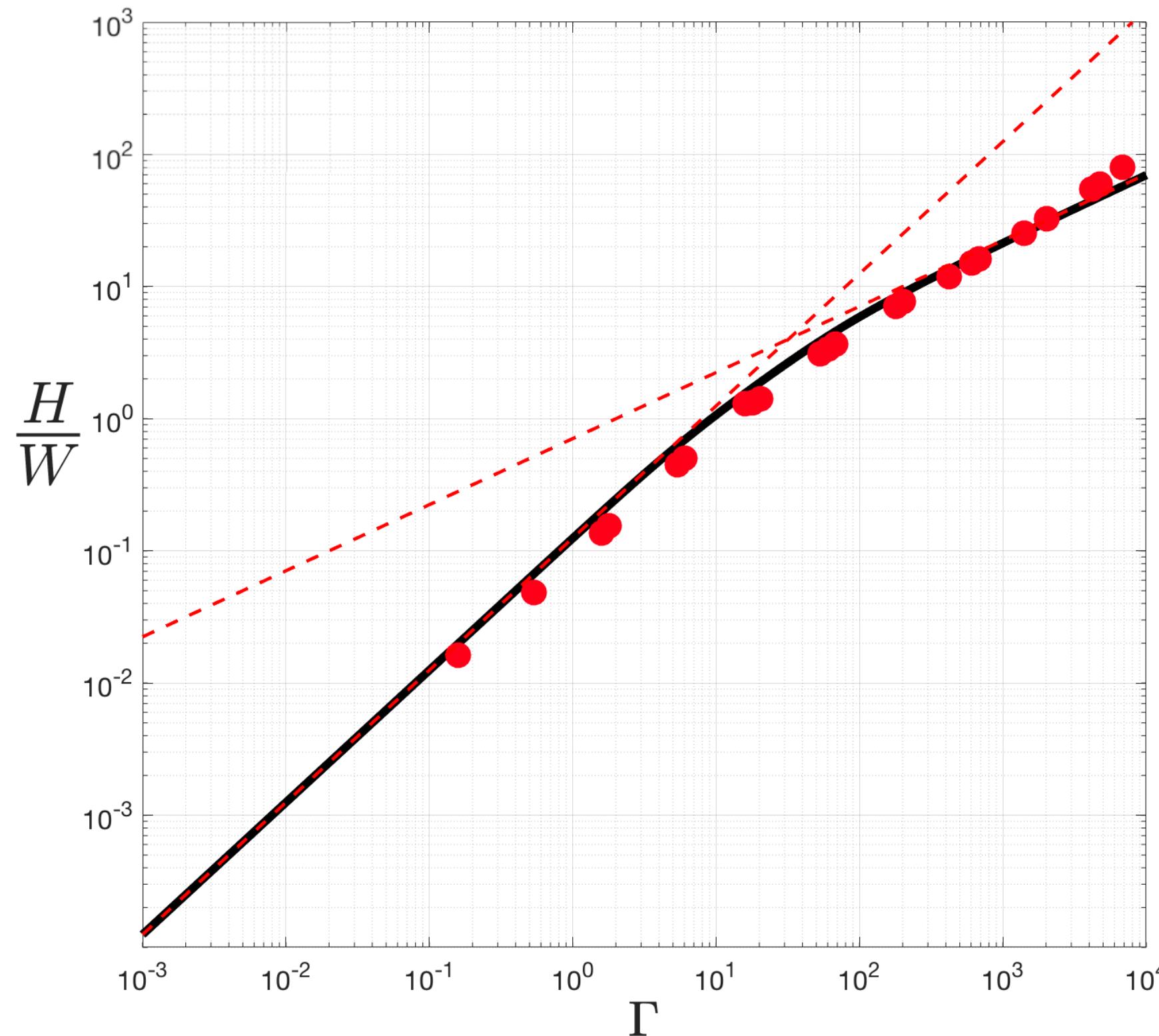
Results

Cantilever test: Projective Dynamics

Bouaziz et al. ACM Transaction on Graphics (2014)

Fitting the bending coefficient

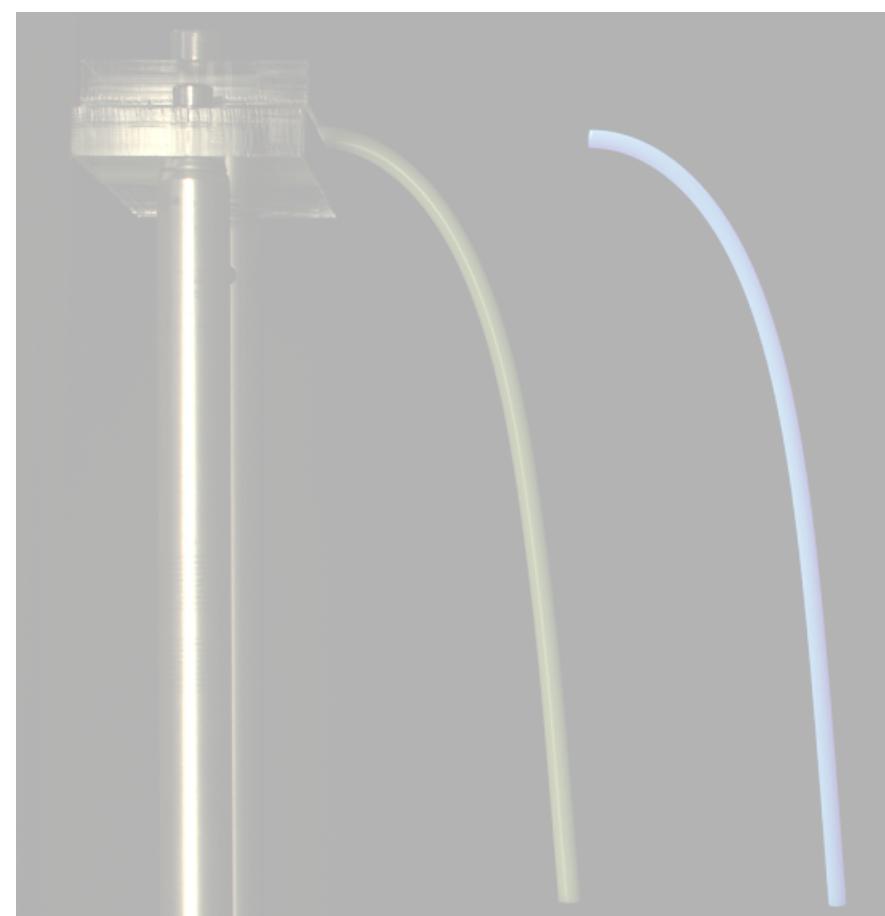
Bending modulus $B = \frac{Eh^3}{12(1 - \nu^2)}$ \rightarrow Fitted coefficient $k_B = 0.25B$



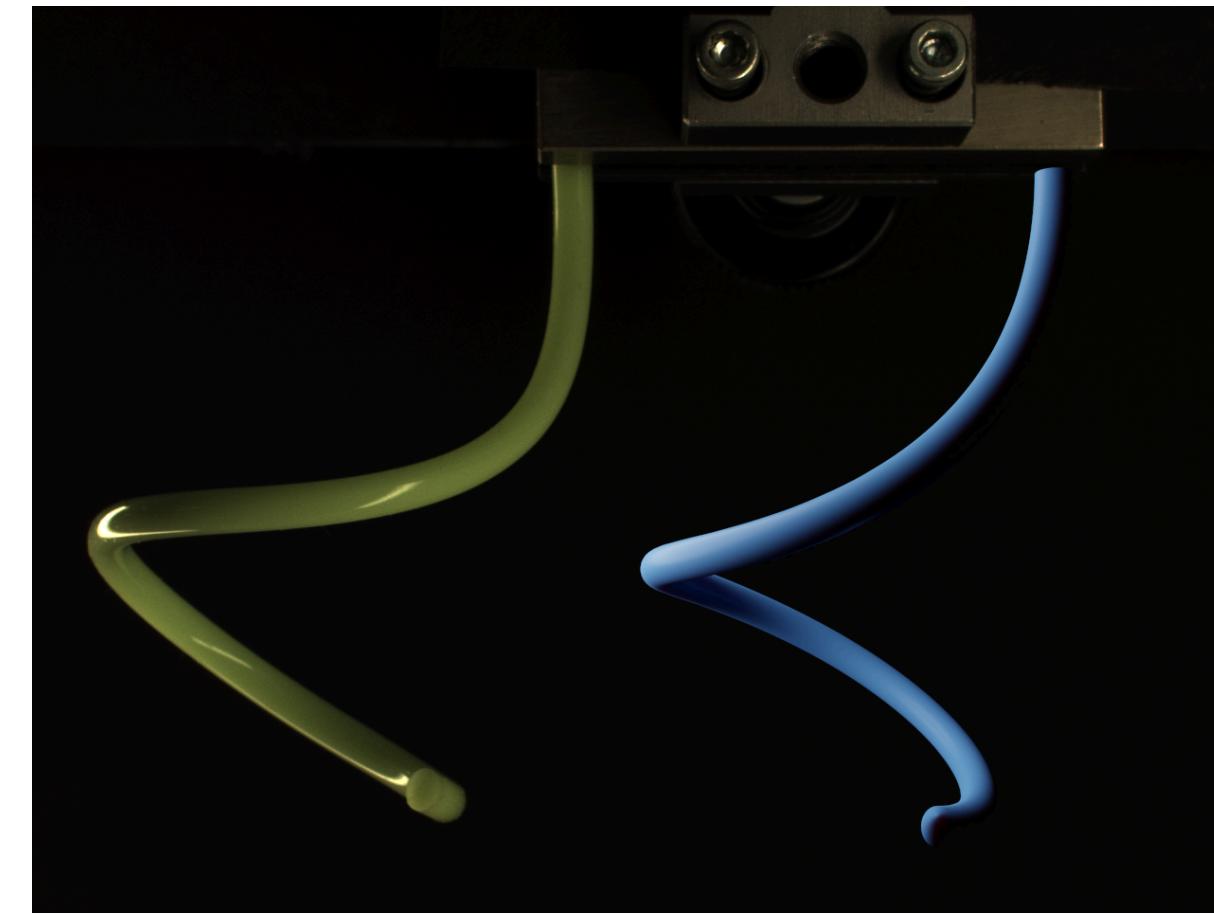
But *sparse results*:
Could not find reasonable solver parameters
to converge for *all* the parameter space

KO

The 4 tests



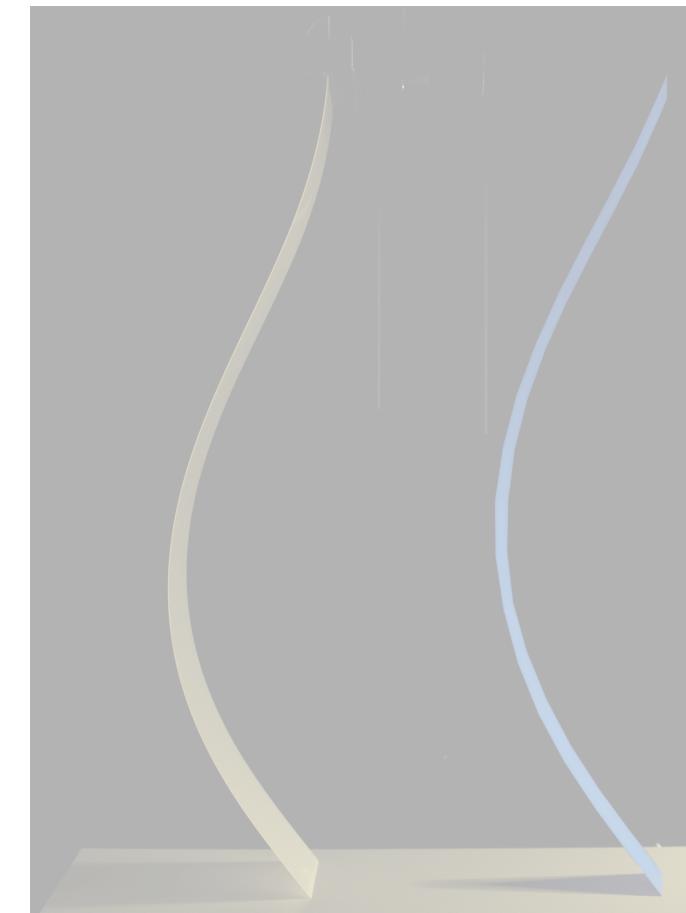
Cantilever



Bend-Twist

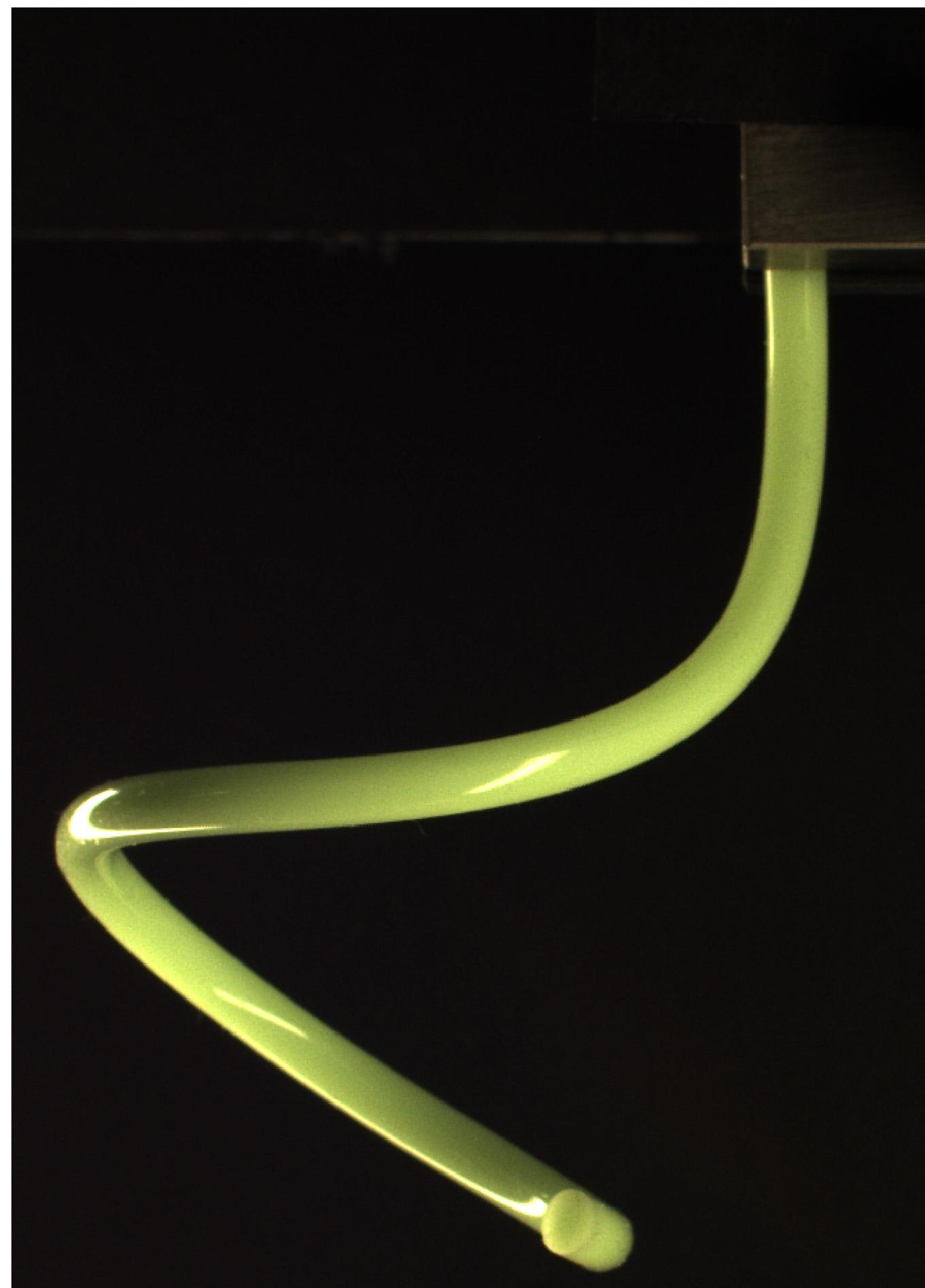


Lateral Buckling



Stick-Slip

Bend-Twist test (inspired from Miller et al. Phys Rev Lett. 2014)



Poisson's ratio $\nu = 0.5$
Twist rigidity $GJ = \frac{2}{3} EI$

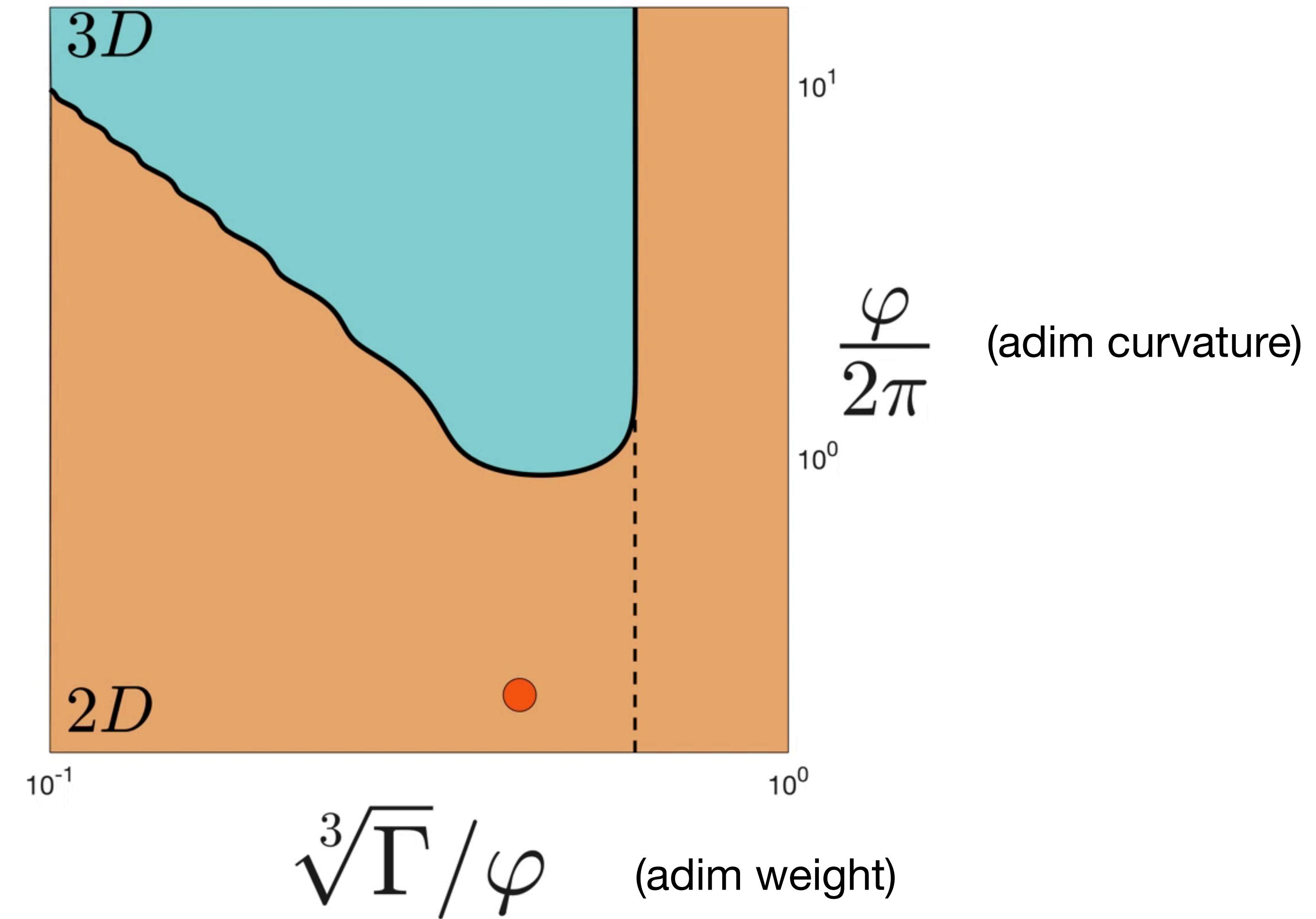
Bending rigidity EI
Length L
Weight Mg
Natural Curvature κ_0



$$\Gamma = \frac{MgL^2}{EI} \text{ and } \varphi = L \times \kappa_0$$

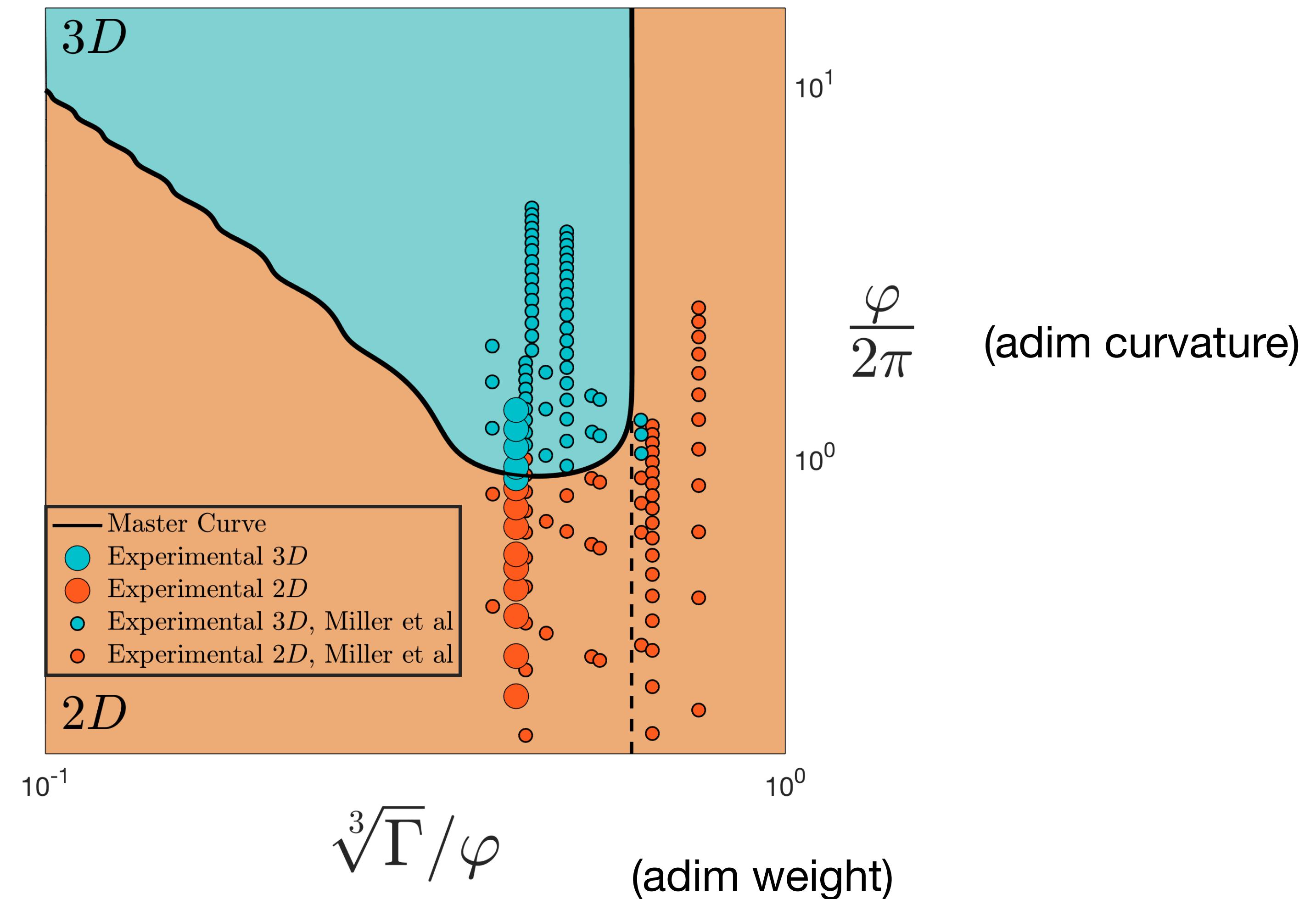
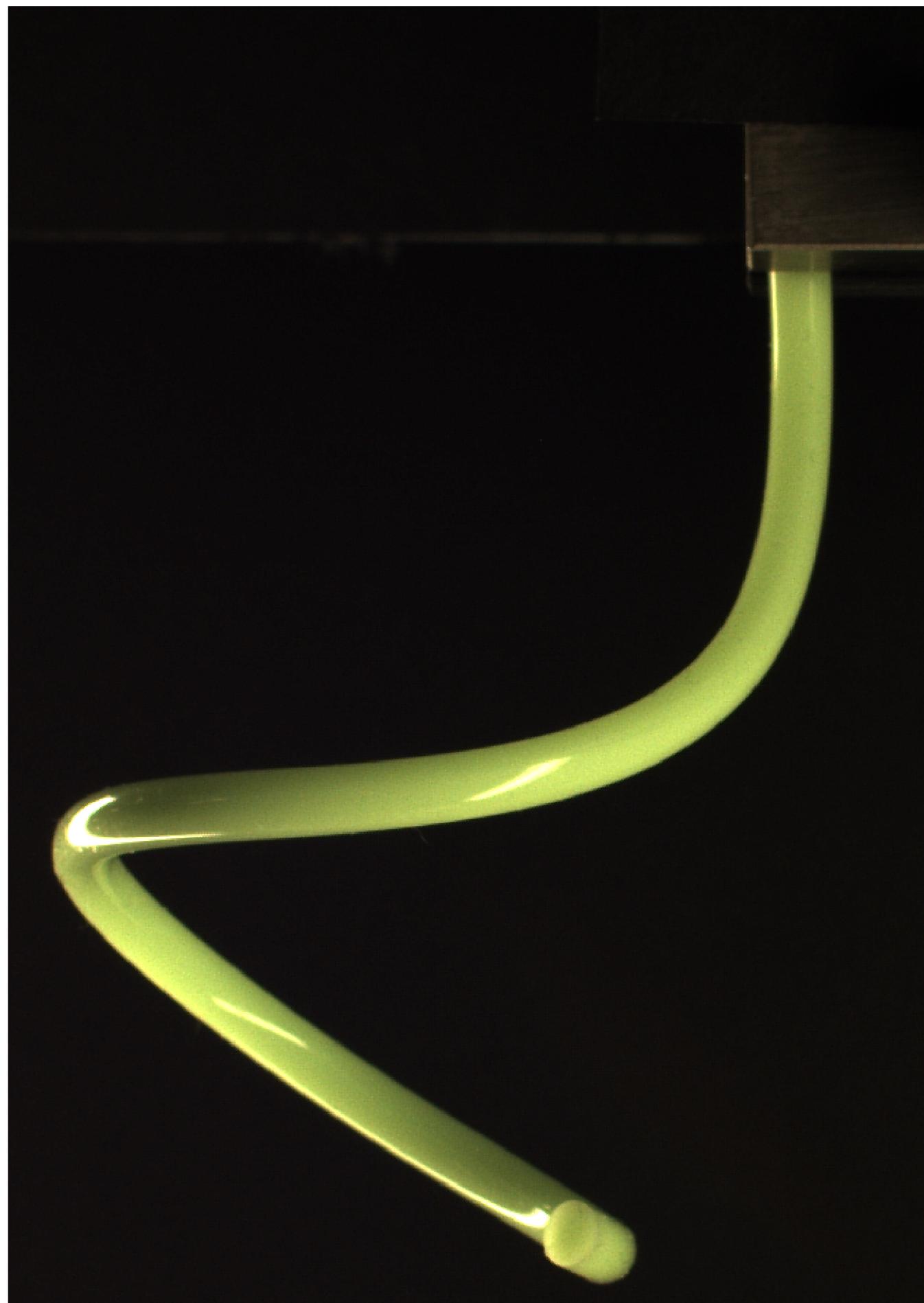
Bend-Twist test (inspired from Miller et al. Phys Rev Lett. 2014)

Experimental validation



Bend-Twist test (inspired from Miller et al. Phys Rev Lett. 2014)

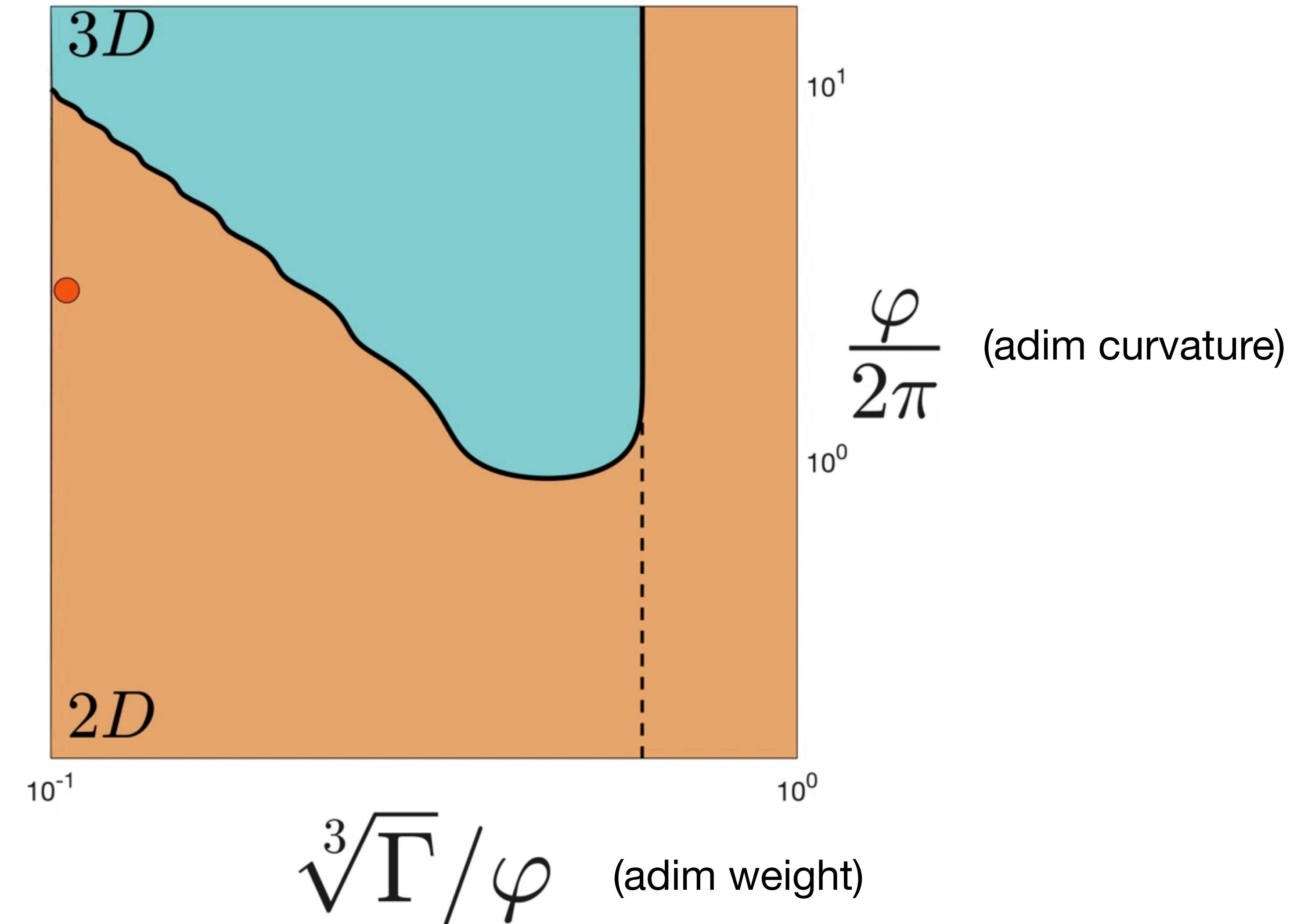
Experimental validation



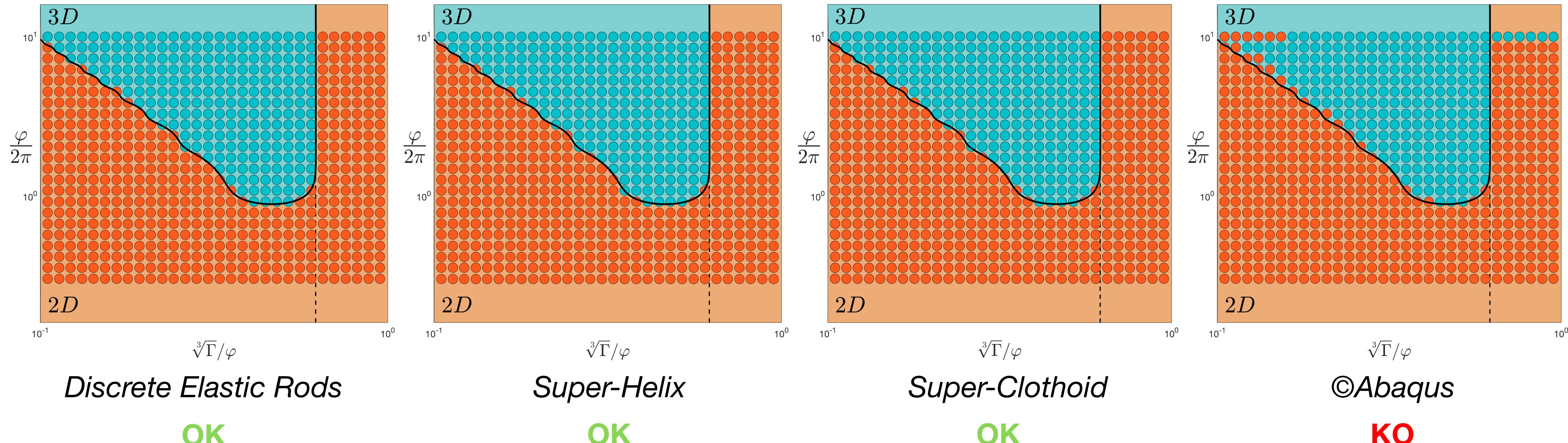
Bend-twist test: numerical results

O

equilibrium
computed
with increasing
 Γ values



Bend-twist test: numerical results



Bergou et al.
ACM Transactions on Graphics
27 #3 (2008)

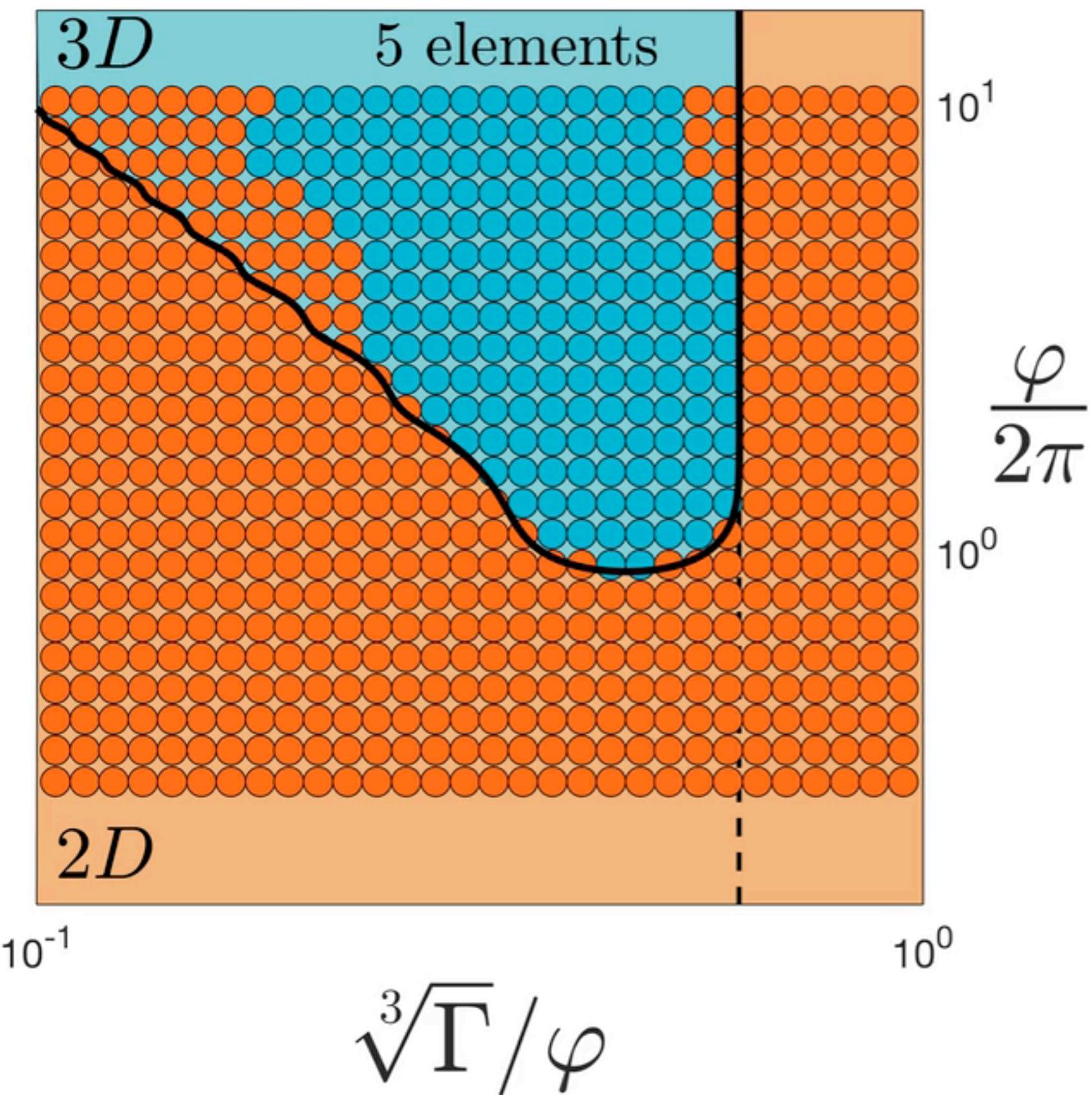
Bertails et al.
ACM Transactions on Graphics
25 #3 (2006)

Casati et al.
ACM Transactions on Graphics
32 #4 (2013)

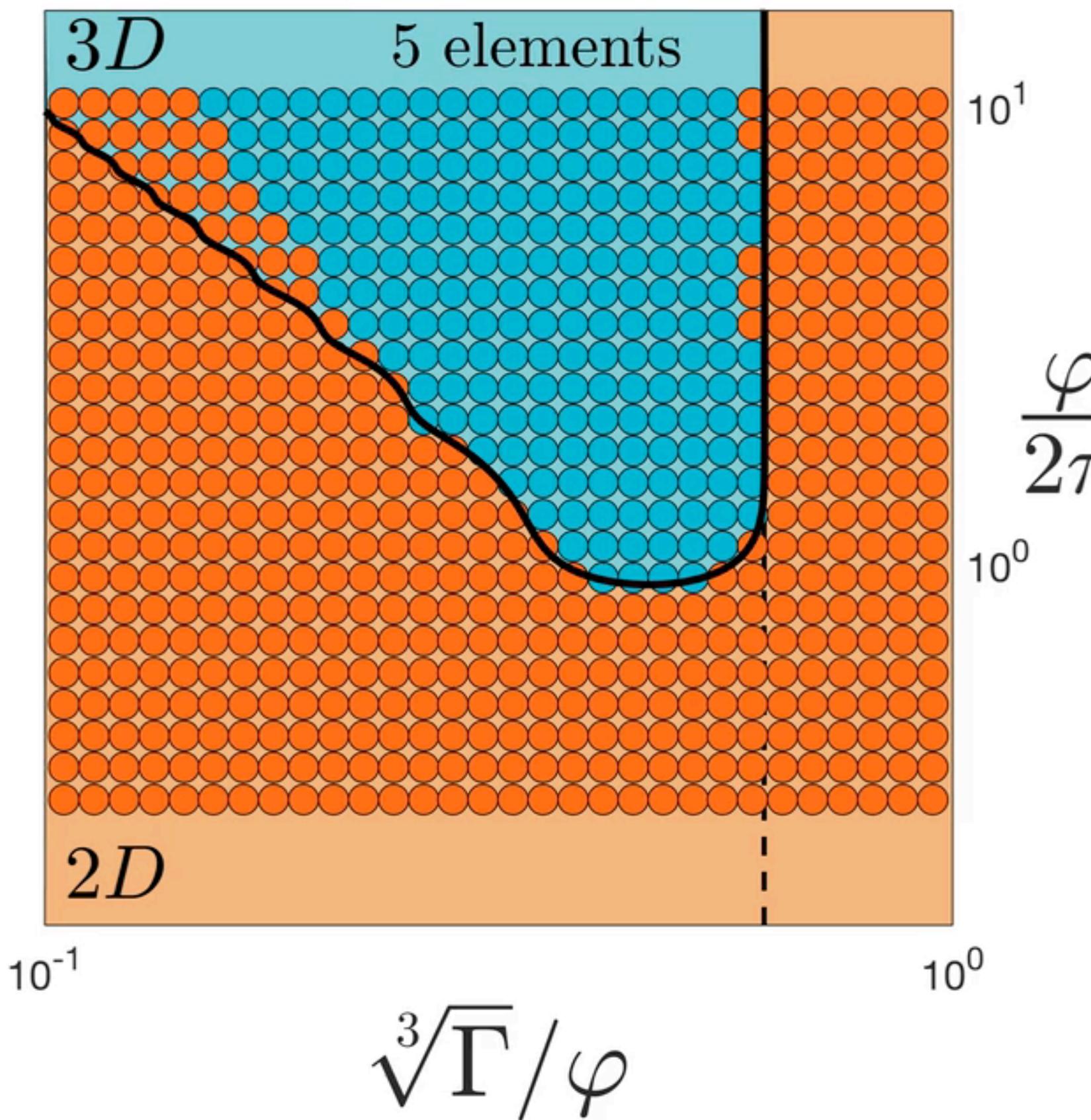
785 elements
Stabilized Newton routine
Warm-start from previous

Bend-twist test: mesh-size dependence

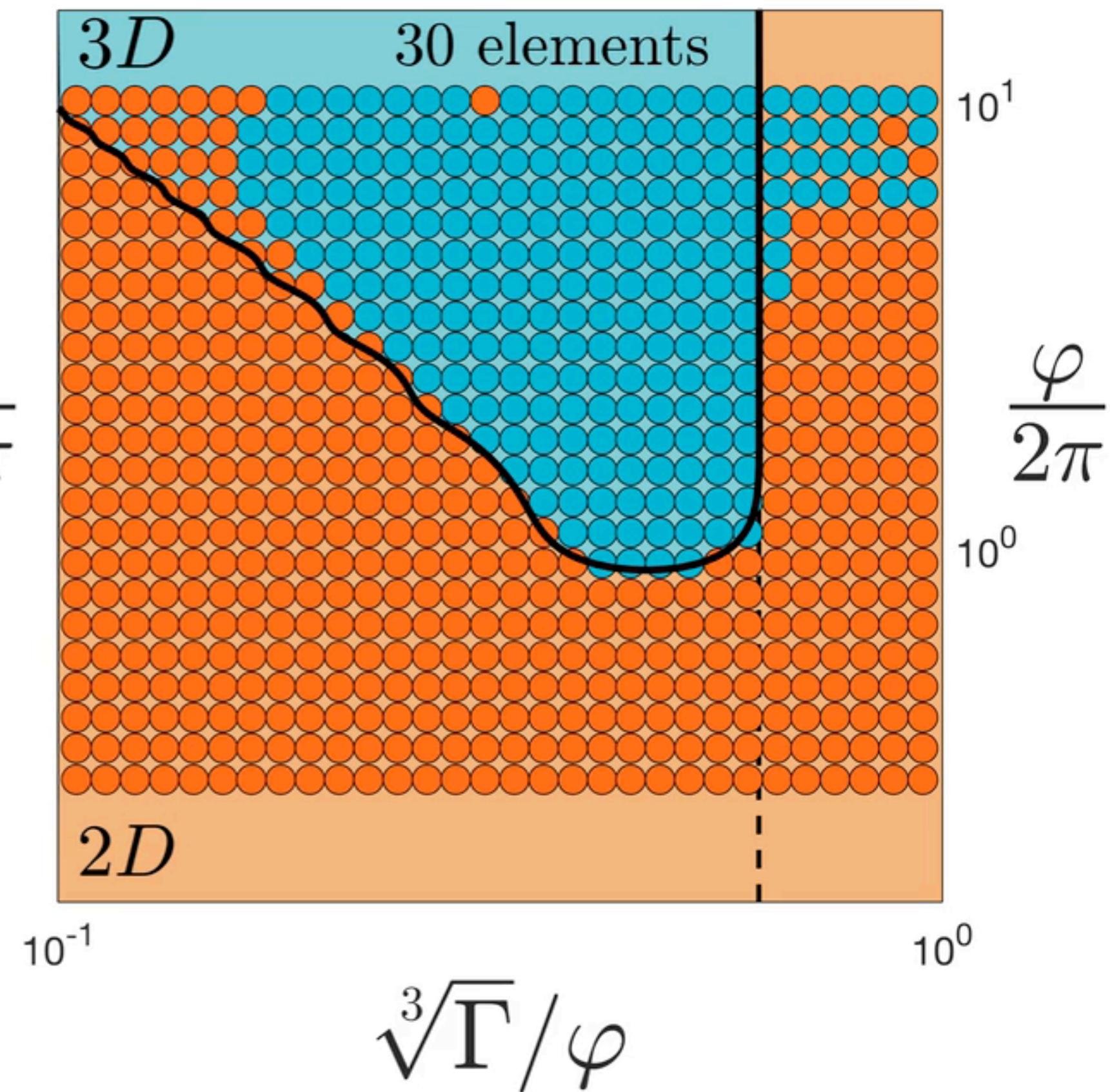
Super-Helix



Super-Clothoid



Discrete Elastic Rod

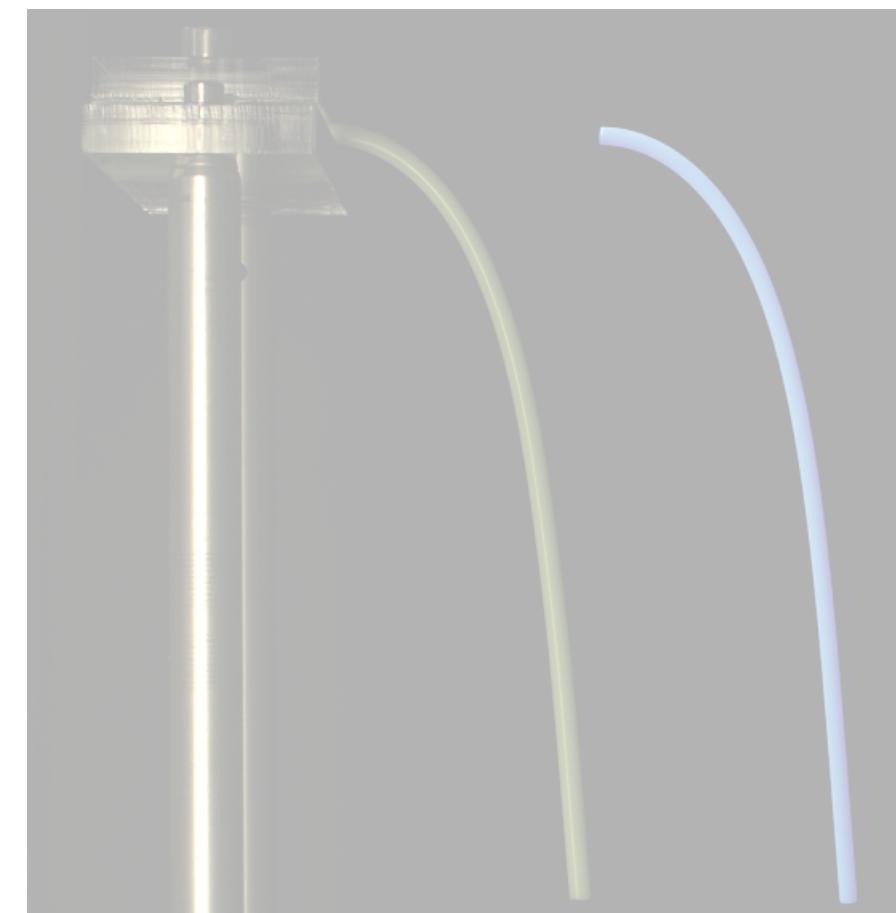


Results

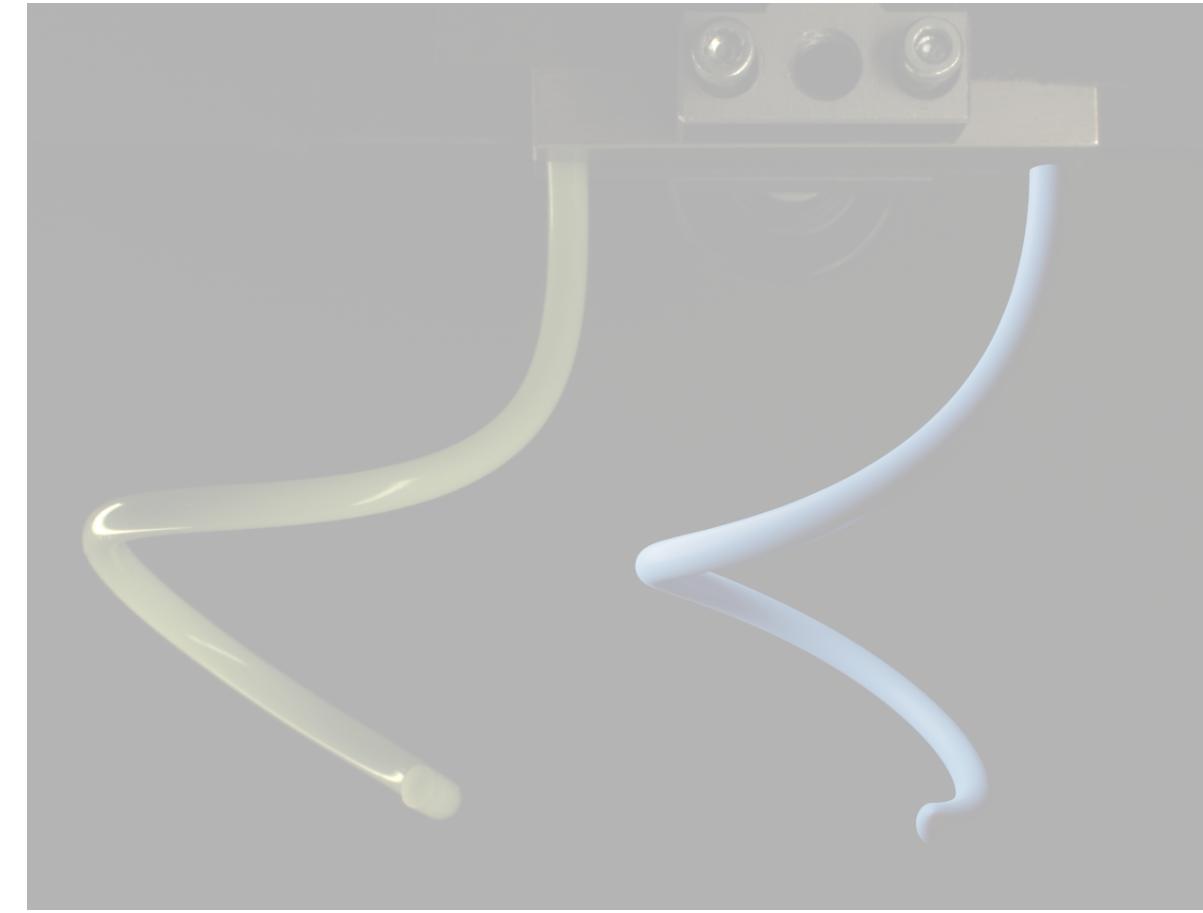
Bend-twist test

| Tested Code | Cantilever | Bend-Twist | Lateral Buckling | Stick-Slip |
|--|-----------------------------------|---------------|-----------------------------------|-------------------|
| Rod | | | | |
| DISCRETE ELASTIC ROD [Bergou et al. 2010] | OK (300 elts) | OK (200 elts) | - | - |
| SUPER-HELIX [Bertails et al. 2006] | OK (50 elts) | OK (30 elts) | - | - |
| SUPER-CLOTHOID [Casati and Bertails-Descoubes 2013] | OK (20 elts) | OK (25 elts) | - | - |
| Ribbon | | | | |
| SUPER-RIBBON [Charrondière et al. 2020] | OK (20 elts) | - | KO | - |
| Plate | | | | |
| LIBSHELL [Chen et al. 2018] | OK (Res 0) | - | OK (Res +) | - |
| DISCRETE SHELL (+ LIBSHELL) [Grinspun et al. 2003] | OK (Res +) | - | KO | - |
| ARCSIM [Narain et al. 2012] | KO | - | X | - |
| DISCRETE SHELL + ARCSIM (tentative fix of ARCSIM) | KO | - | X | - |
| PROJECTIVE DYNAMICS [Bouaziz et al. 2014] (fit) | KO | - | X | - |
| Contact & friction | | | | |
| VISCOUS FRICTION (+ SUPER-HELIX 2D) | - | - | | |
| So-BOGUS [Daviet et al. 2011] (+SUPER-HELIX 2D) | - | - | | |
| ARGUS (\approx ARCSIM + So-BOGUS) [Li et al. 2018] | - | - | | |
| ARGUS NON ADAPTIVE (fix of ARGUS) | - | - | | |
| BRIDSON-HARMON [Bridson et al. 2002; Harmon et al. 2008] (+ ARCSIM) | - | - | | |
| PROJECTIVE FRICTION [Ly et al. 2020] | - | - | | |
| Reference codes in Mechanical Engineering | | | | |
| FENICSHELL [Hale et al. 2018] | OK (Res 0, P _{2,3} elts) | - | OK (Res 0, P _{2,3} elts) | - |
| ©ABAQUS | OK (200 P ₂ elts) | KO | KO | OK (dt=9 μ s) |

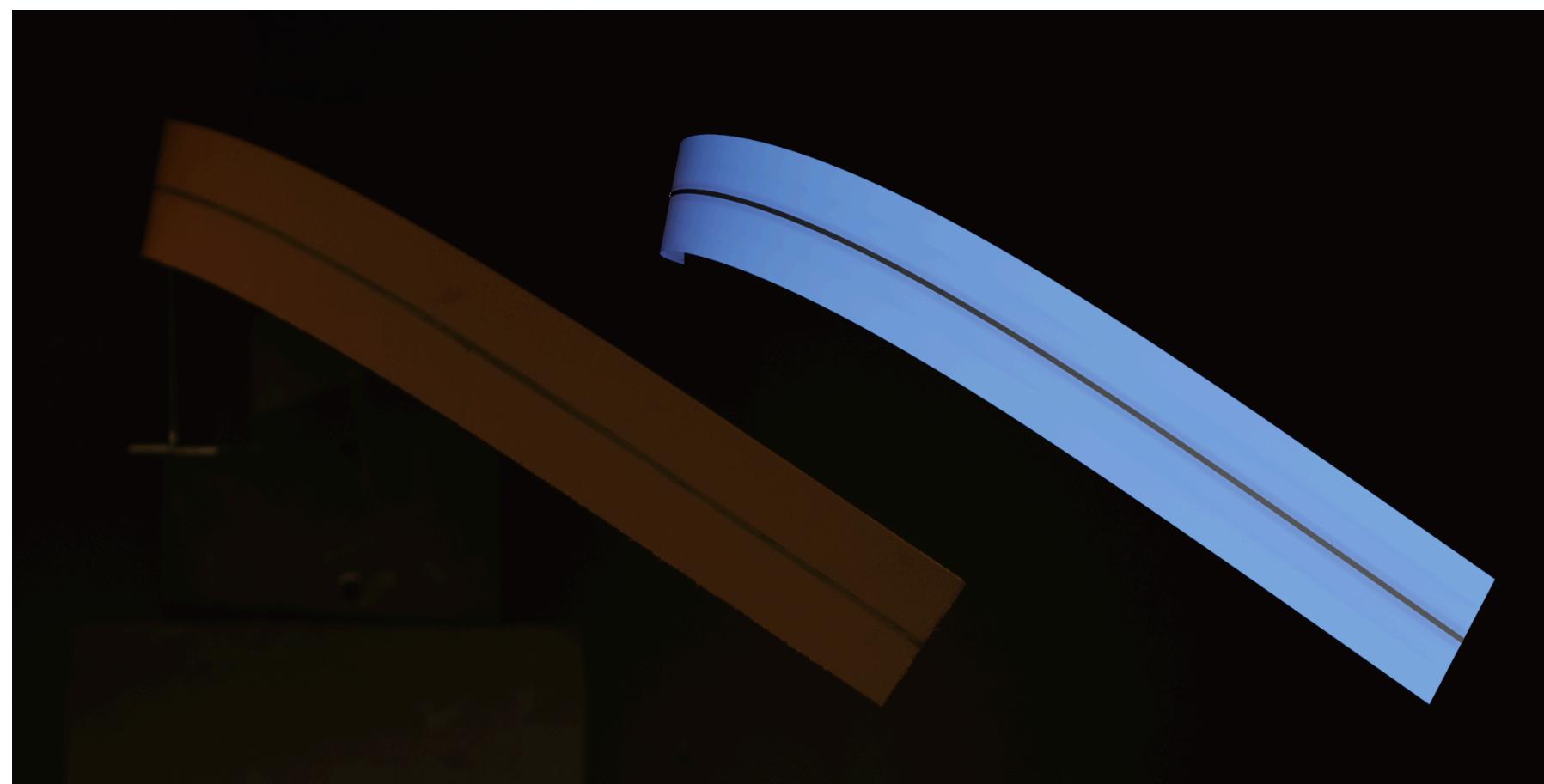
The 4 tests



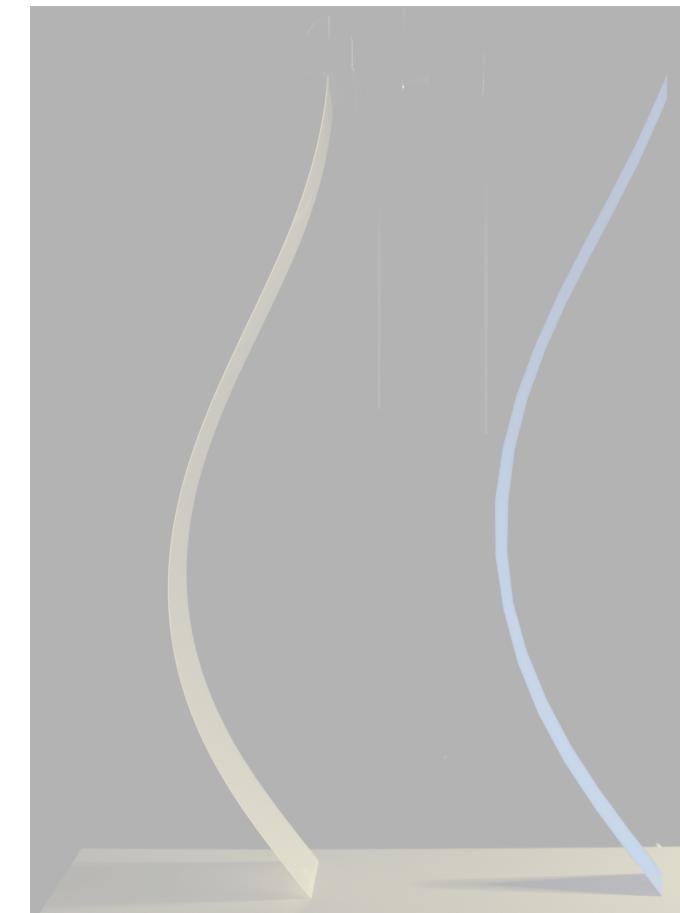
Cantilever



Bend-Twist

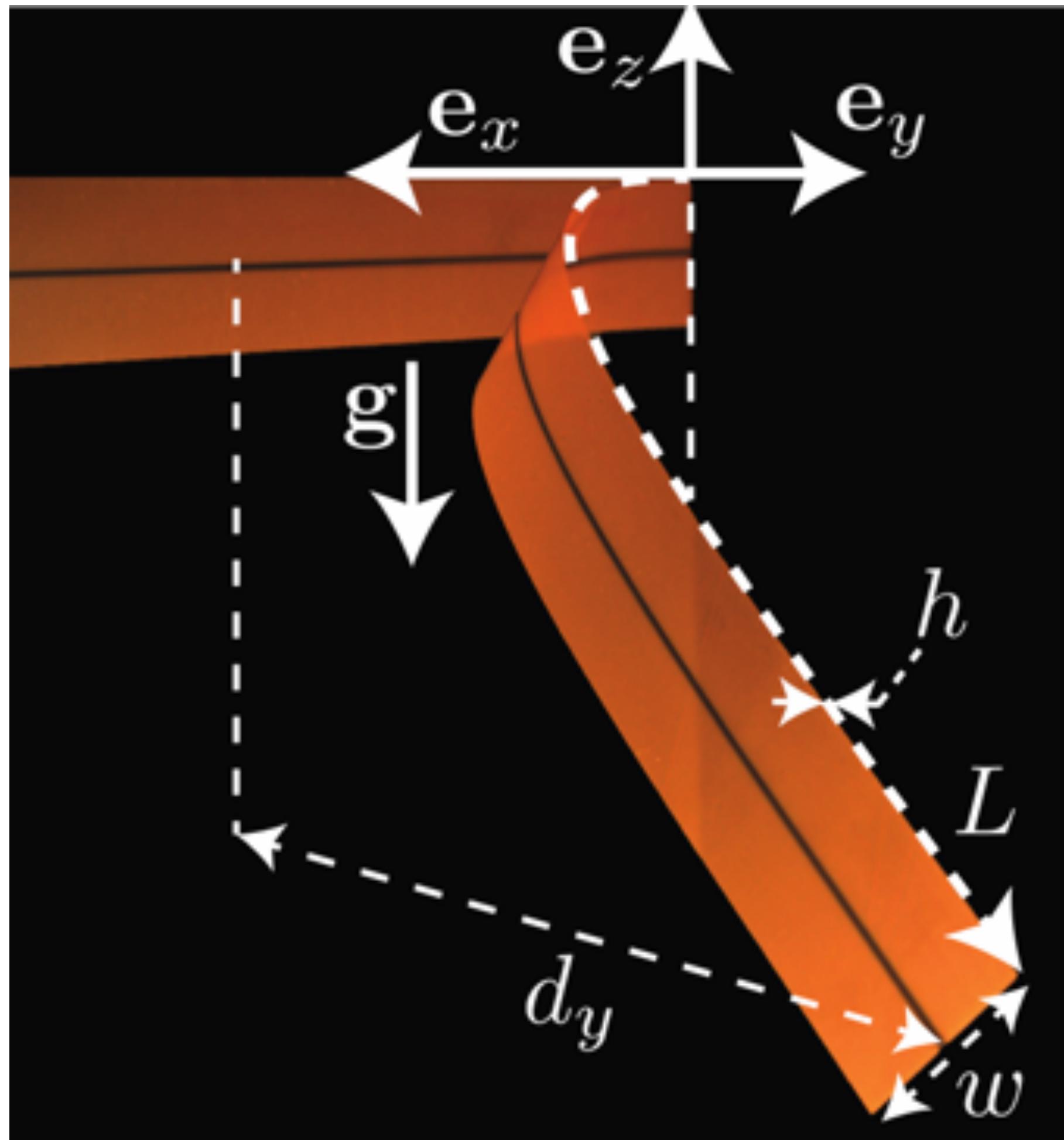


Lateral Buckling



Stick-Slip

Lateral-Buckling test



Stretching rigidity
Poisson's ratio

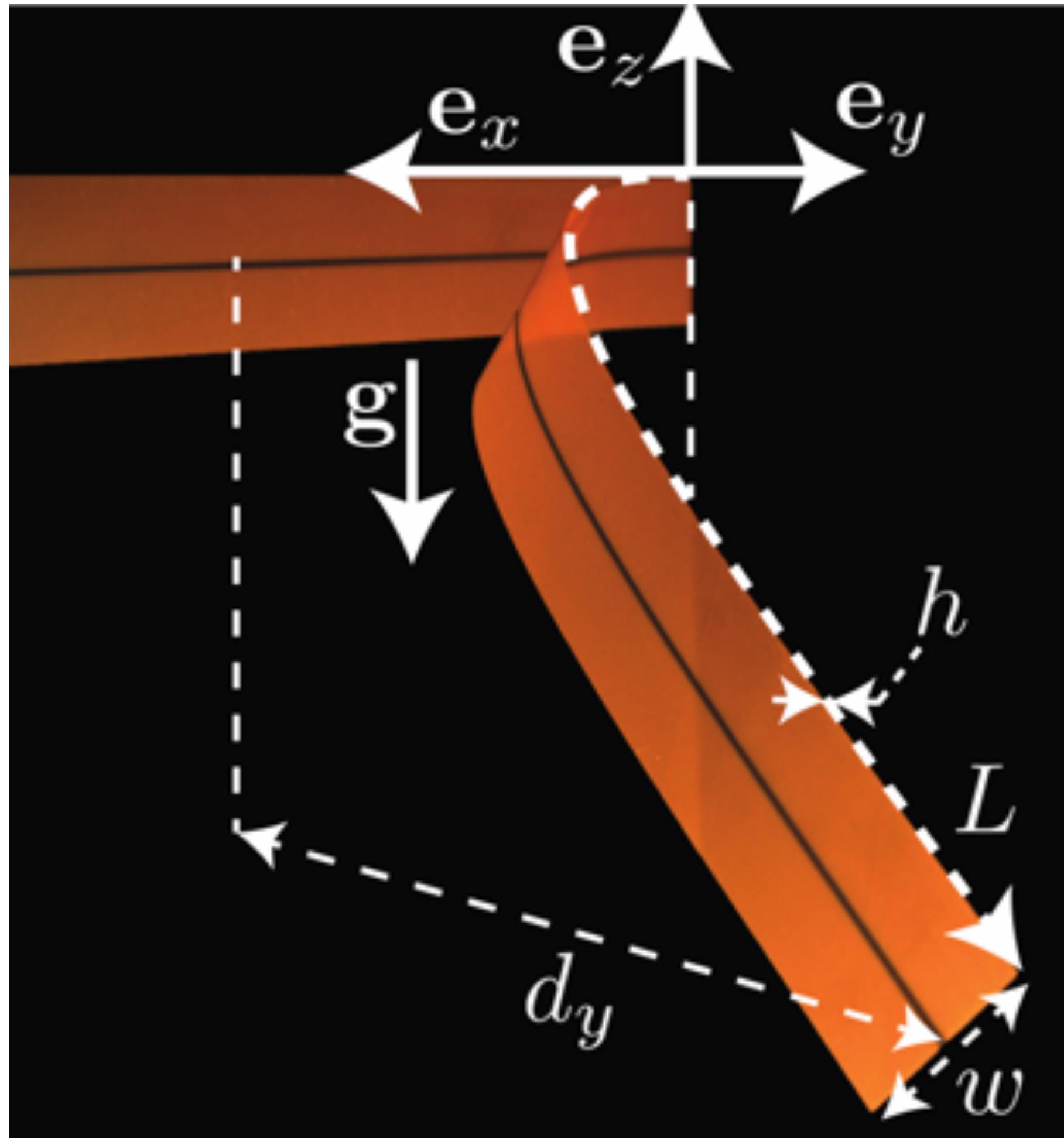
$$A = E h = 12 (1 - \nu^2) D h^2$$
$$\nu = 0.35$$

Classical failure mode in Civil Engineering

Bending rigidity D
Length L
Weight Mg
Thickness h
Width w

$$\Gamma^* = \frac{Mg}{Dw/L^2} \text{ and } \frac{w}{L} \text{ and } \frac{h}{L}$$

Lateral-Buckling test



Stretching rigidity
Poisson's ratio

$$A = E h = 12(1 - \nu^2) D h^2$$
$$\nu = 0.35$$

Classical failure mode in Civil Engineering

Bending rigidity
Length
Weight
Thickness
Width

D
 L
 Mg
 h
 w

limit $h \rightarrow 0$

$$\Gamma^* = \frac{Mg}{Dw/L^2} \text{ and } \frac{w}{L}$$

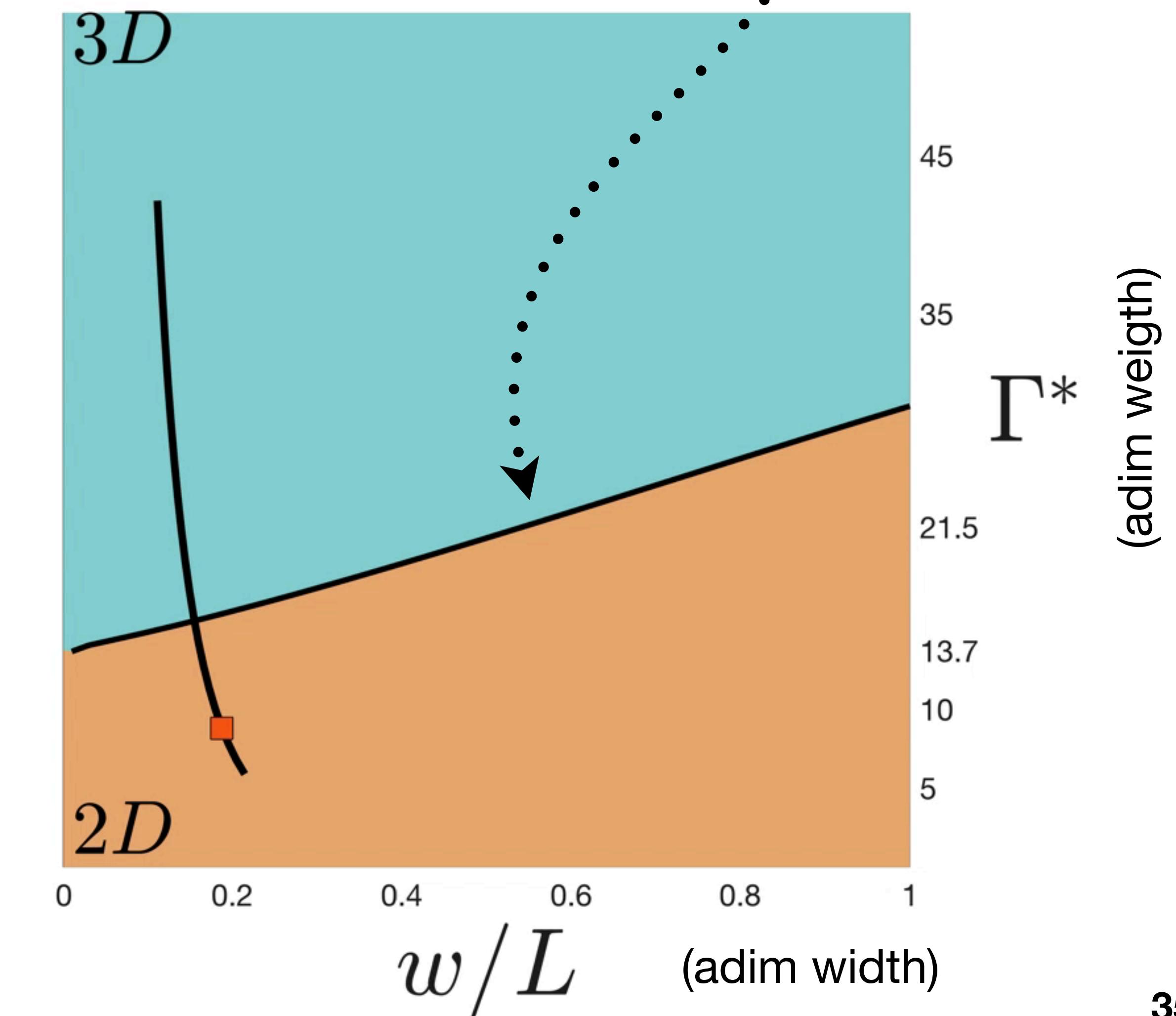
and $\frac{h}{L}$

~~$\frac{h}{L}$~~

Lateral-Buckling test experimental validation

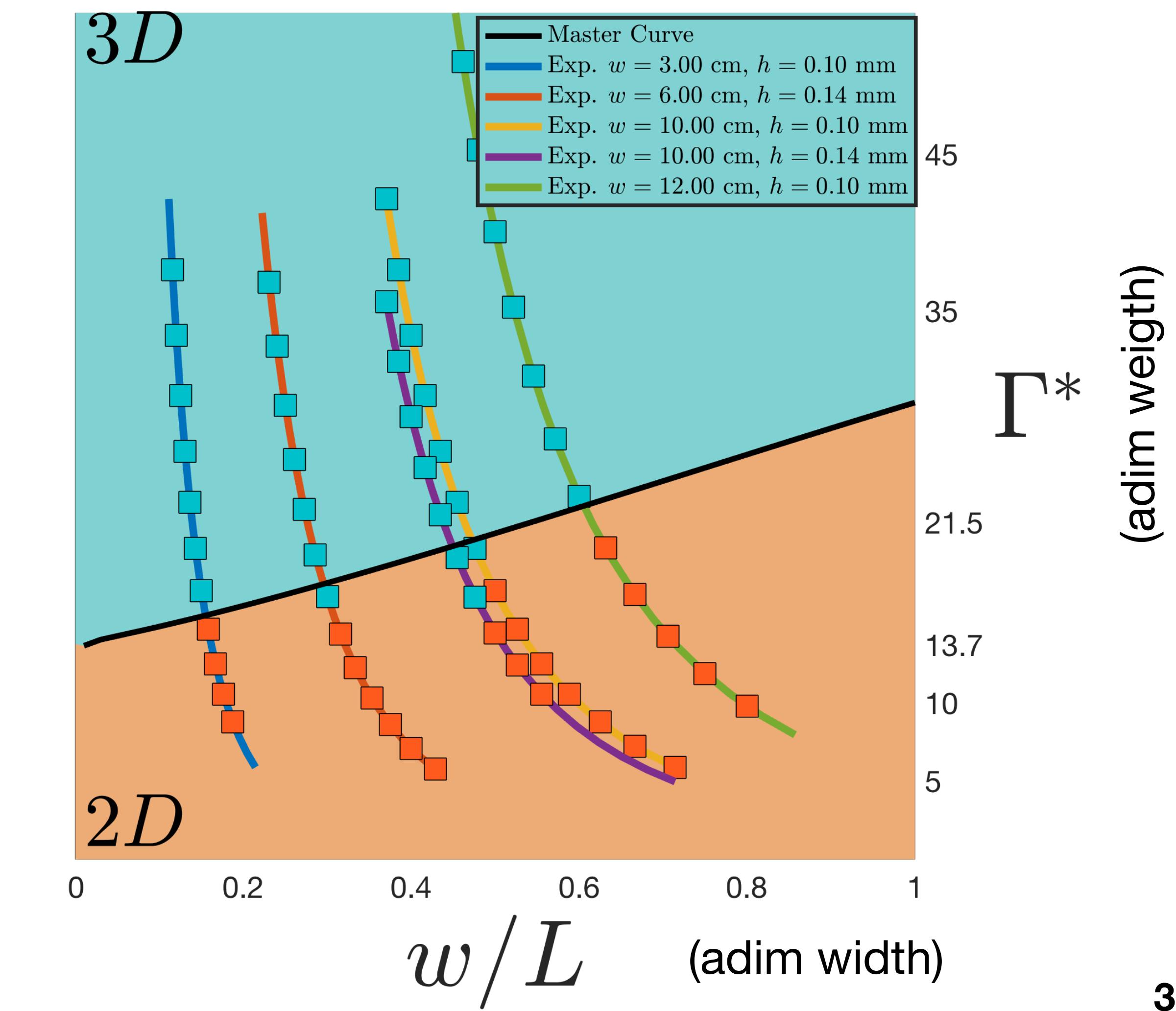
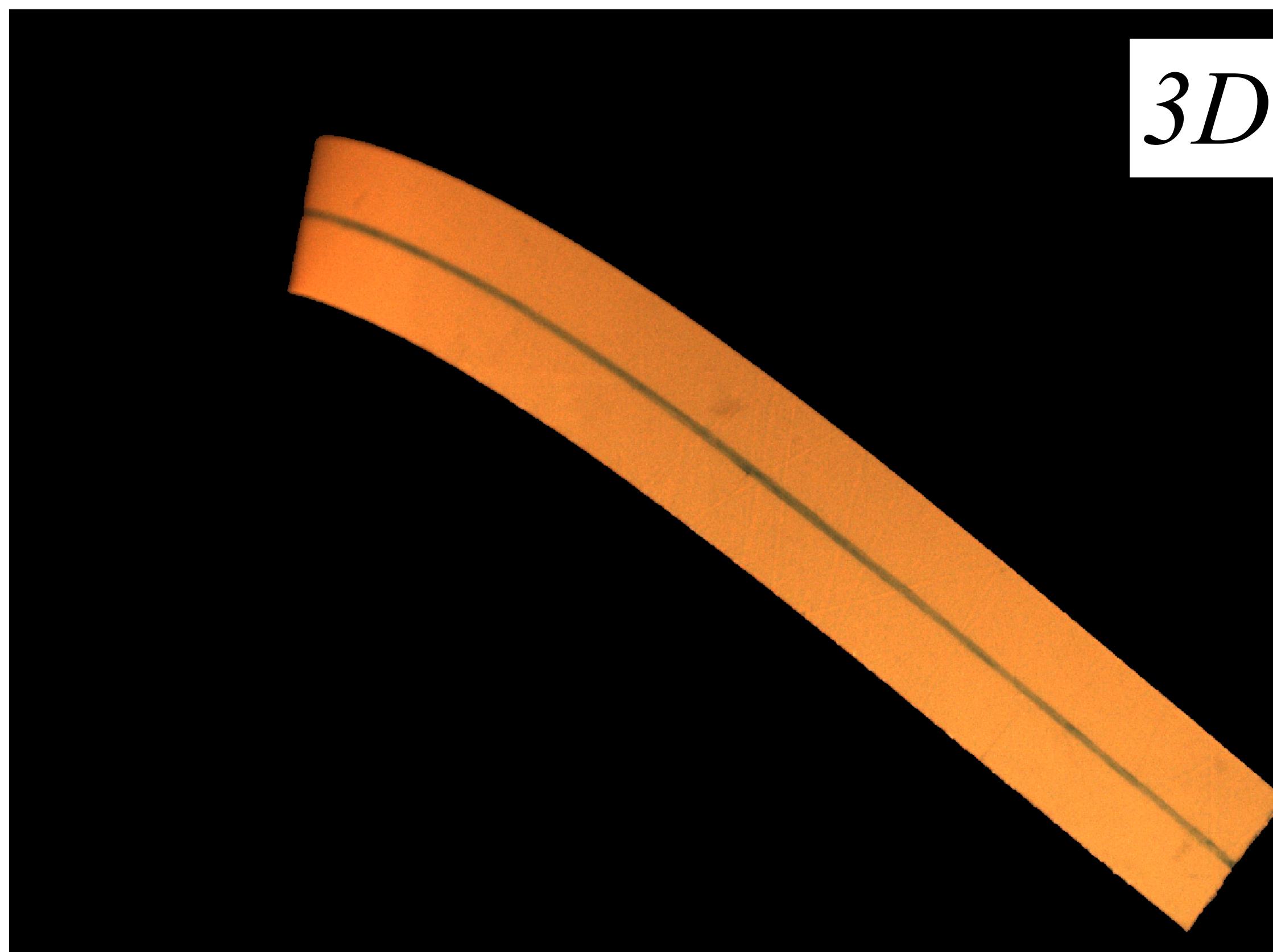
Abaqus eigenvalue analysis

experiment: increase L



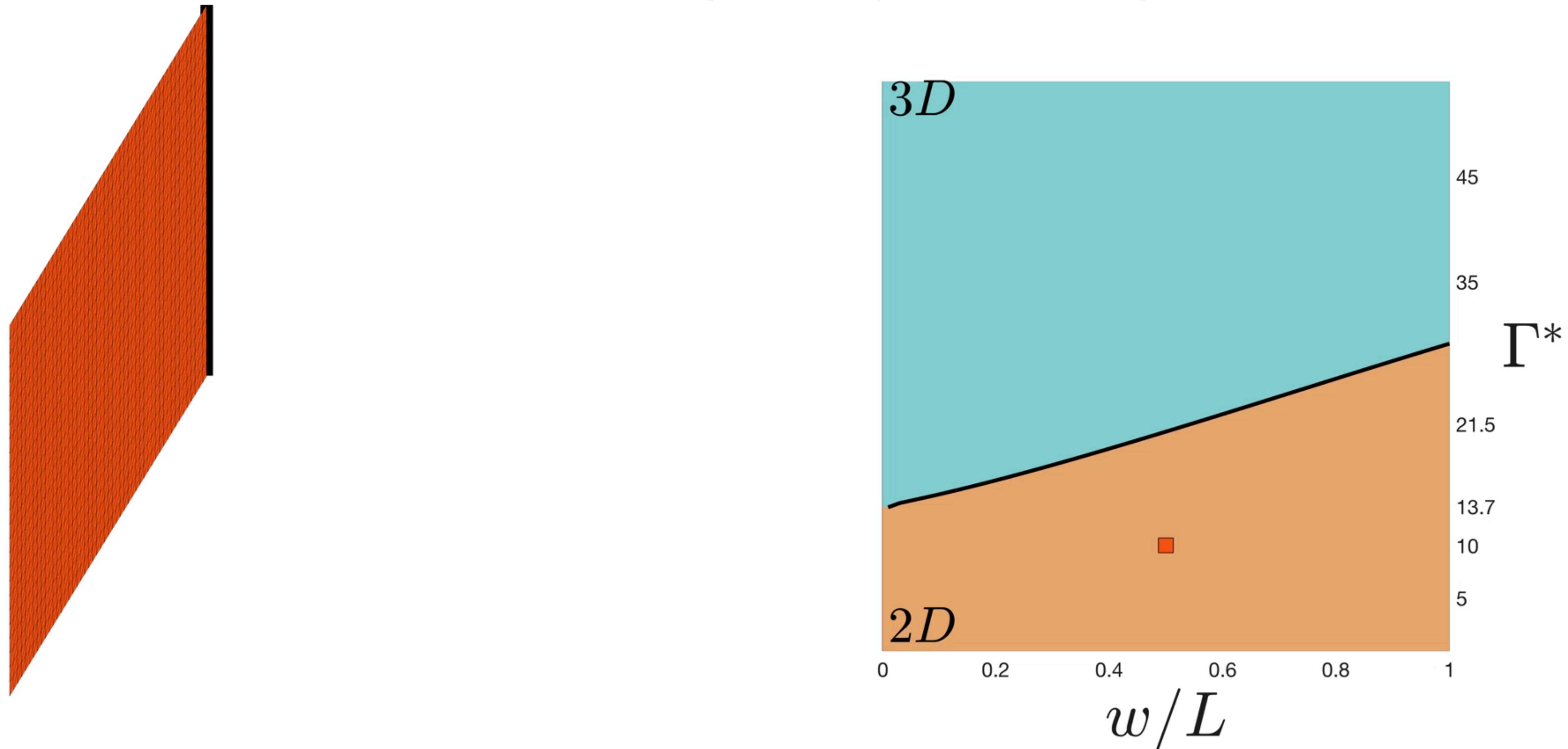
Lateral-Buckling test experimental validation

experiment: increase L



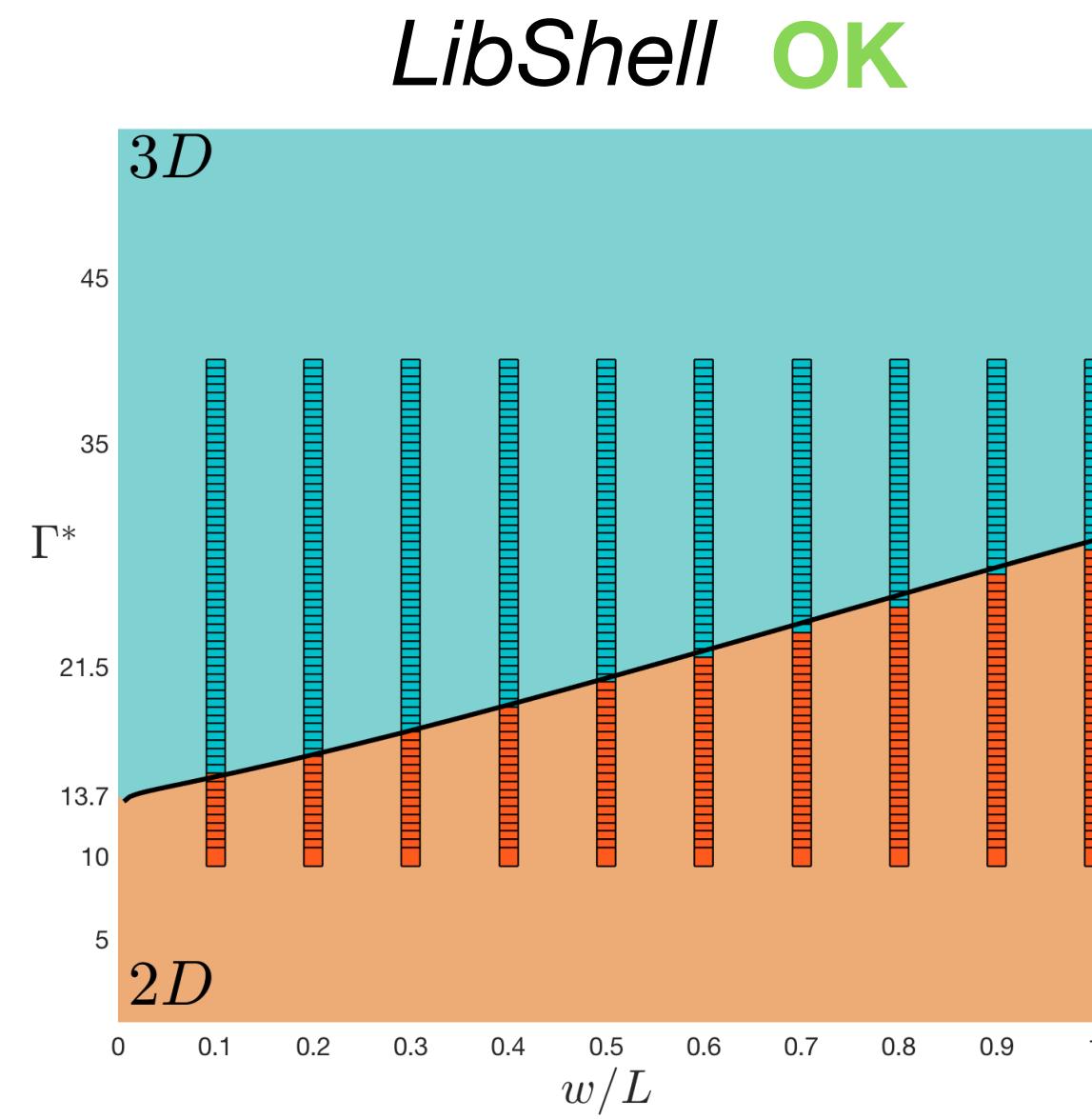
Lateral Buckling test: numerics

FEniCS Shell [Hale et al, Computers & Structures 2018]

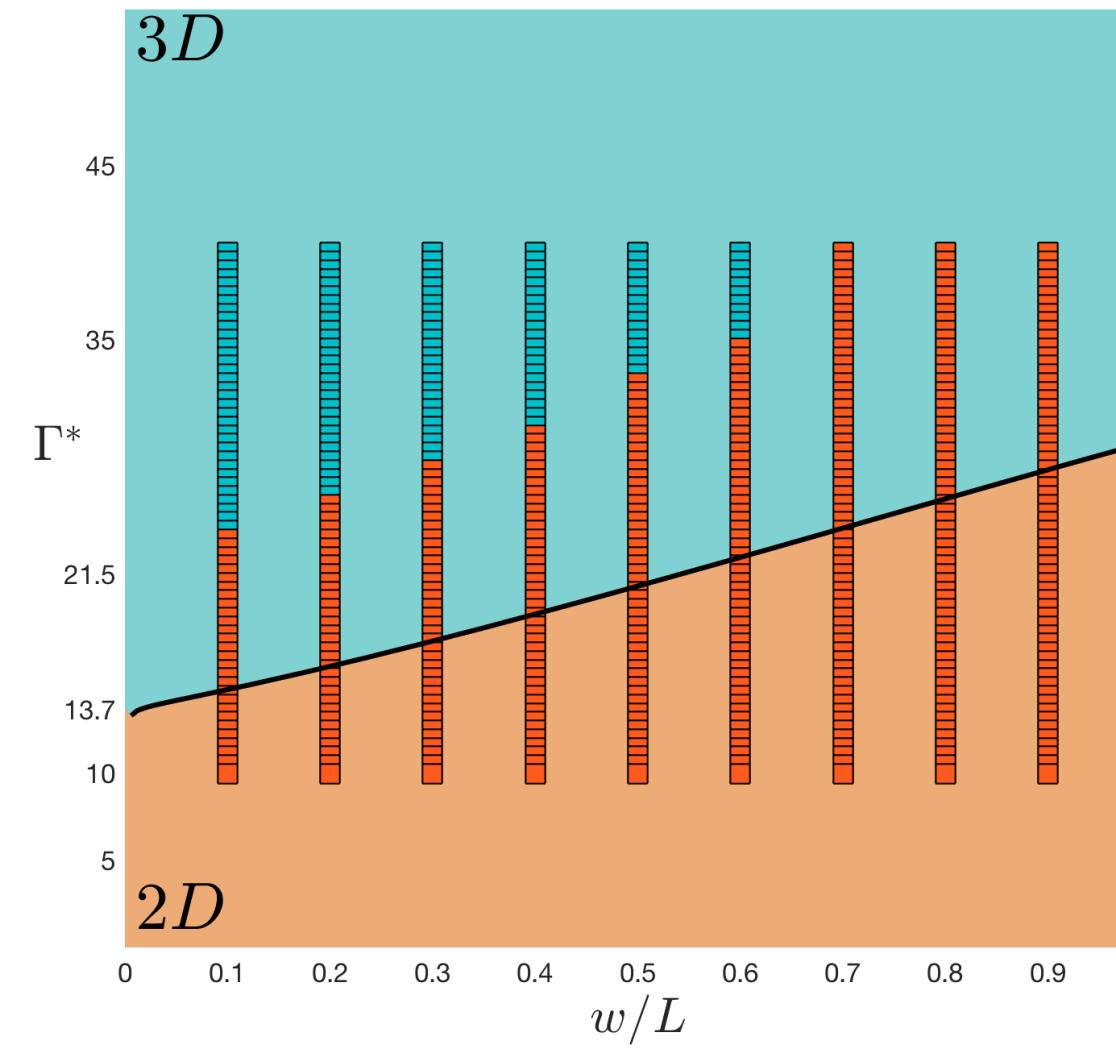


Lateral Buckling test

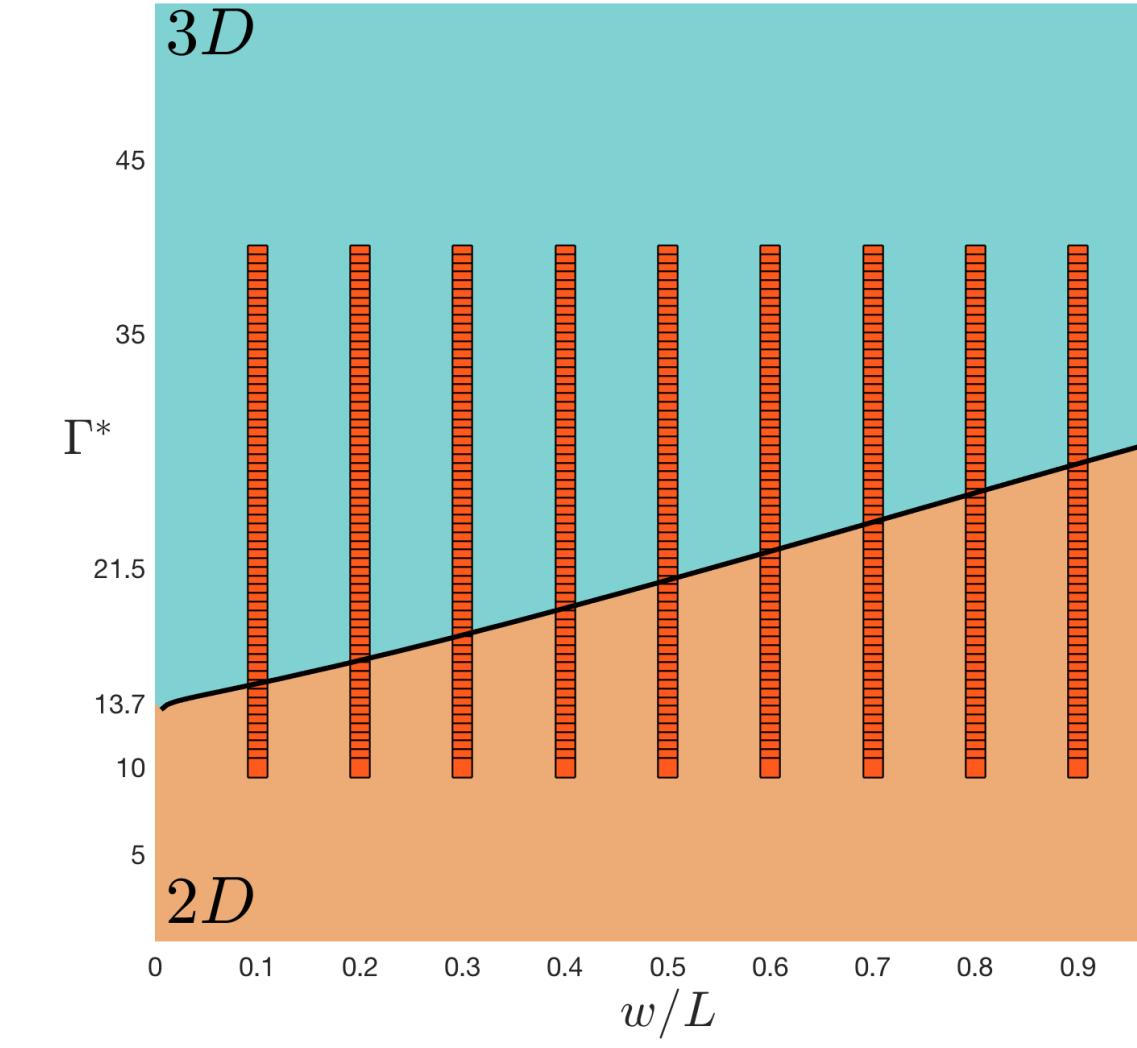
Computer
Graphics
codes



Super-Ribbon **KO**



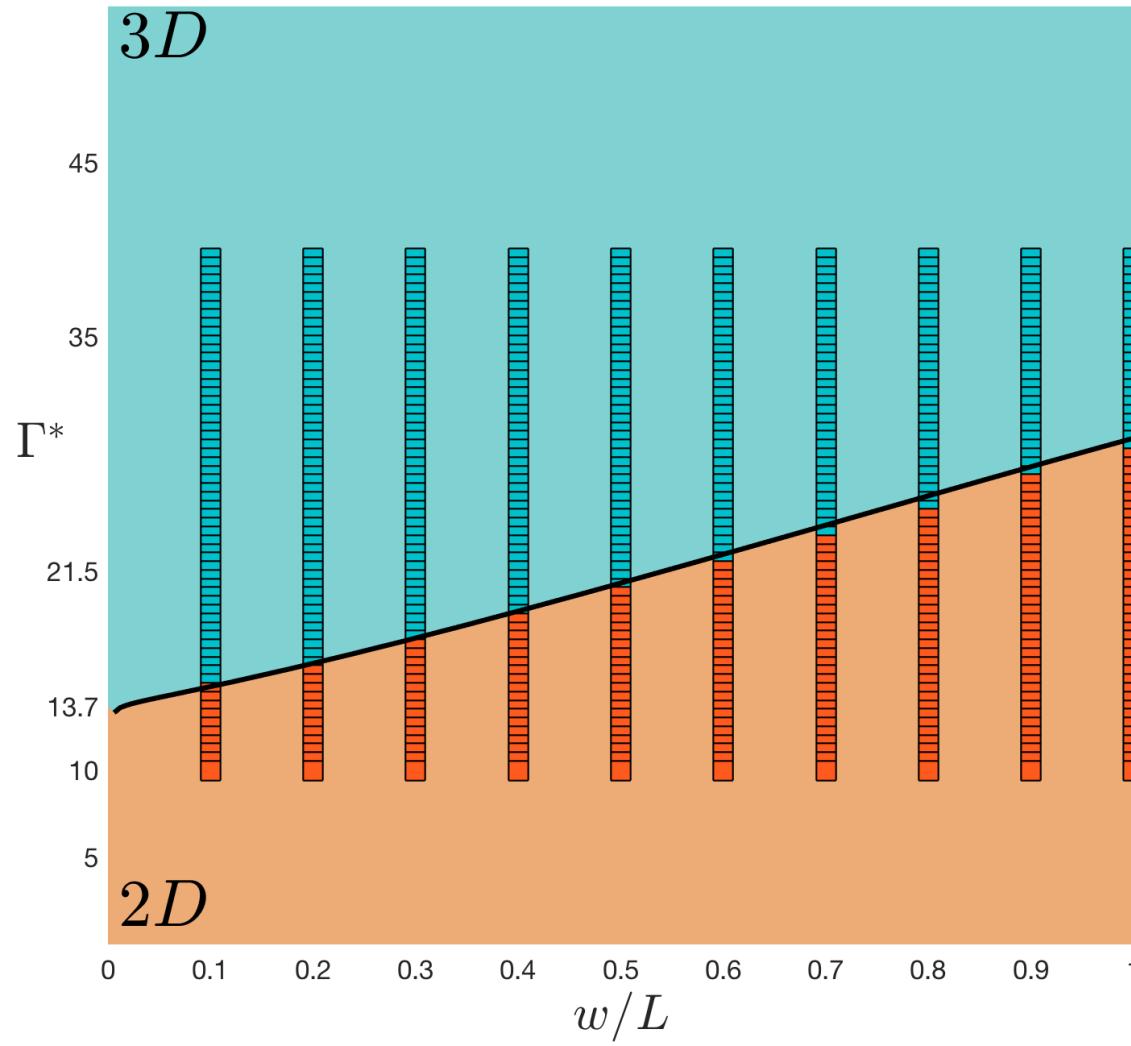
Discrete Shell **KO**



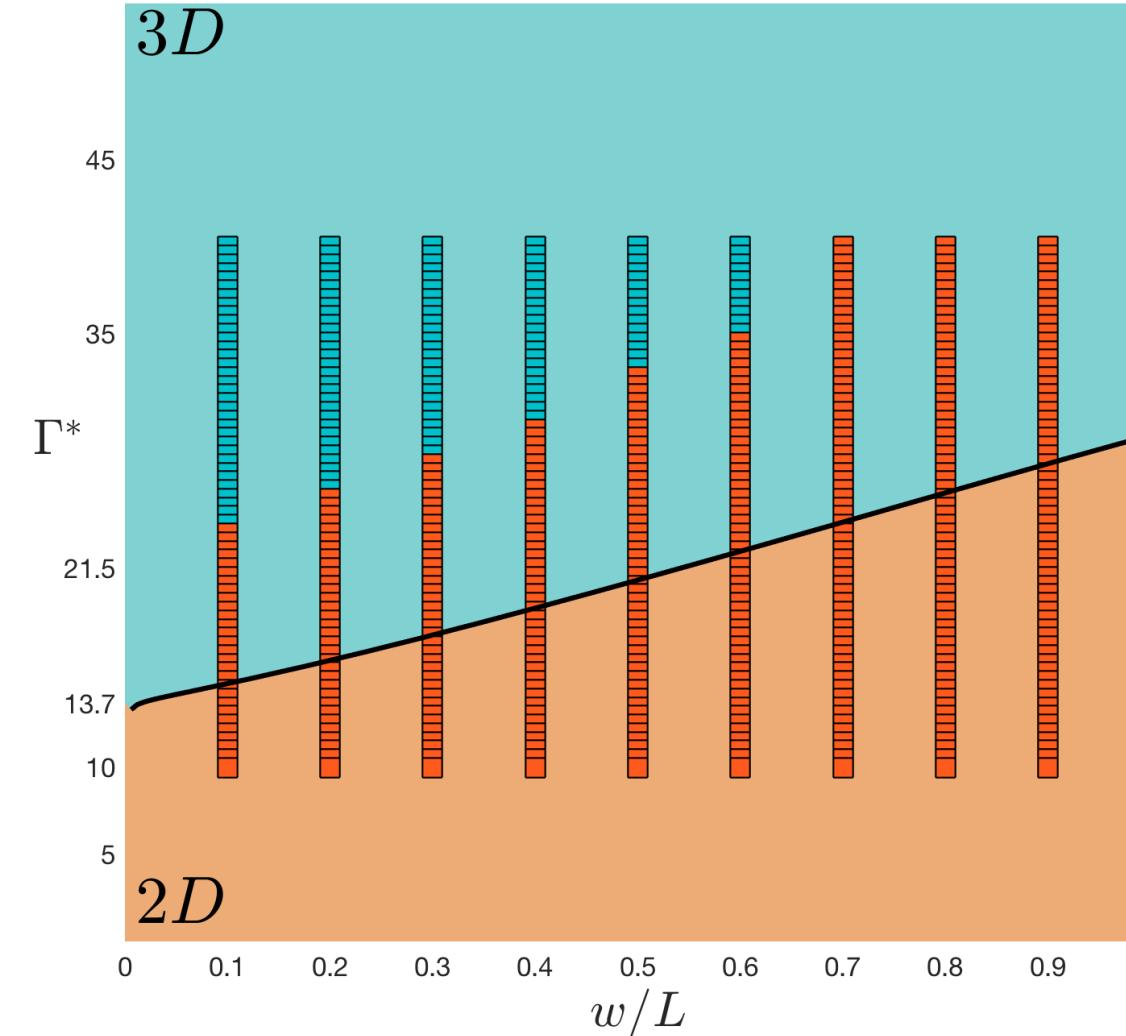
Lateral Buckling test

Computer
Graphics
codes

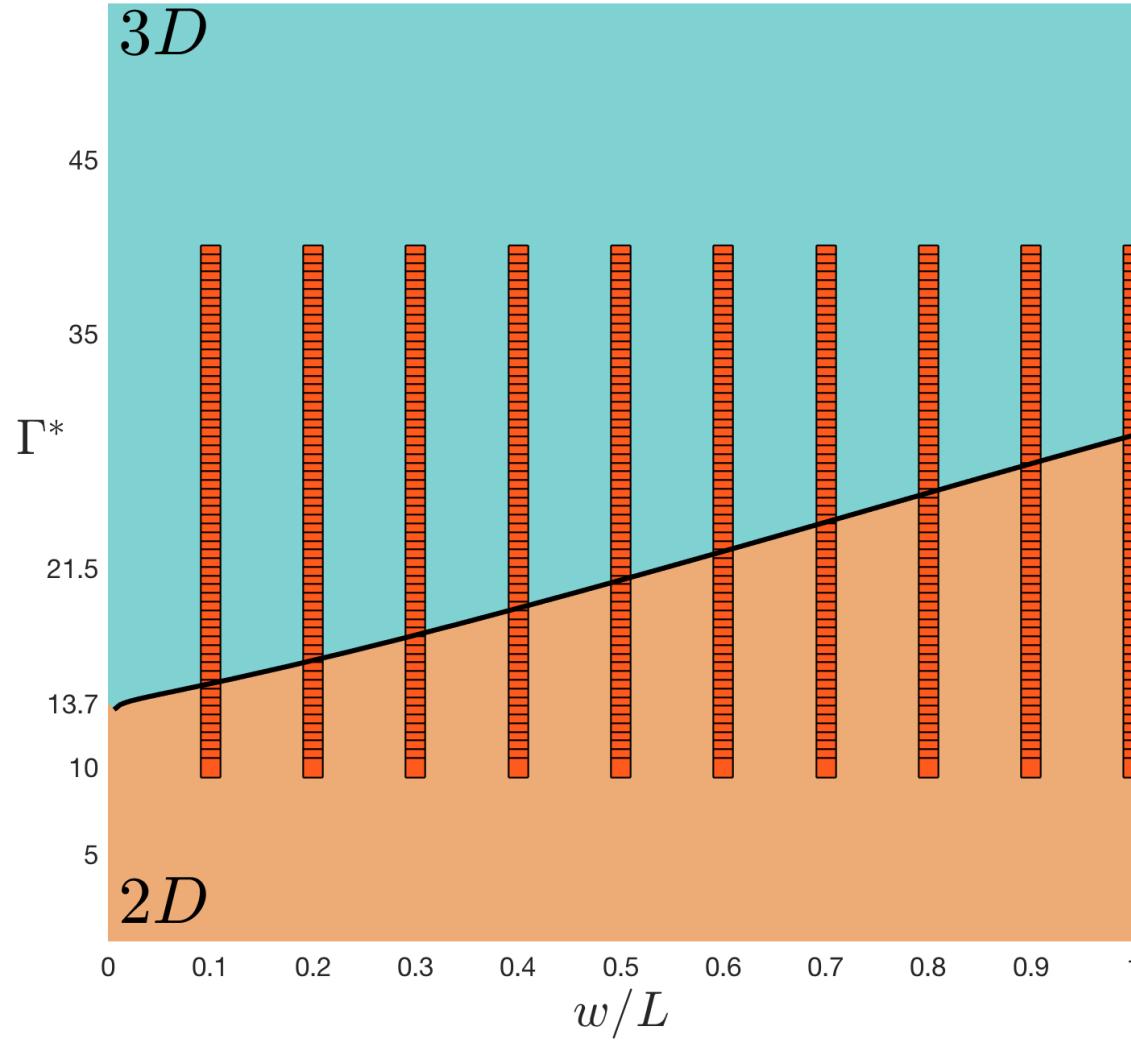
LibShell OK



Super-Ribbon KO

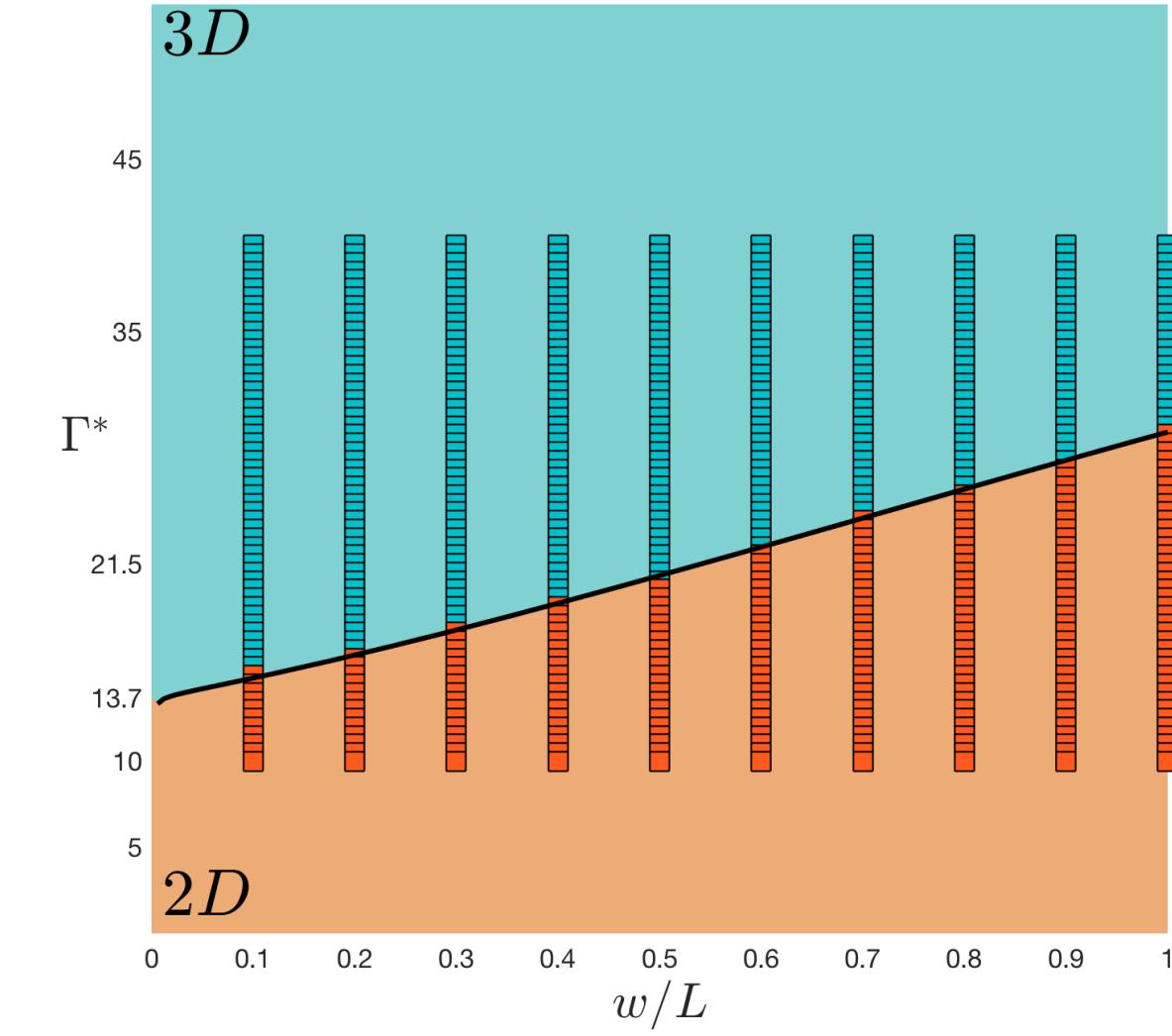


Discrete Shell KO

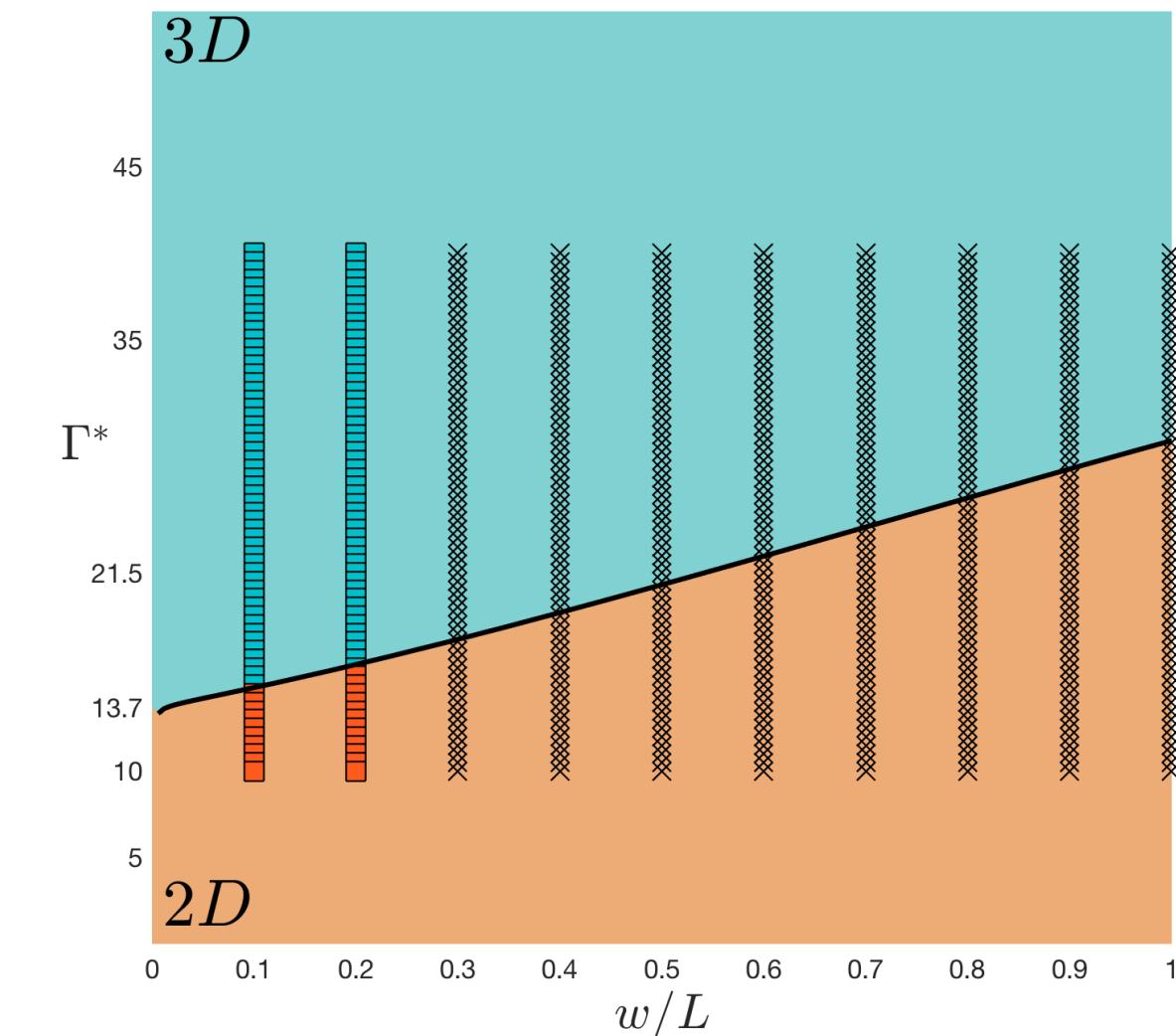


Solid Mechanics codes

FeniCS Shell OK



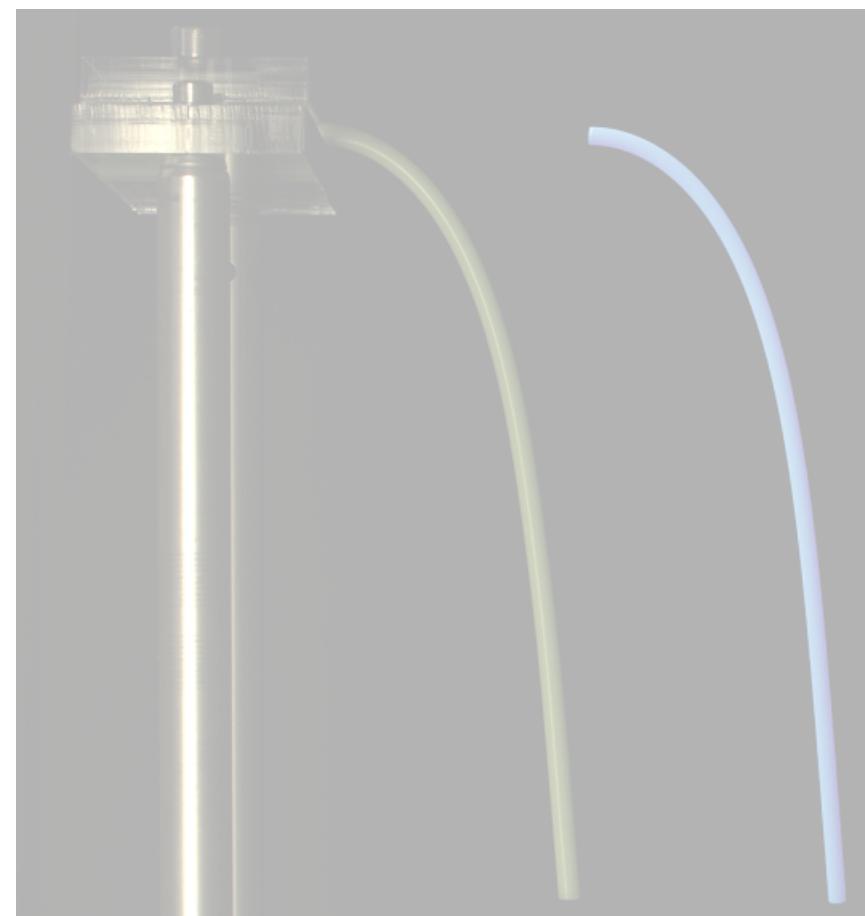
©Abaqus KO



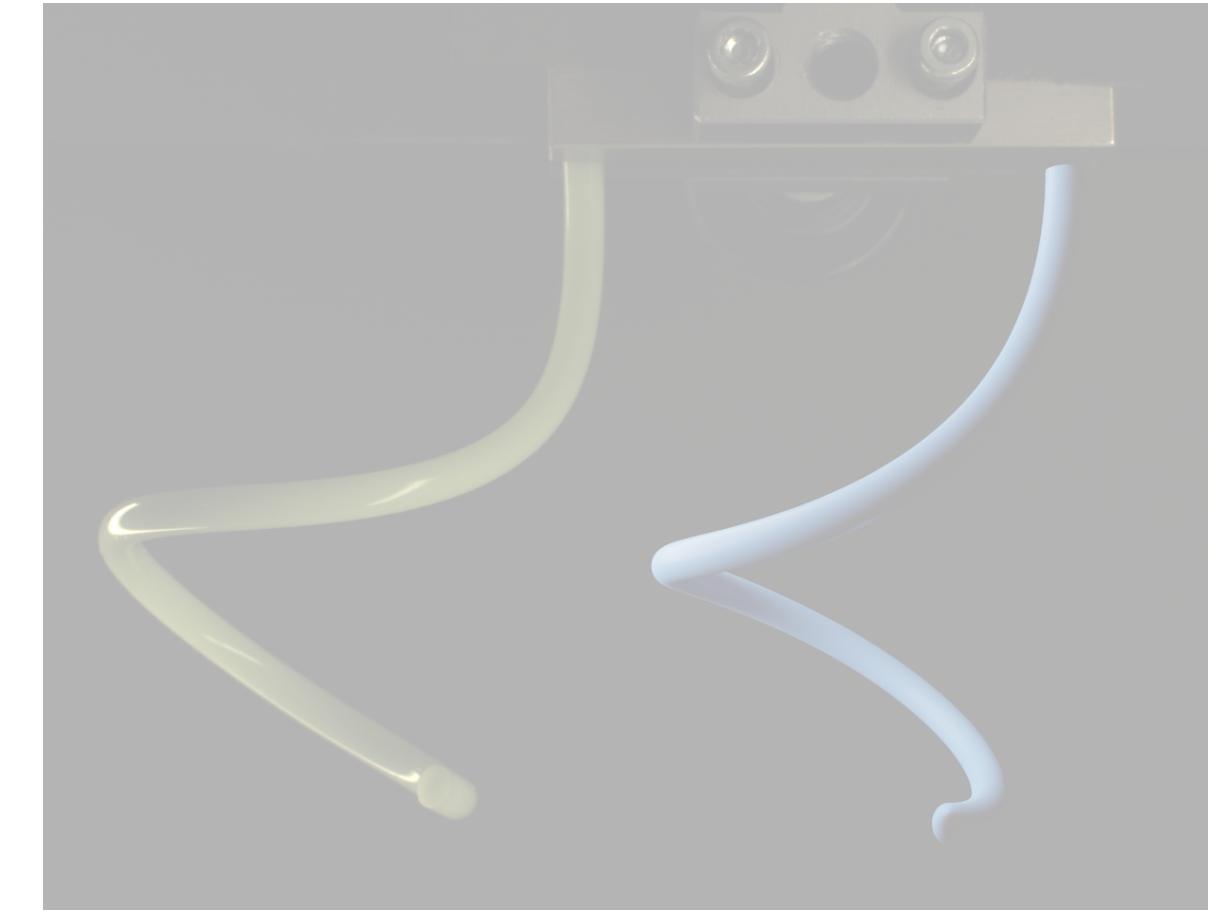
Lateral Buckling test

| Tested Code | Cantilever | Bend-Twist | Lateral Buckling | Stick-Slip |
|--|----------------------------|---------------|----------------------------|---------------------------------------|
| Rod | | | | |
| DISCRETE ELASTIC ROD [Bergou et al. 2010] | OK (300 elts) | OK (200 elts) | - | - |
| SUPER-HELIX [Bertails et al. 2006] | OK (50 elts) | OK (30 elts) | - | - |
| SUPER-CLOTHOID [Casati and Bertails-Descoubes 2013] | OK (20 elts) | OK (25 elts) | - | - |
| Ribbon | | | | |
| SUPER-RIBBON [Charrondière et al. 2020] | OK (20 elts) | - | KO | - |
| Plate | | | | |
| LIBSHELL [Chen et al. 2018] | OK (Res 0) | - | OK (Res +) | - |
| DISCRETE SHELL (+ LIBSHELL) [Grinspun et al. 2003] | OK (Res +) | - | KO | - |
| ARCSIM [Narain et al. 2012] | KO | - | X | - |
| DISCRETE SHELL + ARCSIM (tentative fix of ARCSIM) | KO | - | X | - |
| PROJECTIVE DYNAMICS [Bouaziz et al. 2014] (fit) | KO | - | X | - |
| Contact & friction | | | | |
| VISCOUS FRICTION (+ SUPER-HELIX 2D) | - | - | - | KO |
| So-BOGUS [Daviet et al. 2011] (+ SUPER-HELIX 2D) | - | - | - | OK ($dt=0.5$ ms, tol = 10^{-13} N) |
| ARGUS (\approx ARCSIM + So-BOGUS) [Li et al. 2018] | - | - | - | KO |
| ARGUS NON ADAPTIVE (fix of ARGUS) | - | - | - | OK ($dt=0.5$ ms, tol = 10^{-13} N) |
| BRIDSON-HARMON [Bridson et al. 2002; Harmon et al. 2008] (+ ARCSIM) | - | - | - | KO |
| PROJECTIVE FRICTION [Ly et al. 2020] | - | - | - | KO |
| Reference codes in Mechanical Engineering | | | | |
| FENICSHELL [Hale et al. 2018] | OK (Res 0, $P_{2,3}$ elts) | - | OK (Res 0, $P_{2,3}$ elts) | - |
| ©ABAQUS | OK (200 P_2 elts) | KO | KO | OK ($dt=9\ \mu s$) |

Measurement protocols



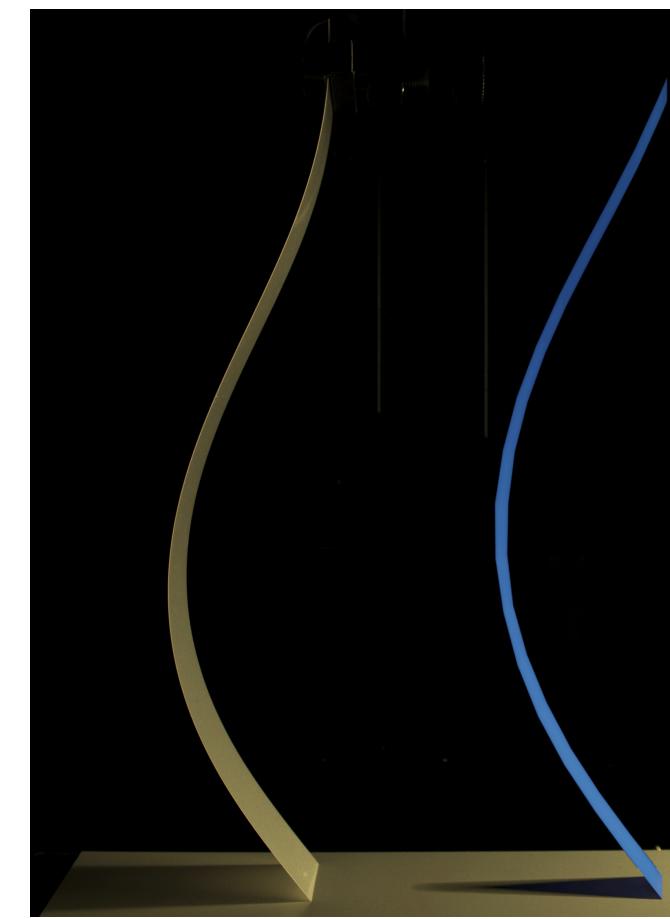
Cantilever



Bend-Twist



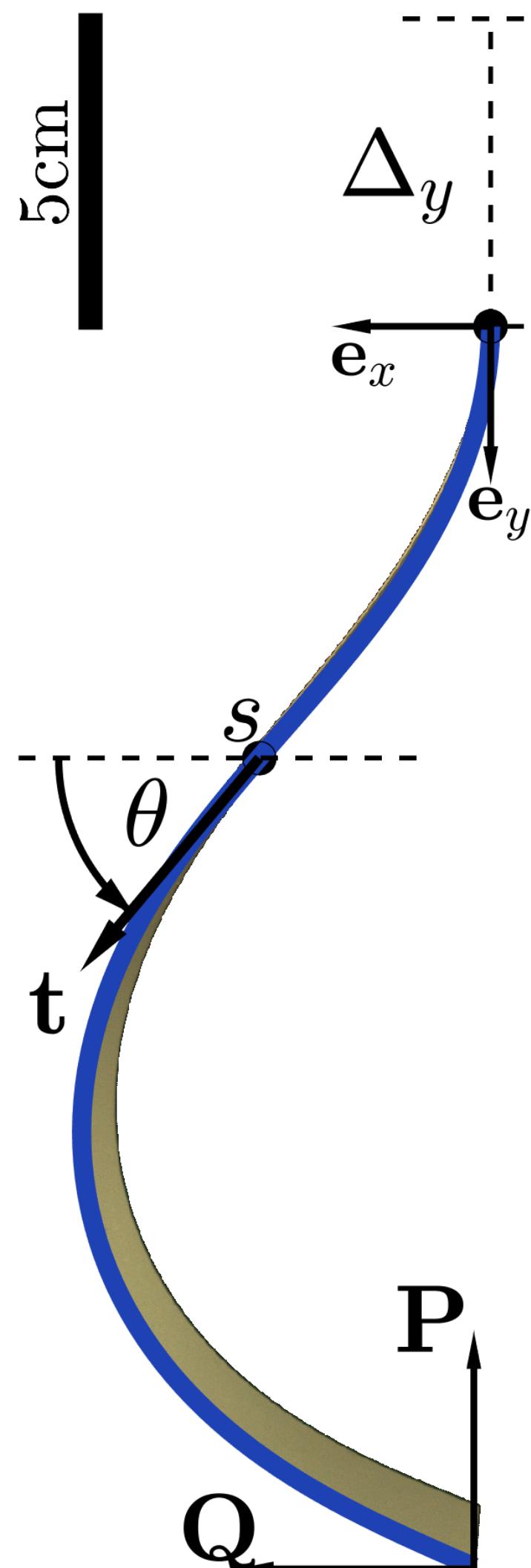
Lateral Buckling



Stick-Slip

Measurement protocols

Stick-Slip test



Experiment Inspired by Sano et al..

Gravity negligible

Normal Force:

P

Tangential Force:

Q

Length:

L

Vertical displacement:

Δ_y

Friction coefficient:

μ



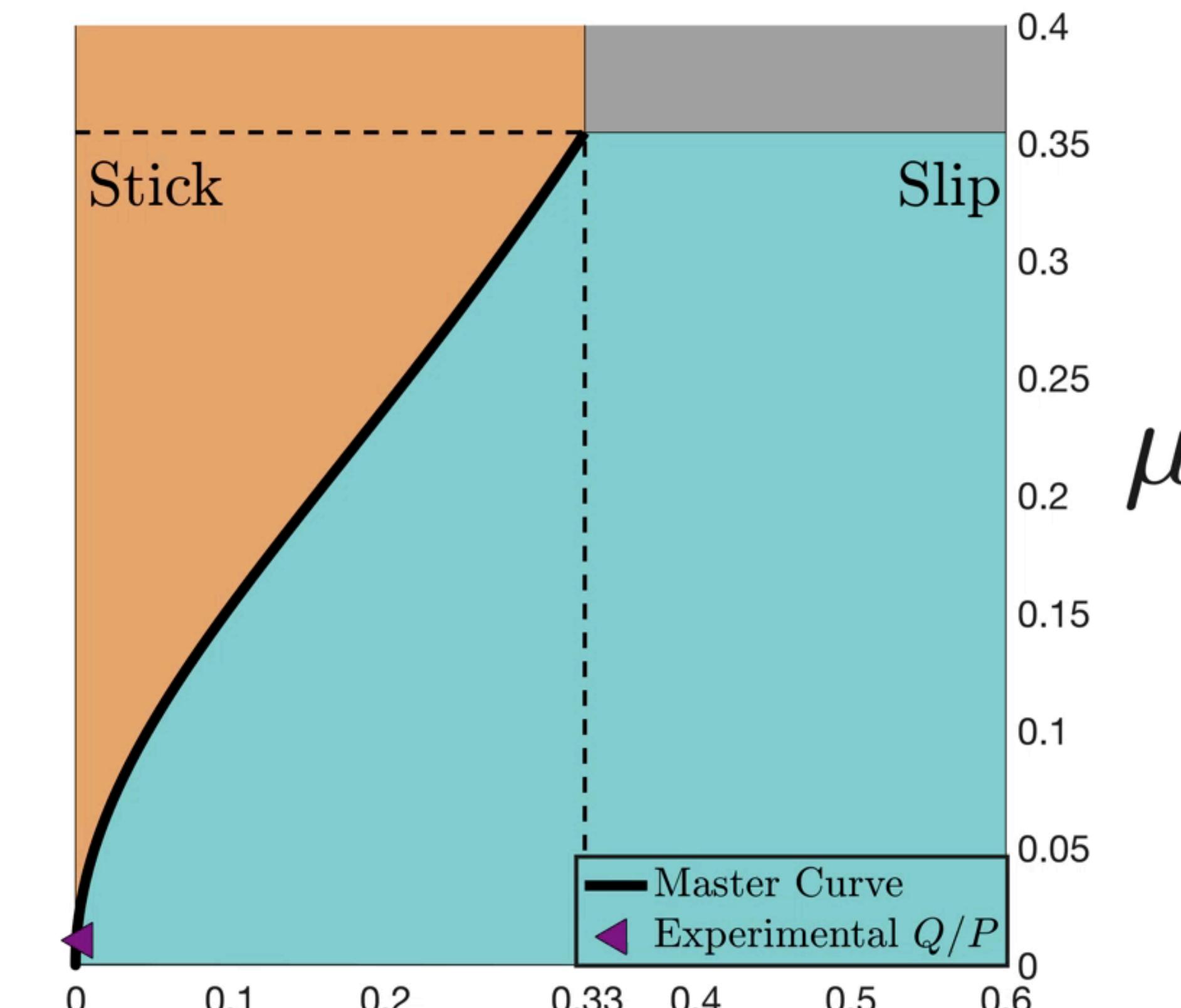
Force ratio = $\frac{Q}{P}$ and Vertical strain $\epsilon_y = \frac{\Delta_y}{L}$

Measurement protocols

Stick-Slip test – experimental validation



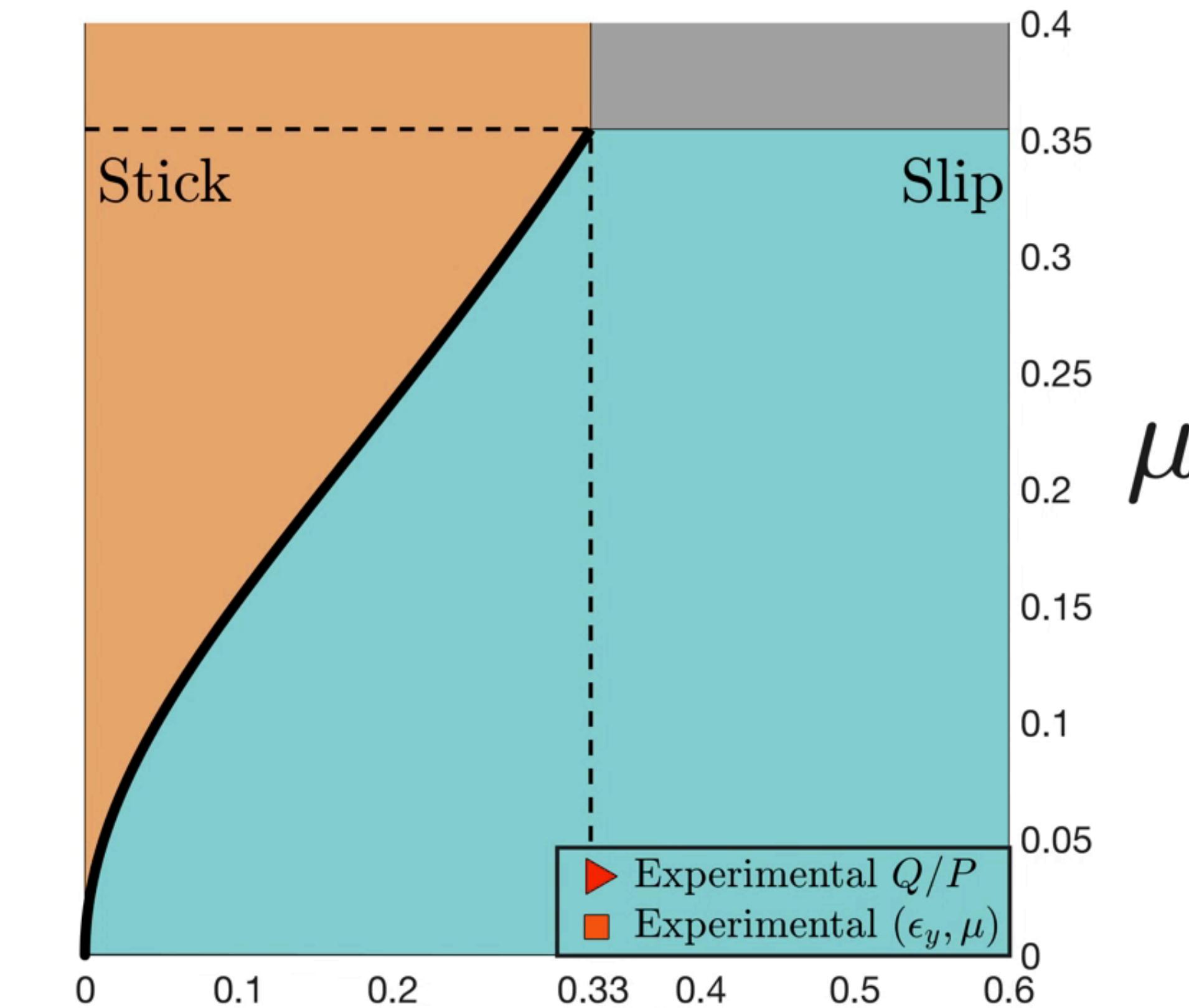
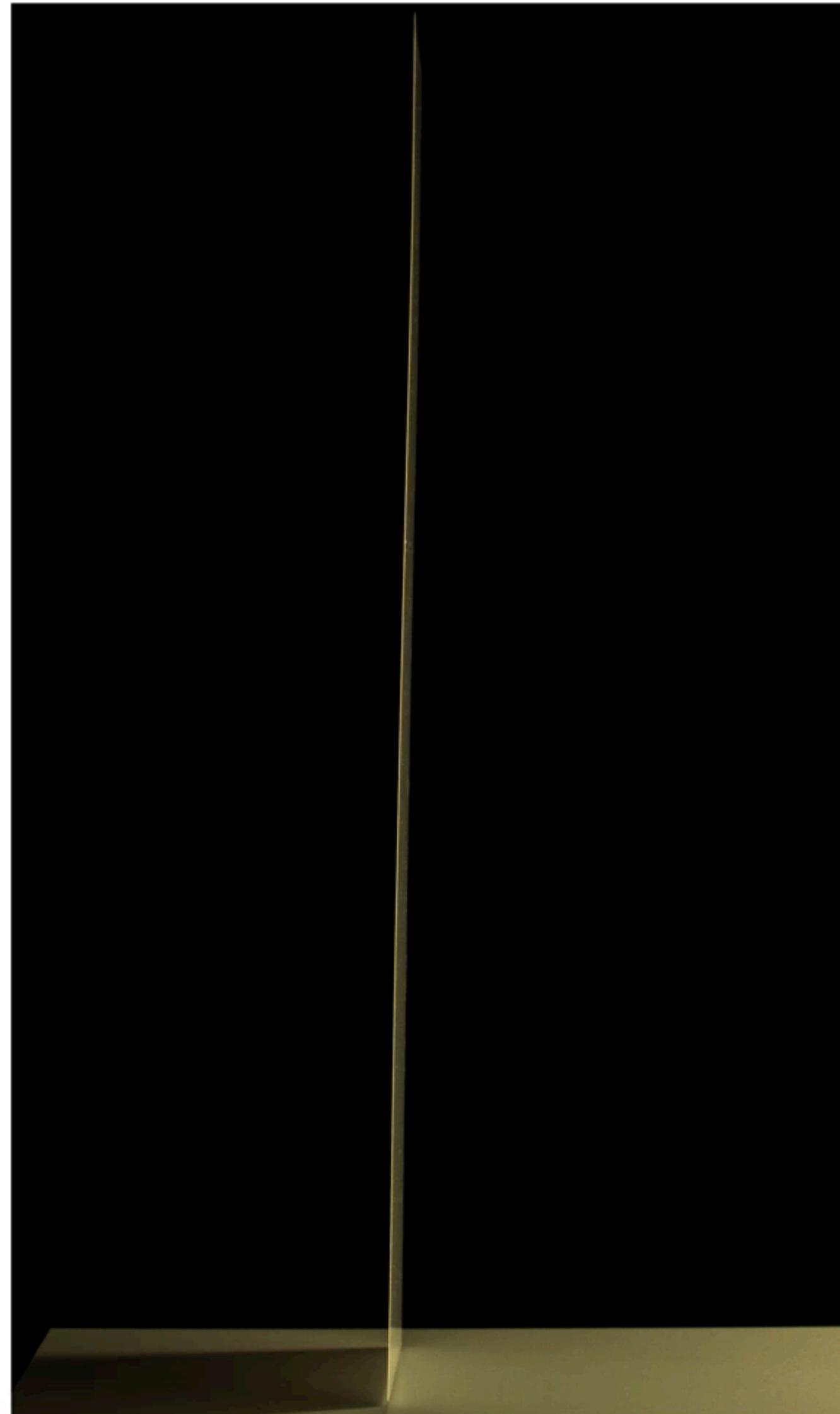
Extended from Sano et al. 2017



$$\epsilon_y = \frac{\Delta_y}{L}$$

Measurement protocols

Stick-Slip test – experimental validation



$$\epsilon_y = \frac{\Delta y}{L}$$

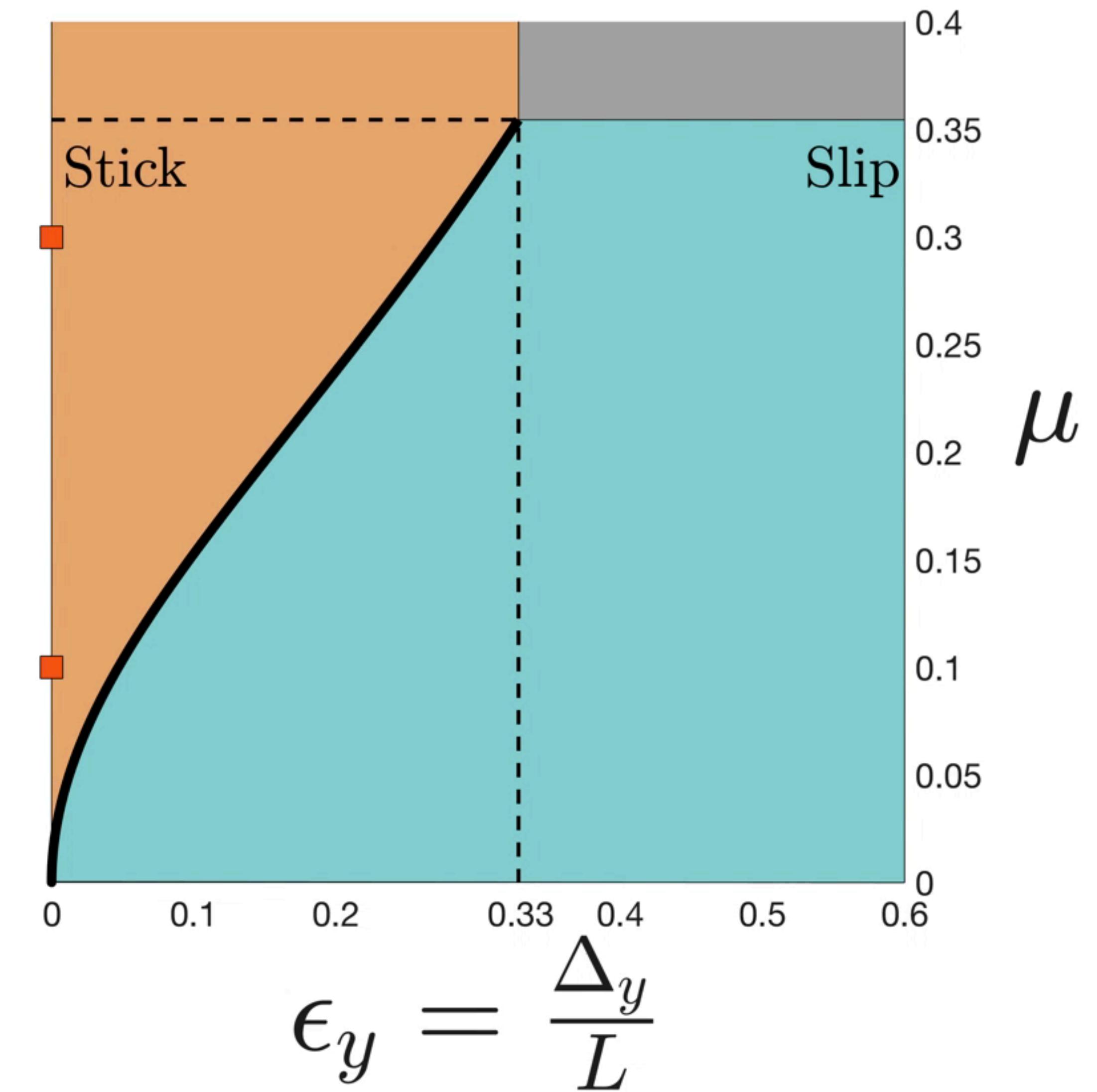
Results

Stick-slip test

| Tested Code | Cantilever | Bend-Twist | Lateral Buckling | Stick-Slip |
|--|----------------------------|---------------|----------------------------|---------------------------------------|
| Rod | | | | |
| DISCRETE ELASTIC ROD [Bergou et al. 2010] | OK (300 elts) | OK (200 elts) | - | - |
| SUPER-HELIX [Bertails et al. 2006] | OK (50 elts) | OK (30 elts) | - | - |
| SUPER-CLOTHOID [Casati and Bertails-Descoubes 2013] | OK (20 elts) | OK (25 elts) | - | - |
| Ribbon | | | | |
| SUPER-RIBBON [Charrondière et al. 2020] | OK (20 elts) | - | KO | - |
| Plate | | | | |
| LIBSHELL [Chen et al. 2018] | OK (Res 0) | - | OK (Res +) | - |
| DISCRETE SHELL (+ LIBSHELL) [Grinspun et al. 2003] | OK (Res +) | - | KO | - |
| ARCSIM [Narain et al. 2012] | KO | - | X | - |
| DISCRETE SHELL + ARCSIM (tentative fix of ARCSIM) | KO | - | X | - |
| PROJECTIVE DYNAMICS [Bouaziz et al. 2014] (fit) | KO | - | X | - |
| Contact & friction | | | | |
| VISCOS FRICTION (+ SUPER-HELIX 2D) | - | - | - | KO |
| So-BOGUS [Daviet et al. 2011] (+ SUPER-HELIX 2D) | - | - | - | OK ($dt=0.5$ ms, $tol = 10^{-13}$ N) |
| ARGUS (\approx ARCSIM + So-BOGUS) [Li et al. 2018] | - | - | - | KO |
| ARGUS NON ADAPTIVE (fix of ARGUS) | - | - | - | OK ($dt=0.5$ ms, $tol = 10^{-13}$ N) |
| BRIDSON-HARMON [Bridson et al. 2002; Harmon et al. 2008] (+ ARCSIM) | - | - | - | KO |
| PROJECTIVE FRICTION [Ly et al. 2020] | - | - | - | KO |
| Reference codes in Mechanical Engineering | | | | |
| FENICSHELL [Hale et al. 2018] | OK (Res 0, $P_{2,3}$ elts) | - | OK (Res 0, $P_{2,3}$ elts) | - |
| ©ABAQUS | OK (200 P_2 elts) | KO | KO | OK ($dt=9 \mu s$) |

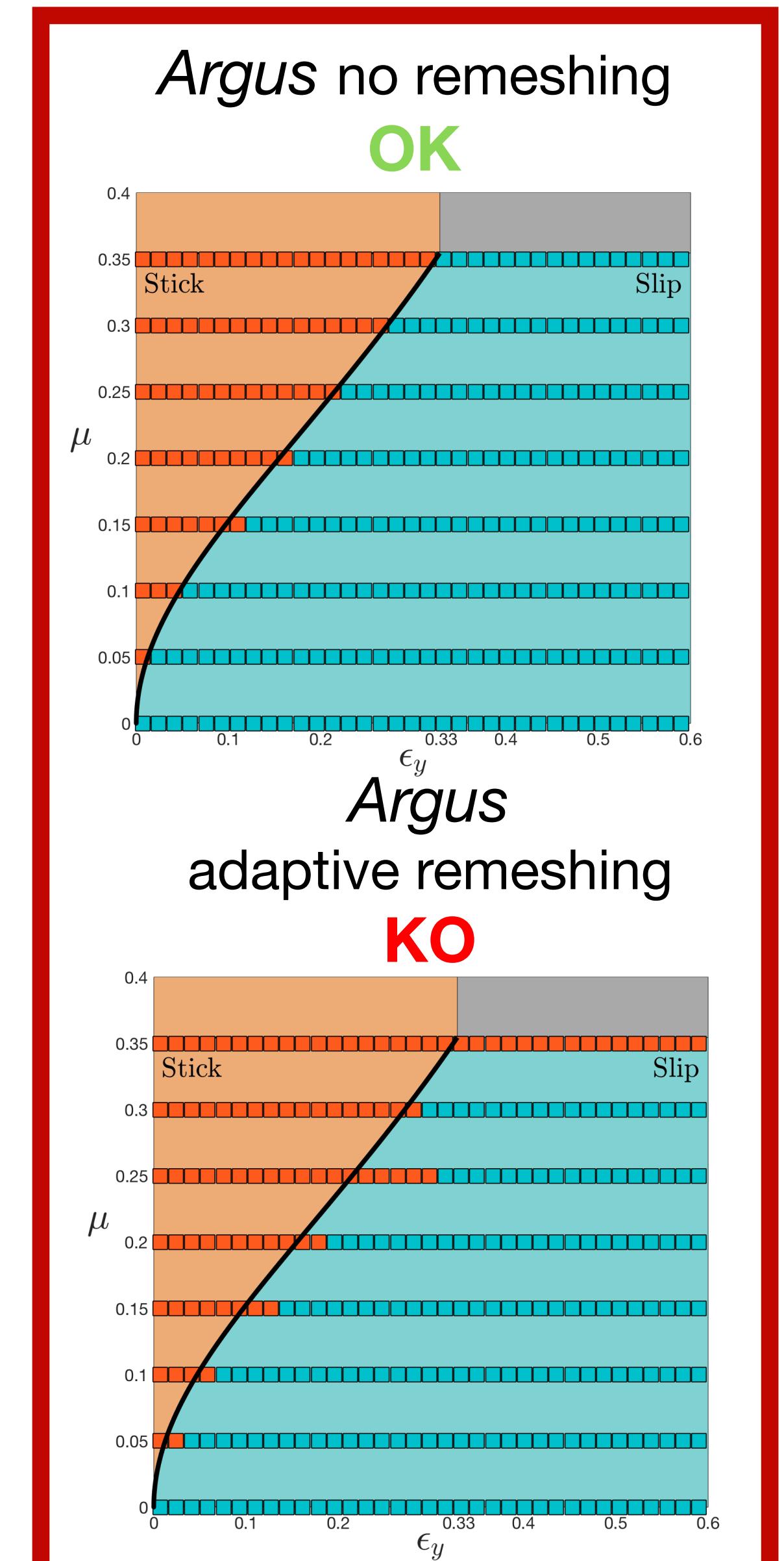
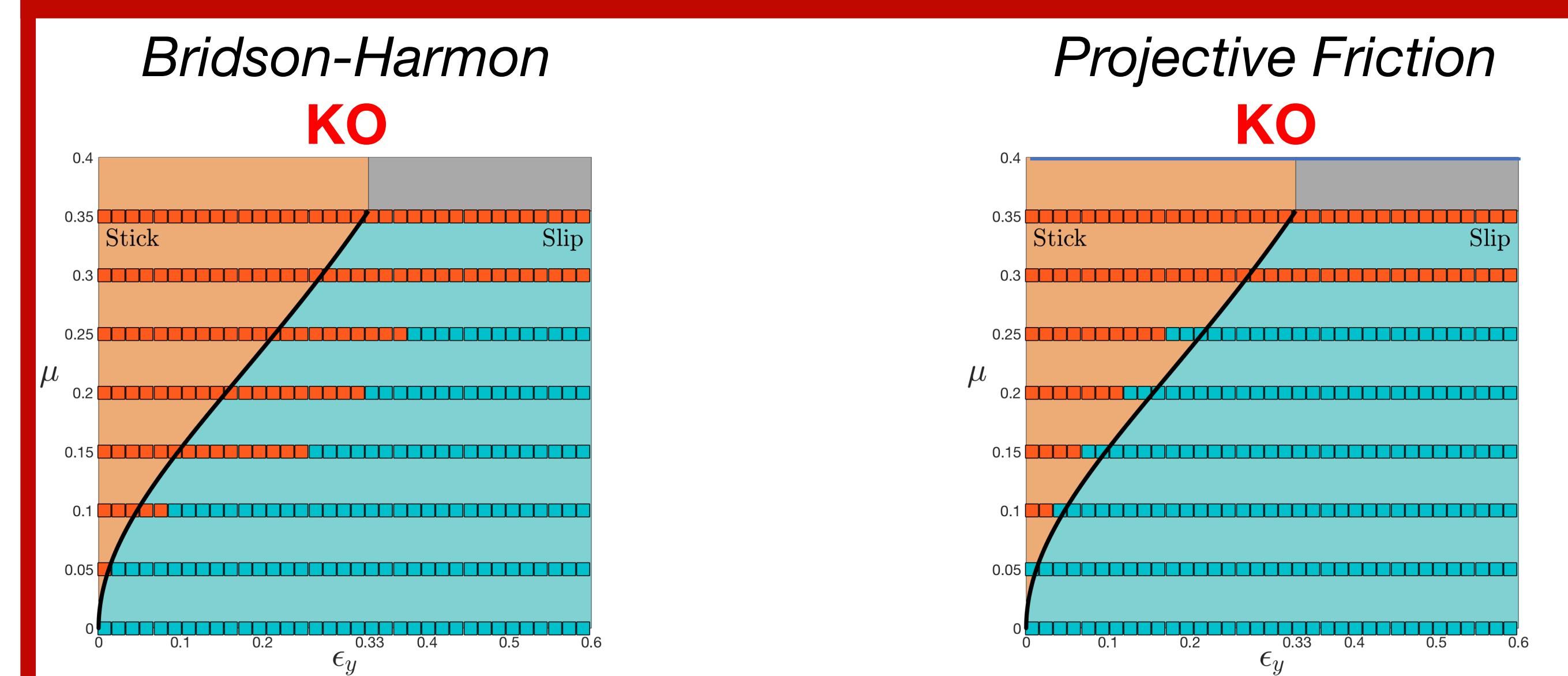
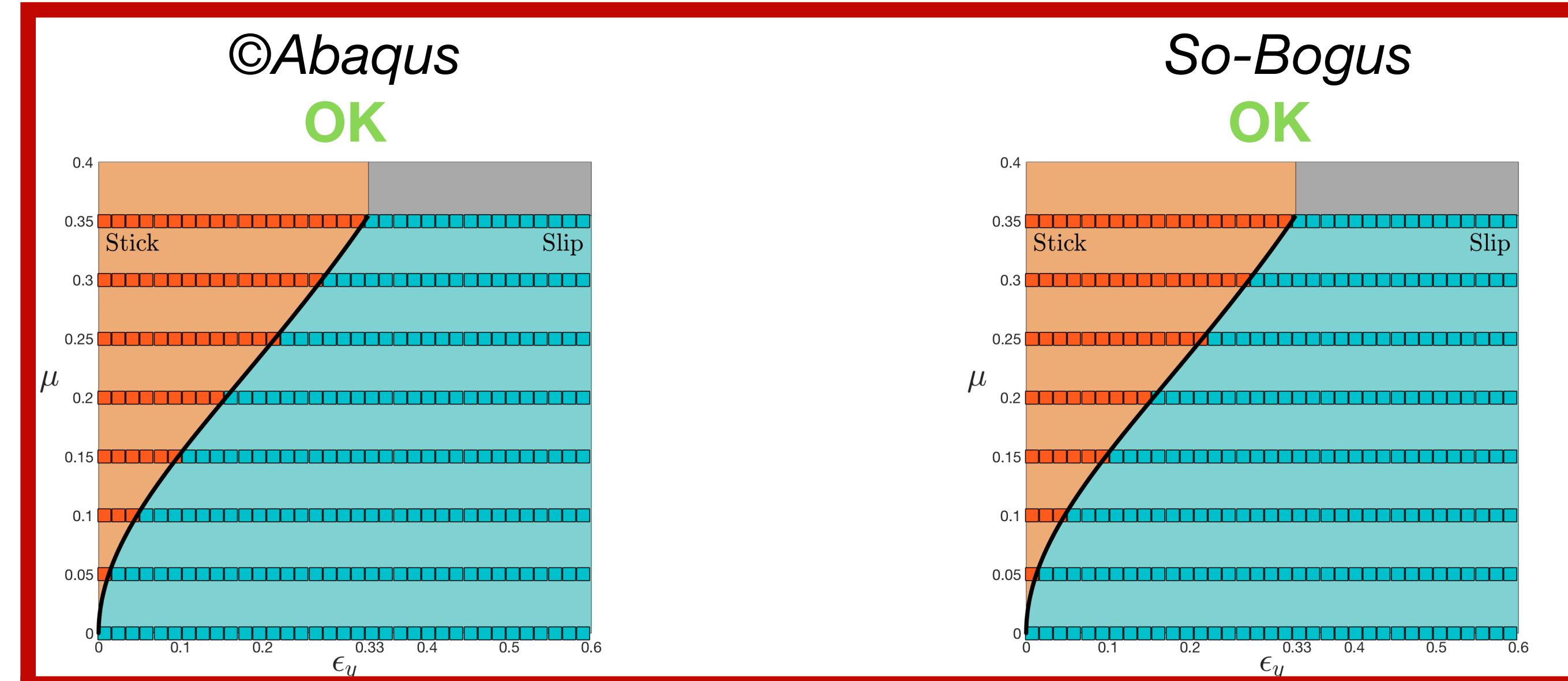
Results

Stick-slip test



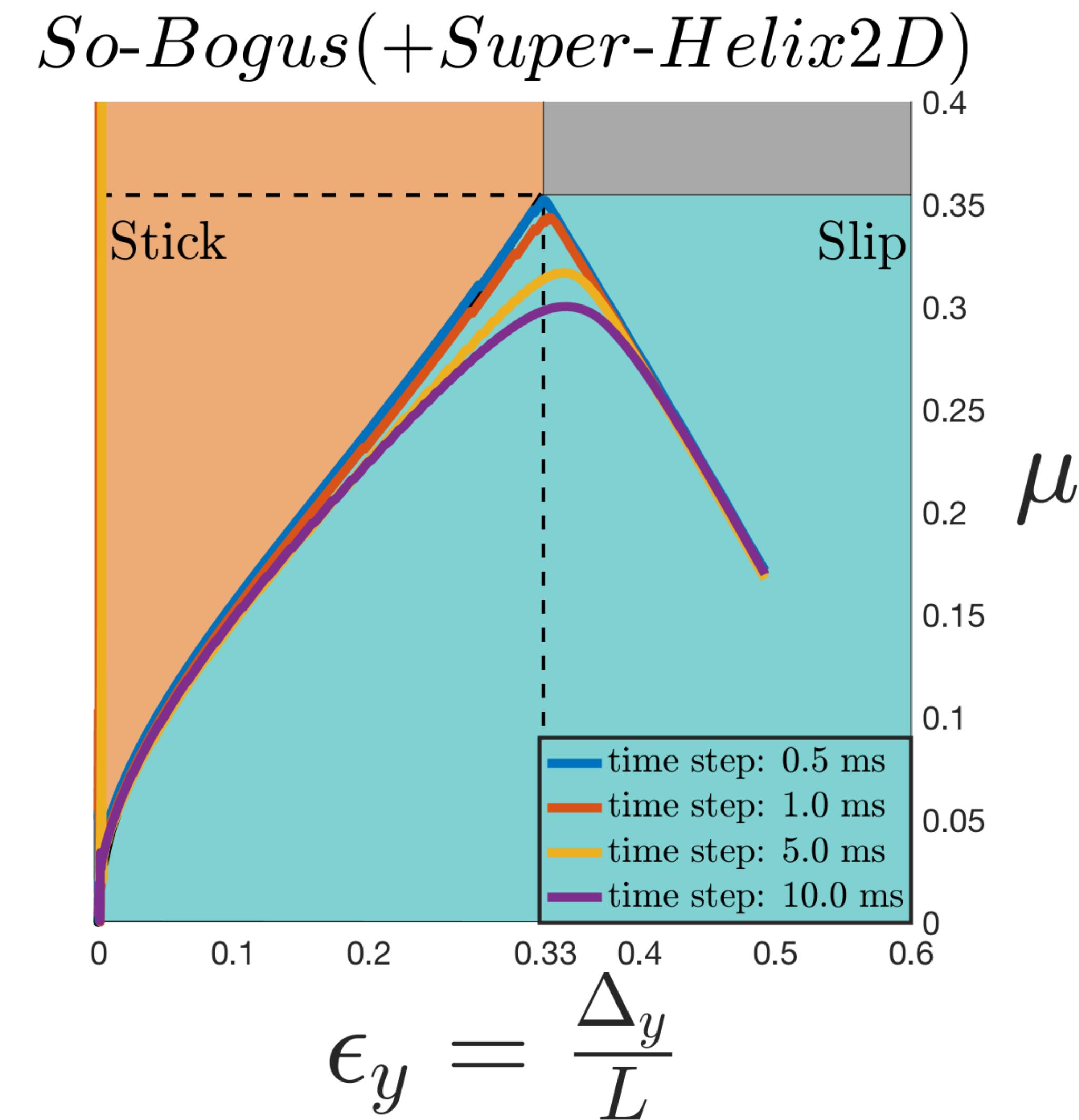
Results

Stick-slip test



Results

Stick-slip test – sensitivity to the time-step



Results

| Tested Code | Cantilever | Bend-Twist | Lateral Buckling | Stick-Slip |
|--|----------------------------|---------------|----------------------------|---------------------------------------|
| Rod | | | | |
| DISCRETE ELASTIC ROD [Bergou et al. 2010] | OK (300 elts) | OK (200 elts) | - | - |
| SUPER-HELIX [Bertails et al. 2006] | OK (50 elts) | OK (30 elts) | - | - |
| SUPER-CLOTHOID [Casati and Bertails-Descoubes 2013] | OK (20 elts) | OK (25 elts) | - | - |
| Ribbon | | | | |
| SUPER-RIBBON [Charrondière et al. 2020] | OK (20 elts) | - | KO | - |
| Plate | | | | |
| LIBSHELL [Chen et al. 2018] | OK (Res 0) | - | OK (Res +) | - |
| DISCRETE SHELL (+ LIBSHELL) [Grinspun et al. 2003] | OK (Res +) | - | KO | - |
| ARCSIM [Narain et al. 2012] | KO | - | X | - |
| DISCRETE SHELL + ARCSIM (tentative fix of ARCSIM) | KO | - | X | - |
| PROJECTIVE DYNAMICS [Bouaziz et al. 2014] (fit) | KO | - | X | - |
| Contact & friction | | | | |
| VISCOS FRICITION (+ SUPER-HELIX 2D) | - | - | - | KO |
| So-BOGUS [Daviet et al. 2011] (+ SUPER-HELIX 2D) | - | - | - | OK ($dt=0.5$ ms, $tol = 10^{-13}$ N) |
| ARGUS (\approx ARCSIM + So-BOGUS) [Li et al. 2018] | - | - | - | KO |
| ARGUS NON ADAPTIVE (fix of ARGUS) | - | - | - | OK ($dt=0.5$ ms, $tol = 10^{-13}$ N) |
| BRIDSON-HARMON [Bridson et al. 2002; Harmon et al. 2008] (+ ARCSIM) | - | - | - | KO |
| PROJECTIVE FRICTION [Ly et al. 2020] | - | - | - | KO |
| Reference codes in Mechanical Engineering | | | | |
| FENICSHELL [Hale et al. 2018] | OK (Res 0, $P_{2,3}$ elts) | - | OK (Res 0, $P_{2,3}$ elts) | - |
| ©ABAQUS | OK (200 P_2 elts) | KO | KO | OK ($dt=9 \mu s$) |

And the Oscar goes to ...

2020 Technical Academy Award (Oscar)

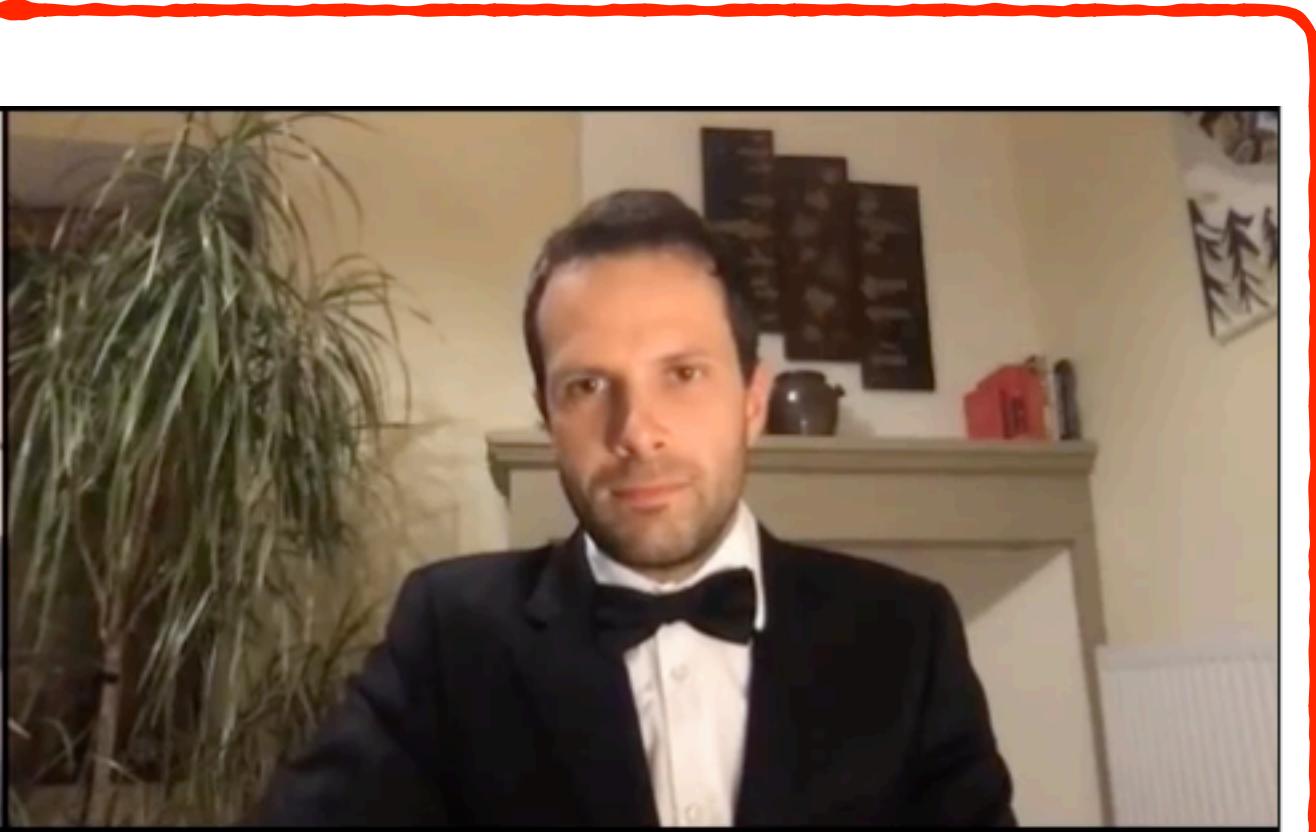
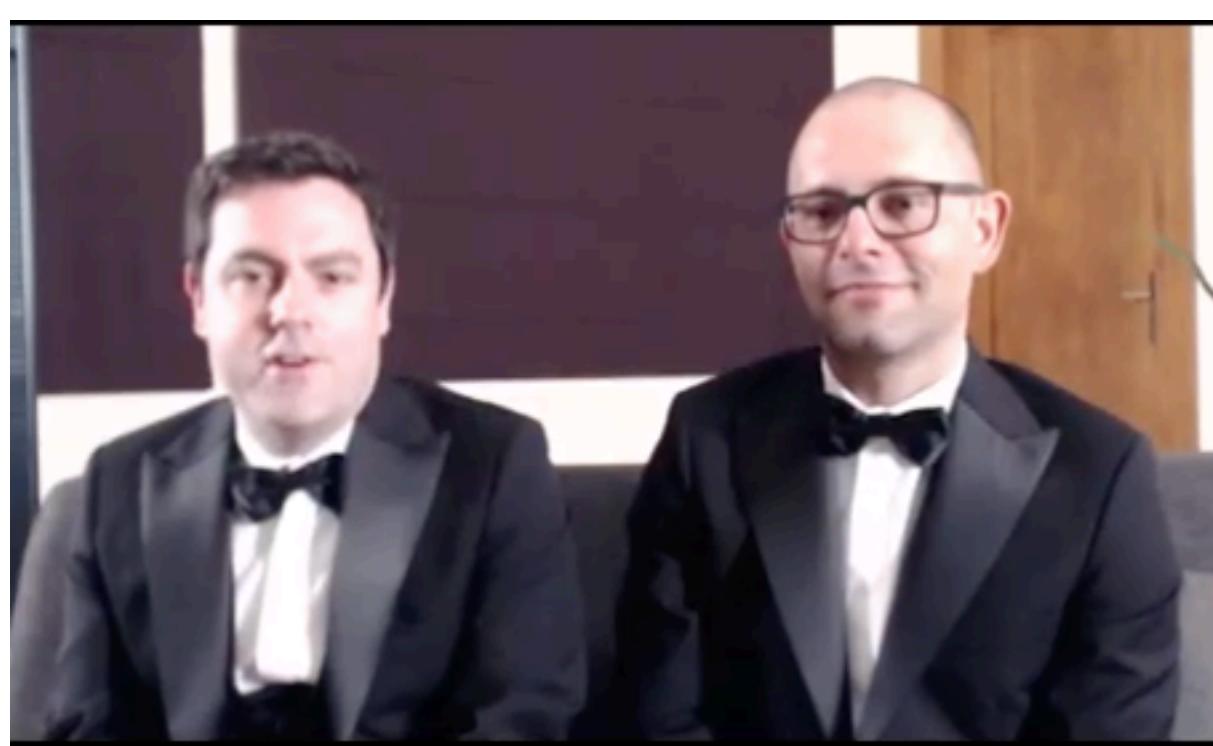


Weta FX special effects (NZ)

“for the Synapse Hair Simulation System”

Alita: Battle Angel (2019)





Gilles Daviet



Gilles Daviet

PhD (2016) INRIA Grenoble
(dir. F. Bertails-Descoubes)

So'Bogus



SIGGRAPH Asia 2011
2000 fibers (25 Hours CPU)



SIGGRAPH 2020

100 000 fibers (with contacts)
 4×10^6 DoF

P. Alart and A. Curnier. 1991. A Mixed Formulation for Frictional Contact Problems Prone to Newton like Solution Methods. *Comput. Methods Appl. Mech. Eng.* 92, 3 (1991).

M. Jean and J.J. Moreau. 1988. Dynamics in the presence of unilateral contacts and dry friction : a numerical approach. In *Second Meeting on Unilateral Problems in Structural Analysis (Unilateral Problems in Structural Analysis, 2)*. Springer.



Conclusion

- Four protocols based on solid mechanics
- dimensionless parameters
- well-established master (bifurcation) curves
- limitations: only statics, no self-contact, purely elastic
- Results on 15 codes from Computer Graphics and 2 from Mechanical Engineering
- Encouraging results for Computer Graphics Models

Download the master curves:

https://elan.inrialpes.fr/people/vromerog/Validation134_sggph2021.html



Thank you
for your attention

