

# Elastic knots

(elastic beam under finite rotation and self-contact)

Sébastien Neukirch

CNRS & Univ Paris 6 (France)  
d'Alembert Institute for Mechanics

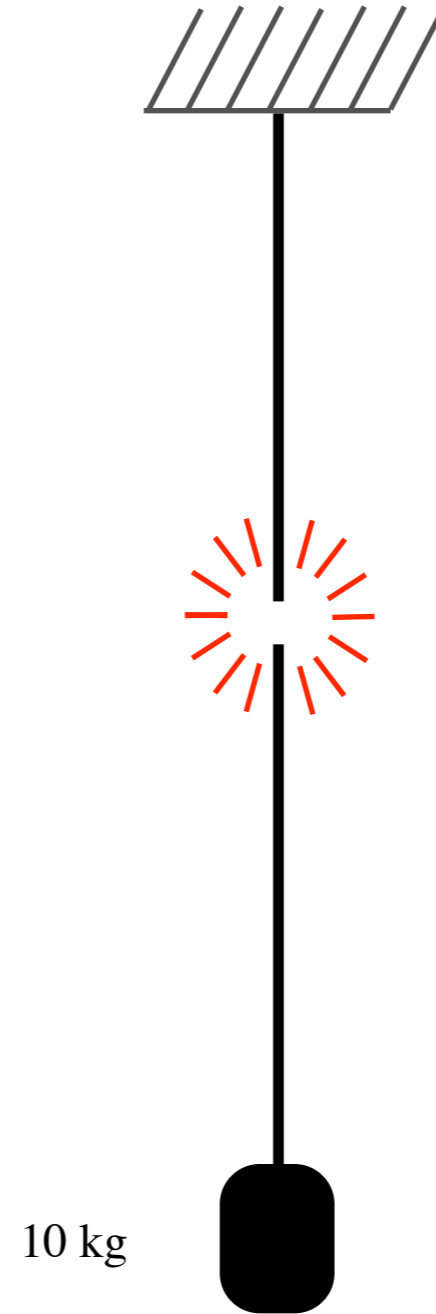
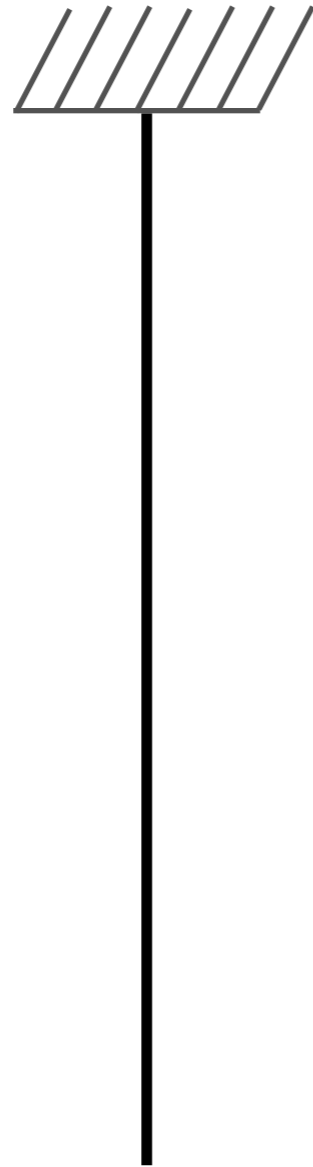
joint work with:

Nicolas Clauvelin (PhD work)

Basile Audoly

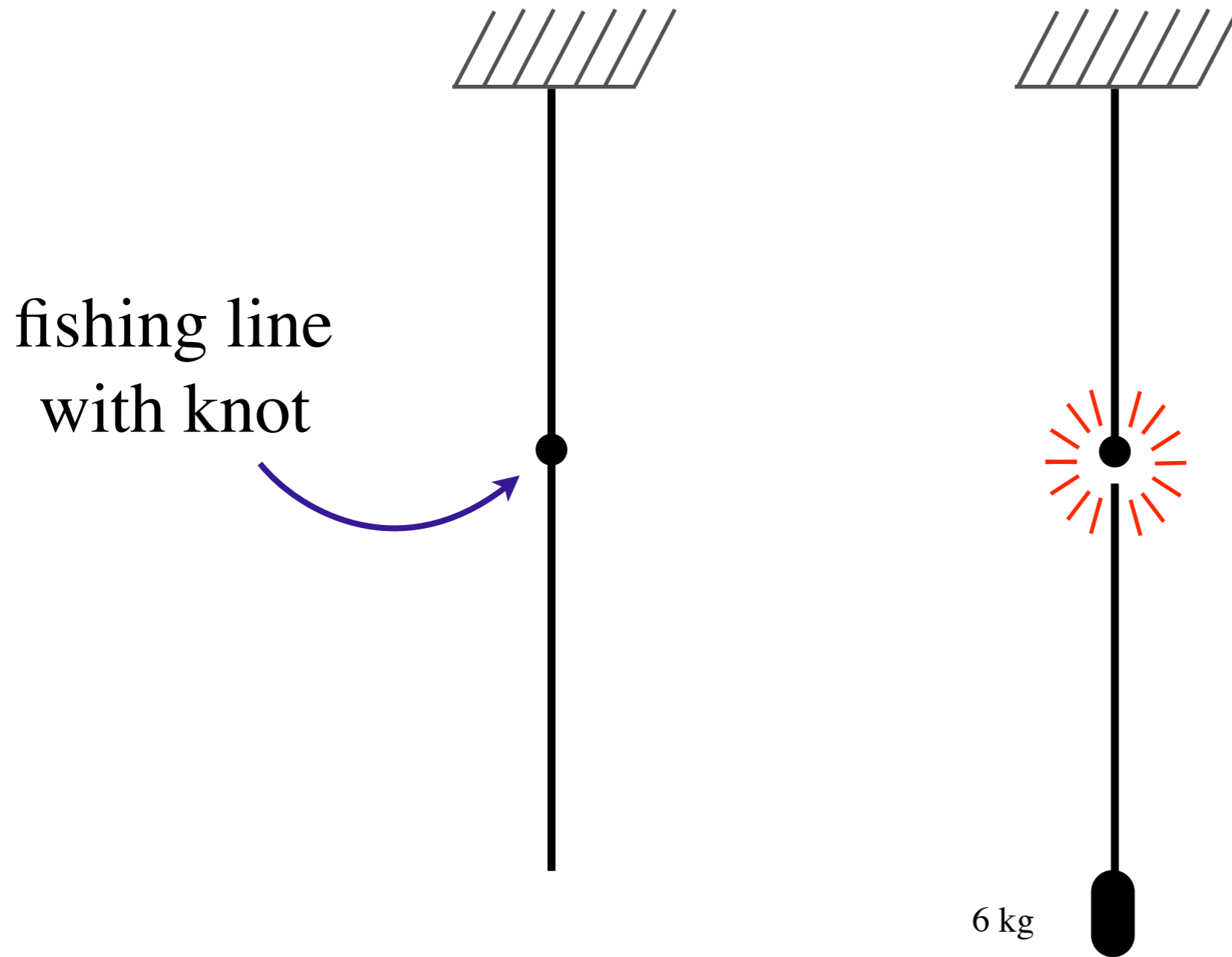
# Tensile strength of a wire

fishing line



Stasiak et al, *Science* (1999)

# Tensile strength of a wire



Stasiak et al, *Science* (1999)

# Knots are everywhere

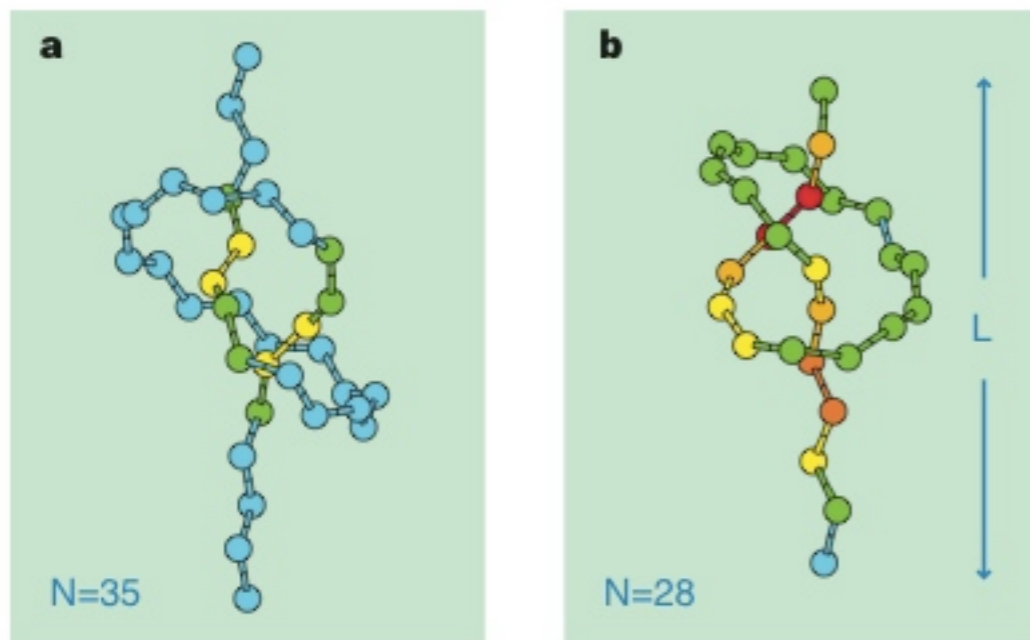
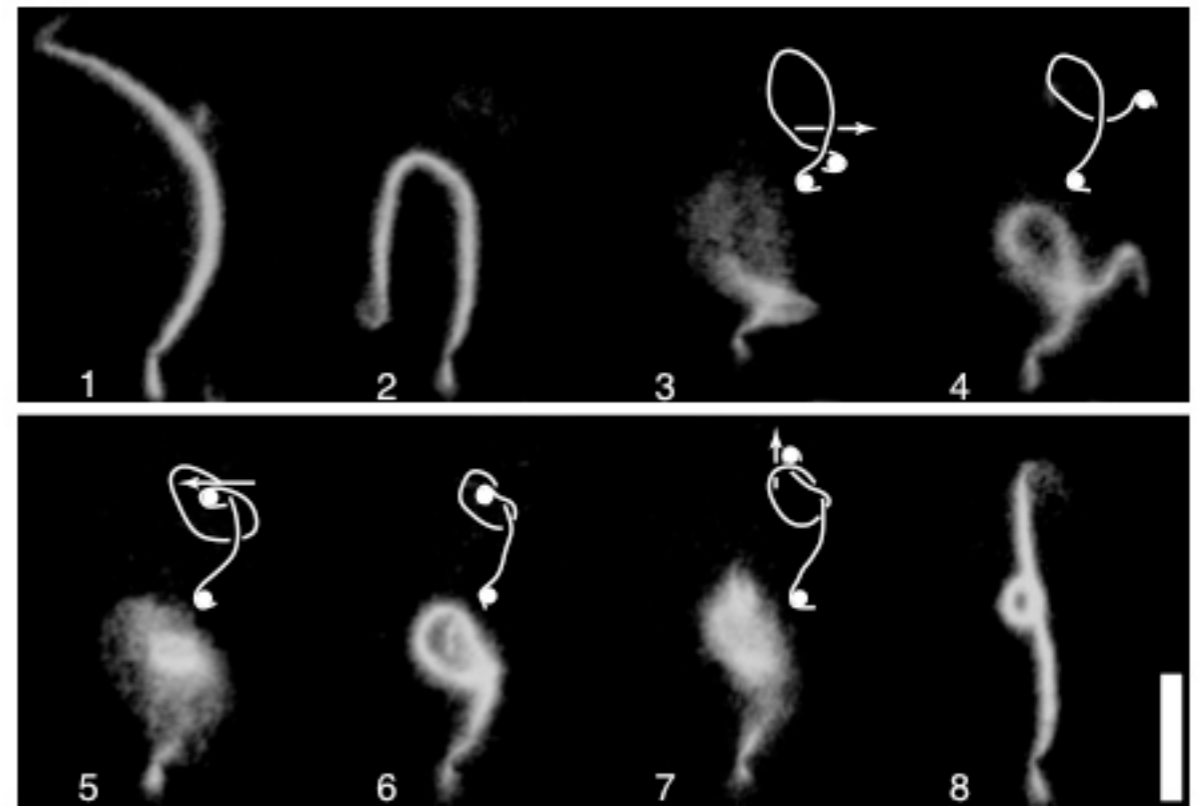
Long enough polymers are (almost) certainly knotted

Sumners+Whittington, *J. Phys. A : Math. Gen.* 1988

273 knotted proteins in the ProteinDataBank (1%)

Single molecule experiment  
with knotted F-Actin filaments

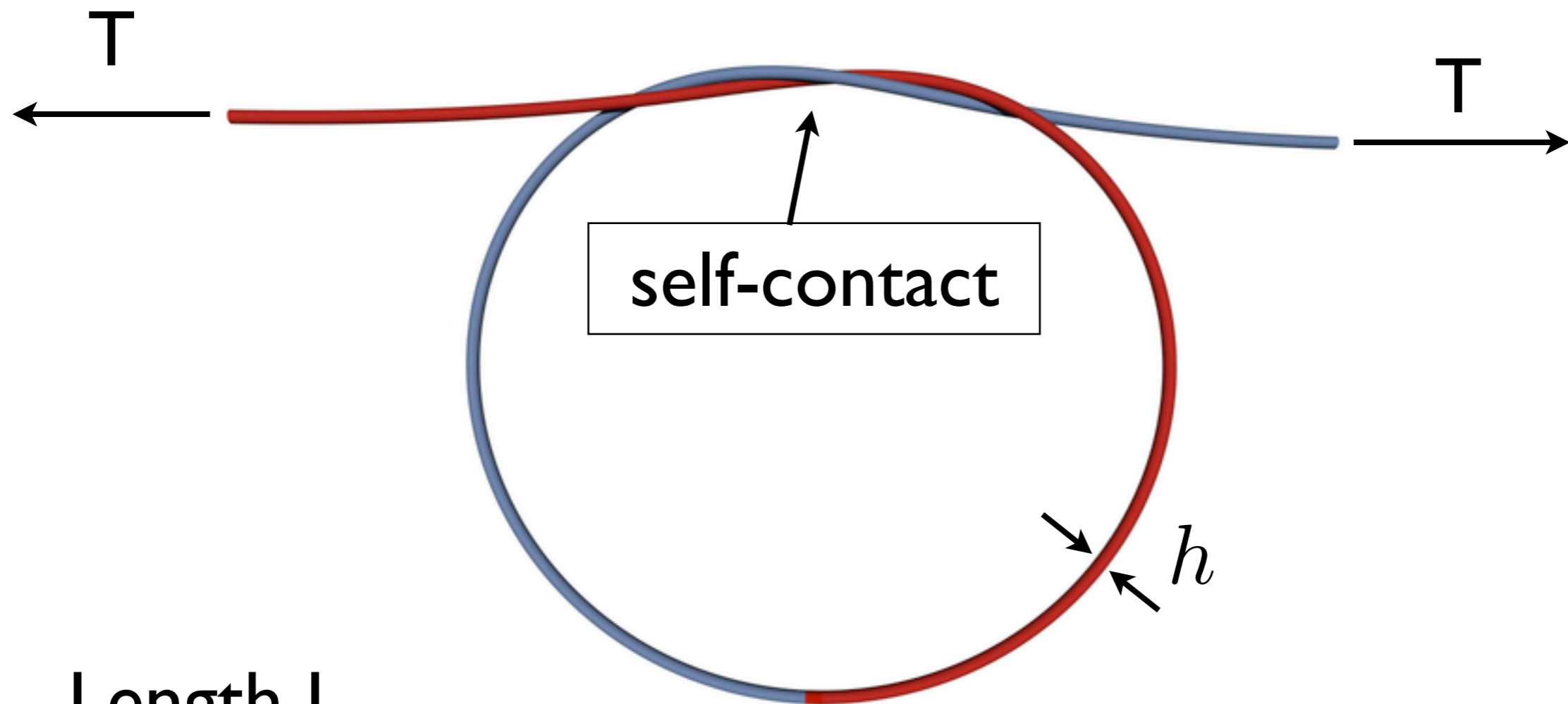
Arai et al, *Nature* (1999)



Ab-initio molecular simulations  
for alkane molecule ( $C_{10}H_{22}$ )

Saitta et al, *Nature* (1999)

# Elastic knots



- Length  $L$
- Circular cross-section: radius  $h$
- Bending rigidity :  $E I$
- Twist rigidity :  $G J$

$E$  : Young's modulus

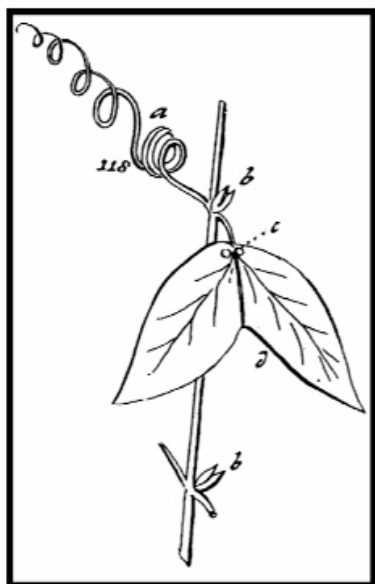
$G$  : shear modulus

$$I = \frac{\pi h^4}{4}$$

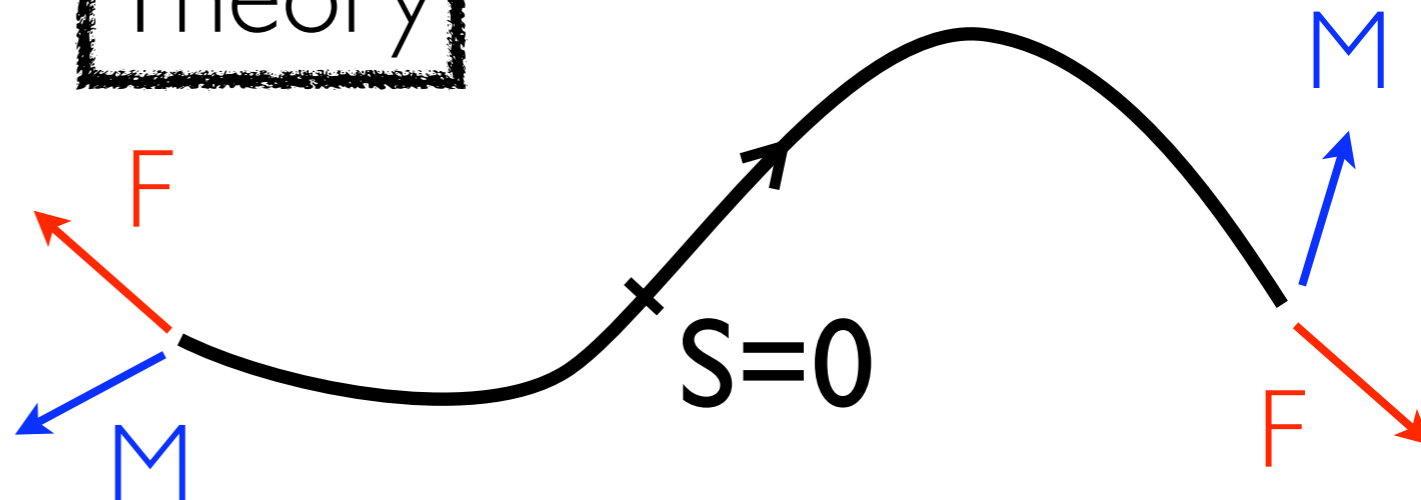
$$J = \frac{\pi h^4}{2}$$

# Elastic filaments

climbing plants

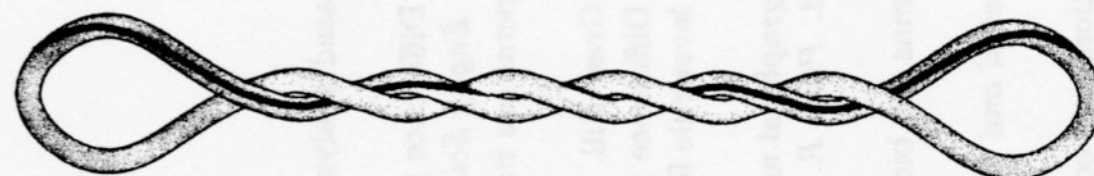


Theory

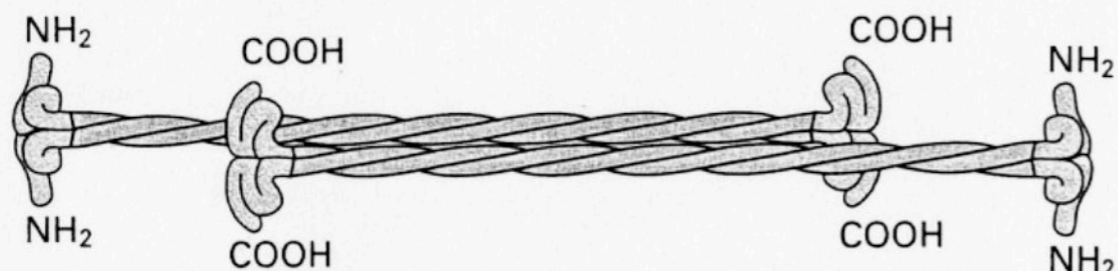


Applications

DNA supercoiling

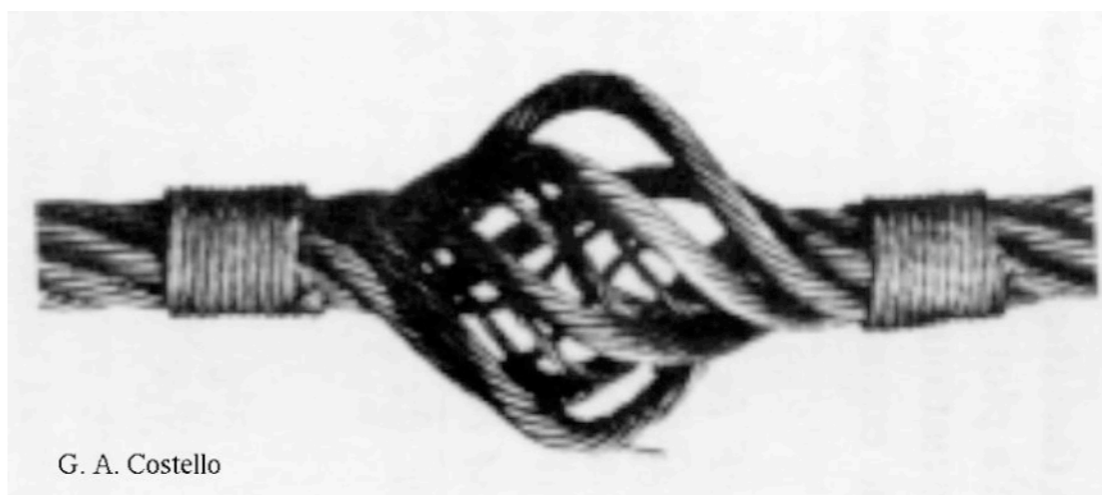


fibrous proteins

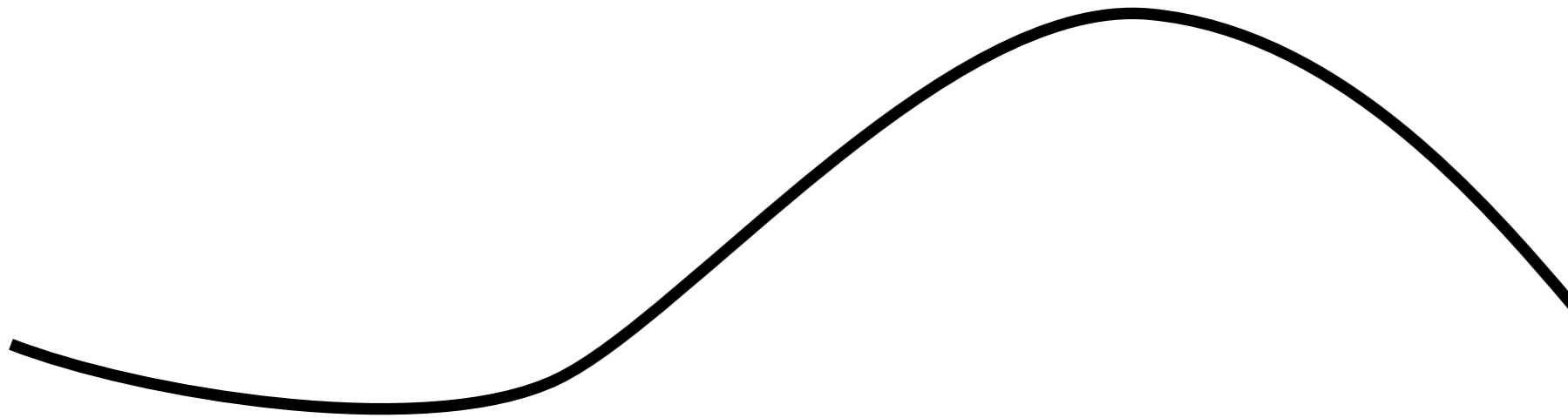


tétramère fait de deux dimères superenroulés étagés

cables



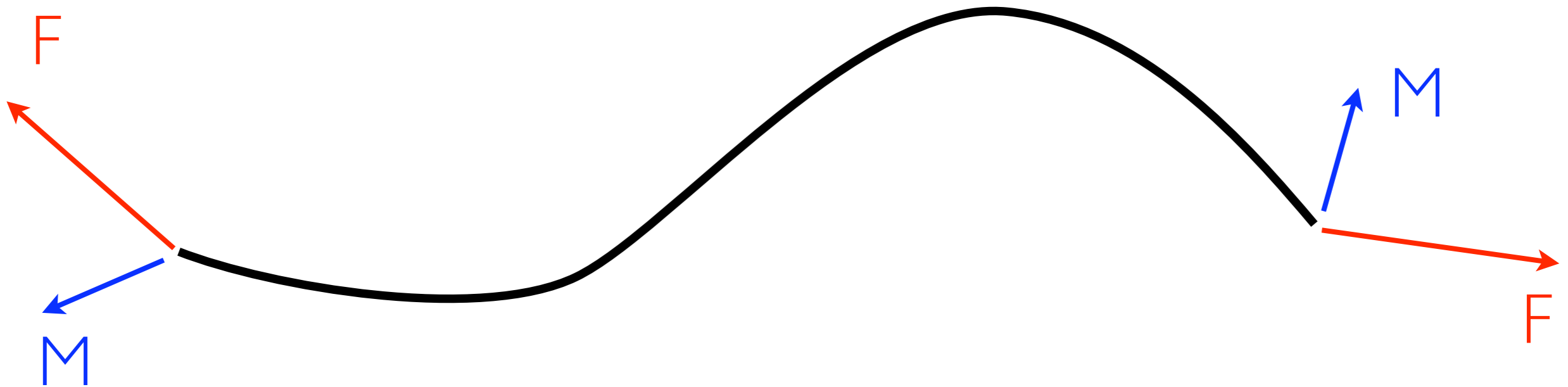
# Kirchhoff equations



apply to :

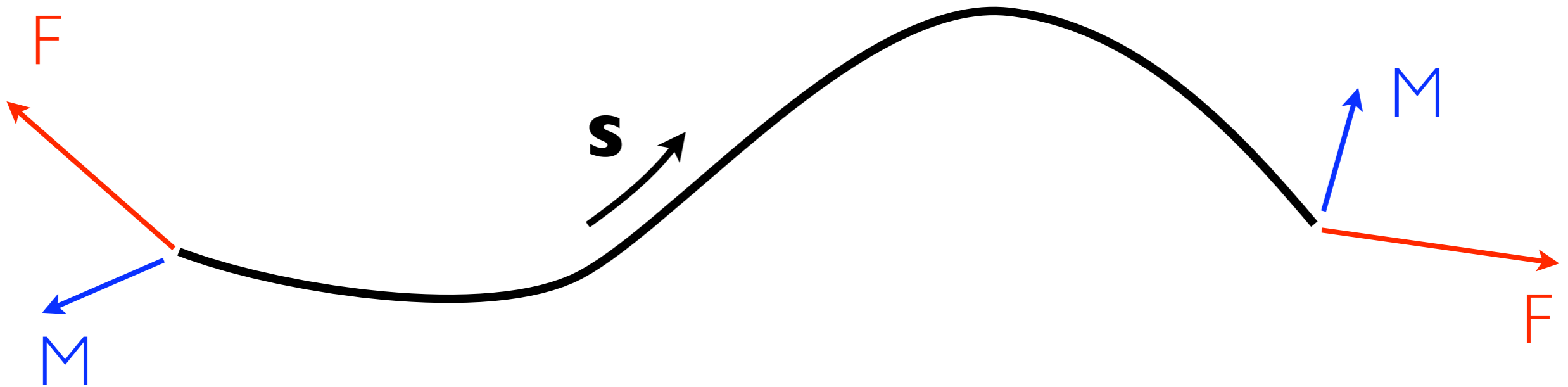
- slender bodies
- not too bent

# Kirchhoff equations

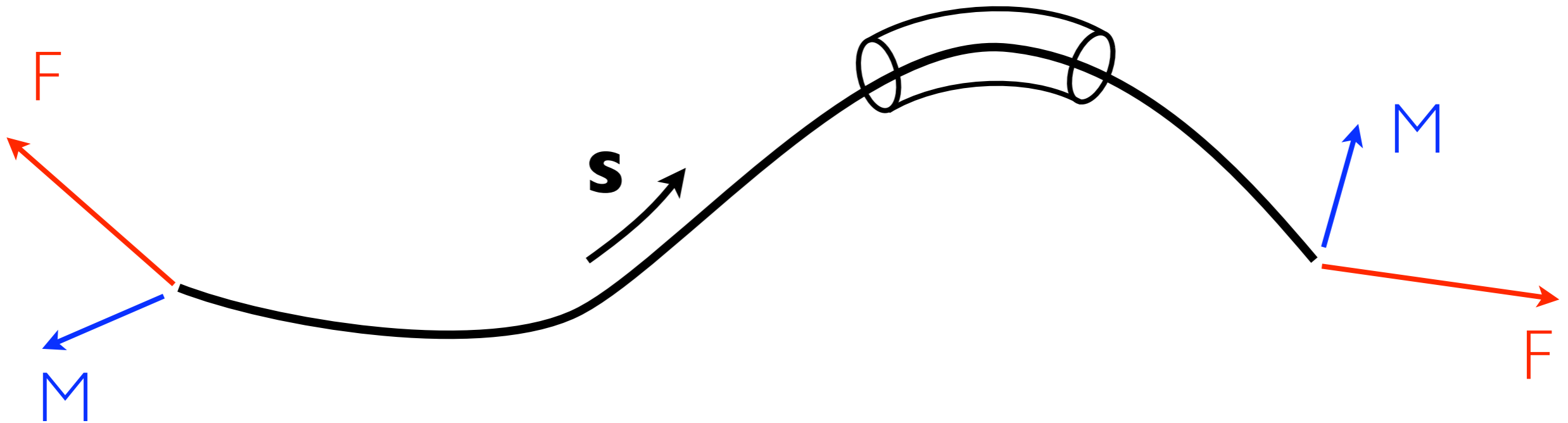




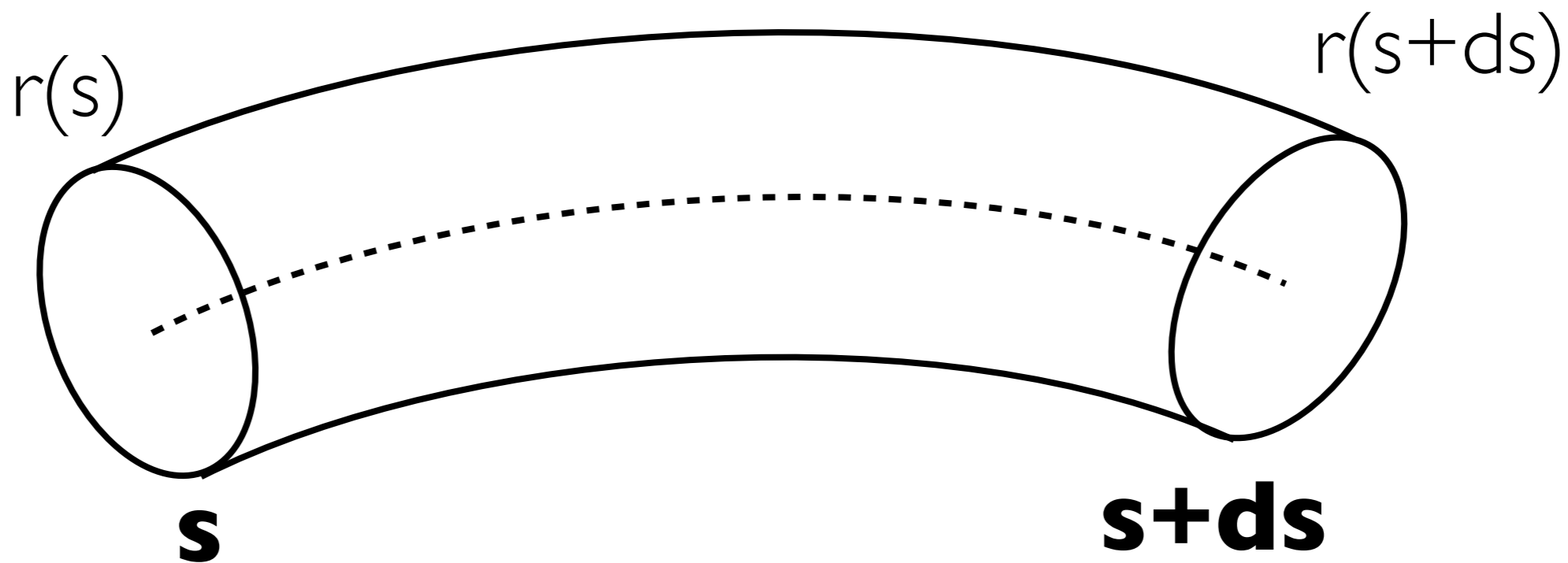
# Kirchhoff equations



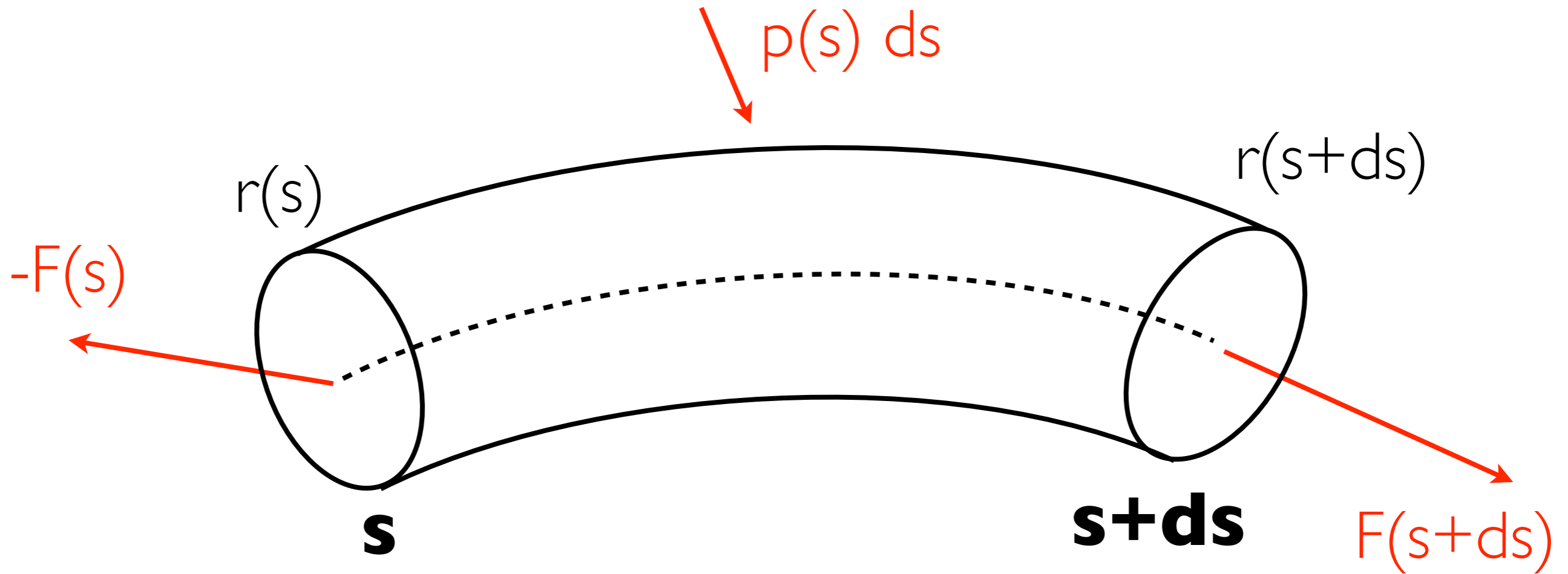
# Kirchhoff equations



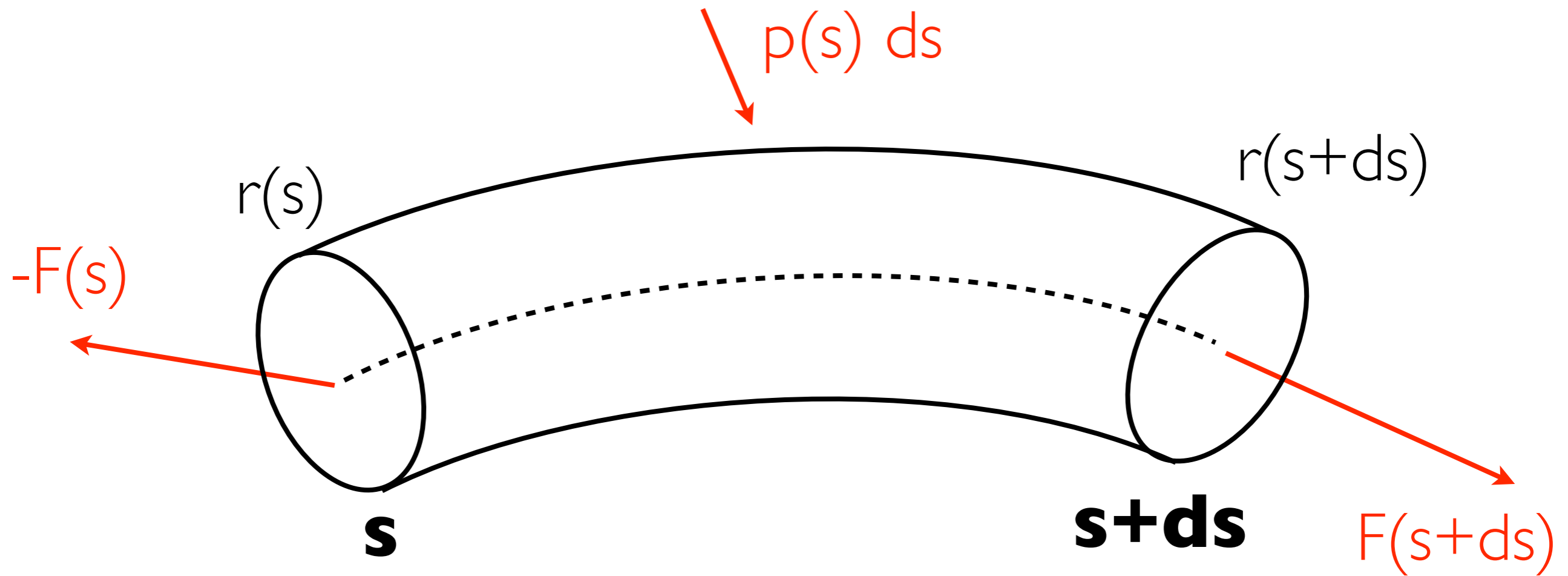
# Kirchhoff equations



# Kirchhoff equations



# Kirchhoff equations

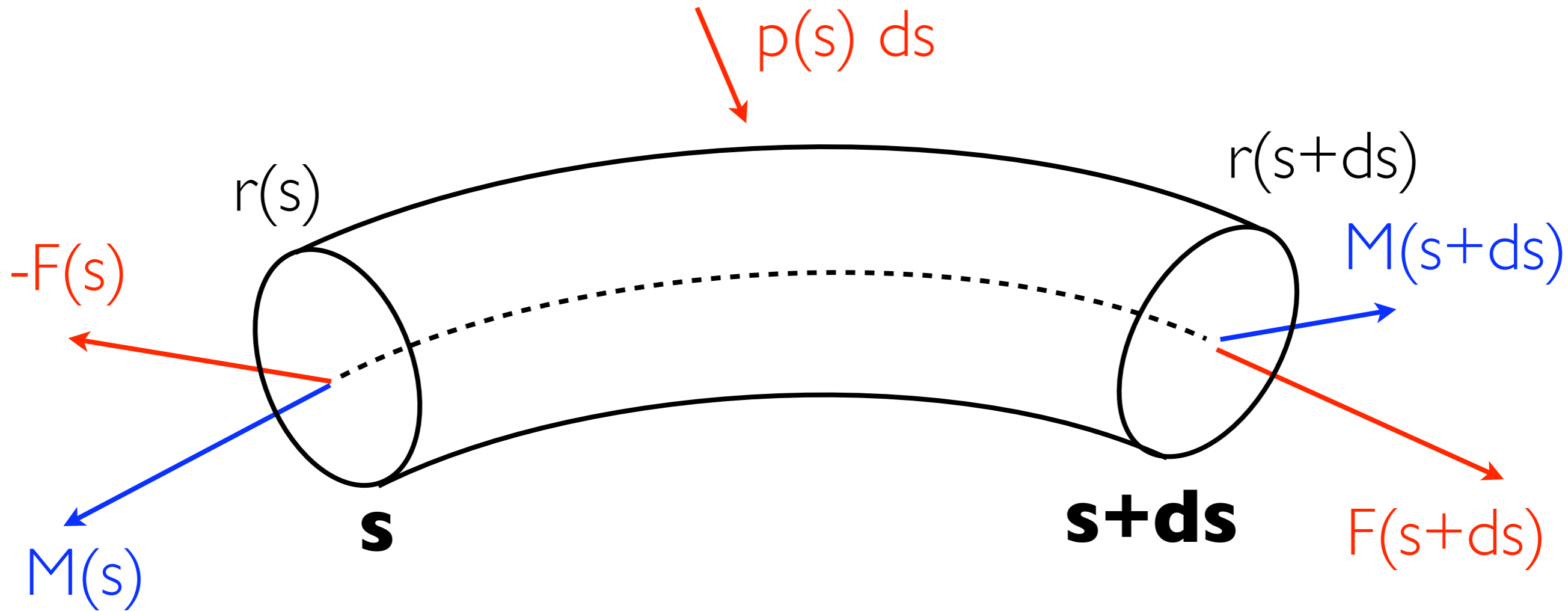


$$F(s+ds) - F(s) + p(s) ds = 0$$

Equilibrium

$$F'(s) + p(s) = 0$$

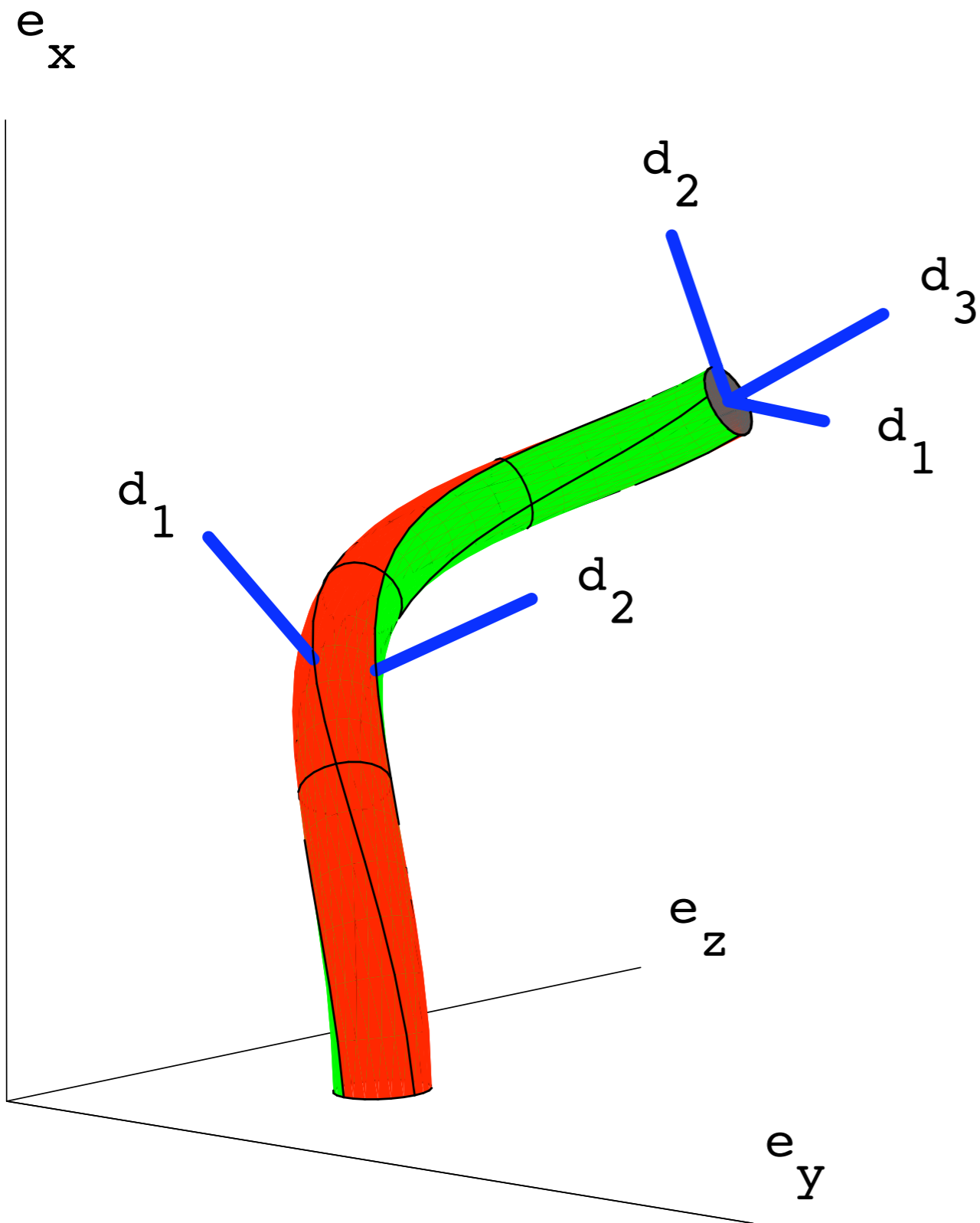
# Kirchhoff equations



Equilibrium

$$M' + r' \times F = 0$$

# Kirchhoff equations



Cosserat frame

$$d'_1 = u \times d_1$$

$$d'_2 = u \times d_2$$

$$d'_3 = u \times d_3$$

$$u = \{ \kappa_1, \kappa_2, \tau \} d_i$$

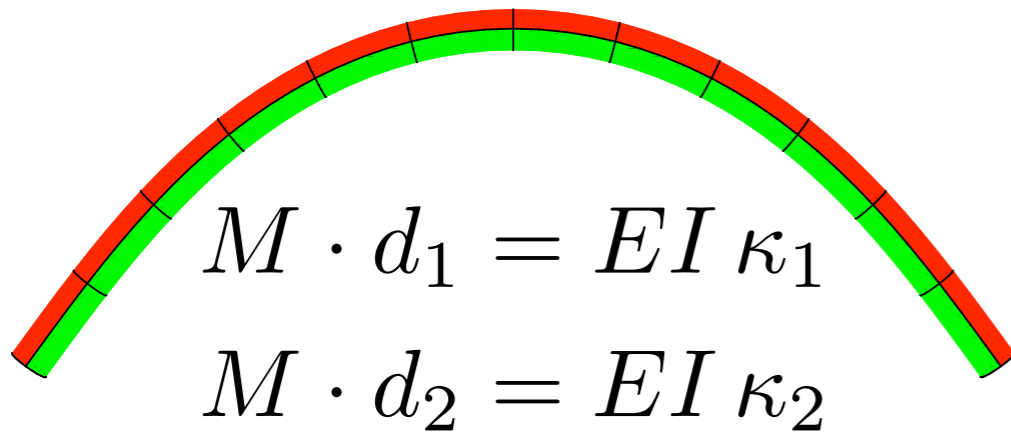
curvatures

twist

# Kirchhoff equations

constitutive relations

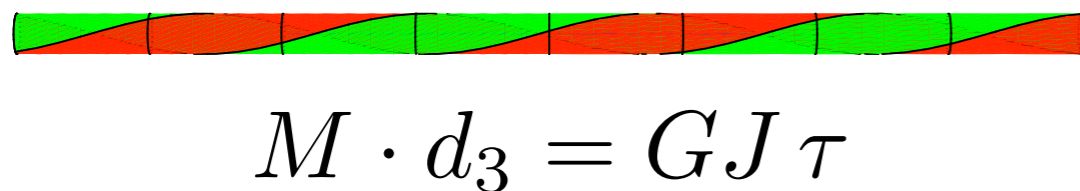
curvature



$E$  Young's modulus

$I$  second moment of area

twist



$G$  shear modulus

$J$  polar moment of area



# Kirchhoff equations

21 ODEs with variable :  $s$

ordinary differential equations

$$\frac{d}{ds} \vec{F} = \vec{p}$$

$$\frac{d}{ds} \vec{M} = \vec{F} \wedge \vec{d}_3$$

$$\frac{d}{ds} \vec{r} = \vec{d}_3$$

$$\frac{d}{ds} \vec{d}_i = \vec{u} \wedge \vec{d}_i$$

$$m_i = K_i u_i$$

linear elasticity

21 unknowns

$$\vec{F}(s)$$

$$\vec{M}(s)$$

$$\vec{r}(s)$$

$$\vec{d}_3(s)$$

$$\vec{d}_2(s)$$

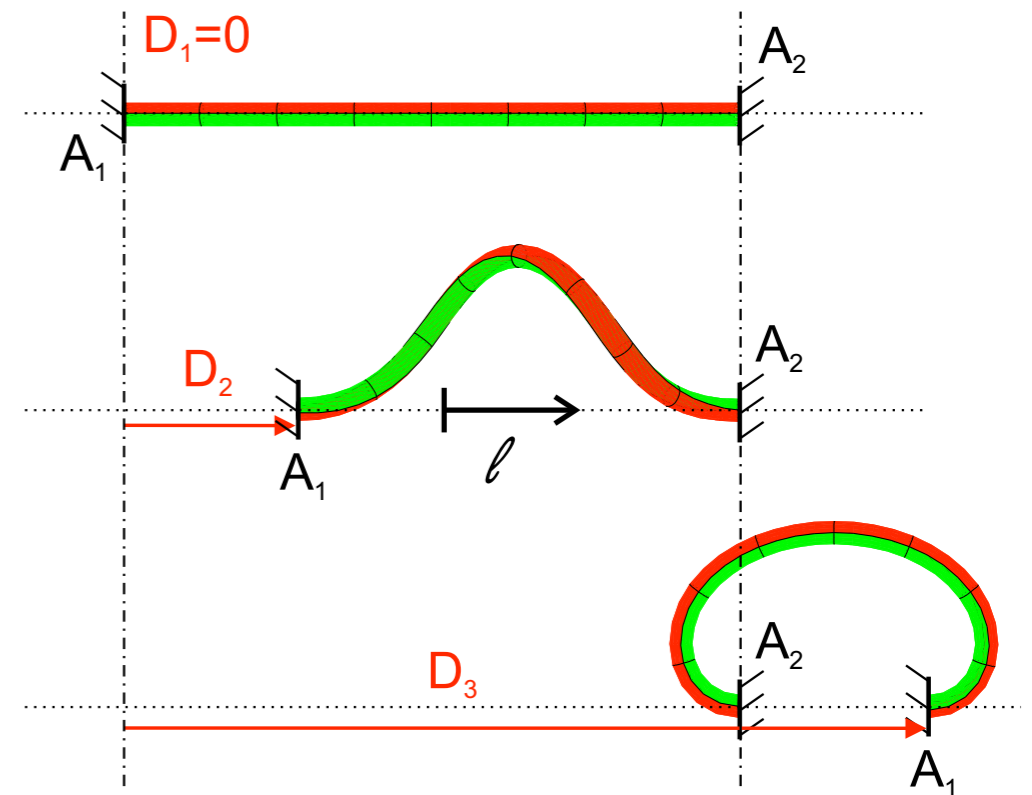
$$\vec{d}_1(s)$$

$$\vec{u}(s)$$

$i = 1, 2, 3$

boundary conditions

- how the rod is held
- few solutions are admissibles

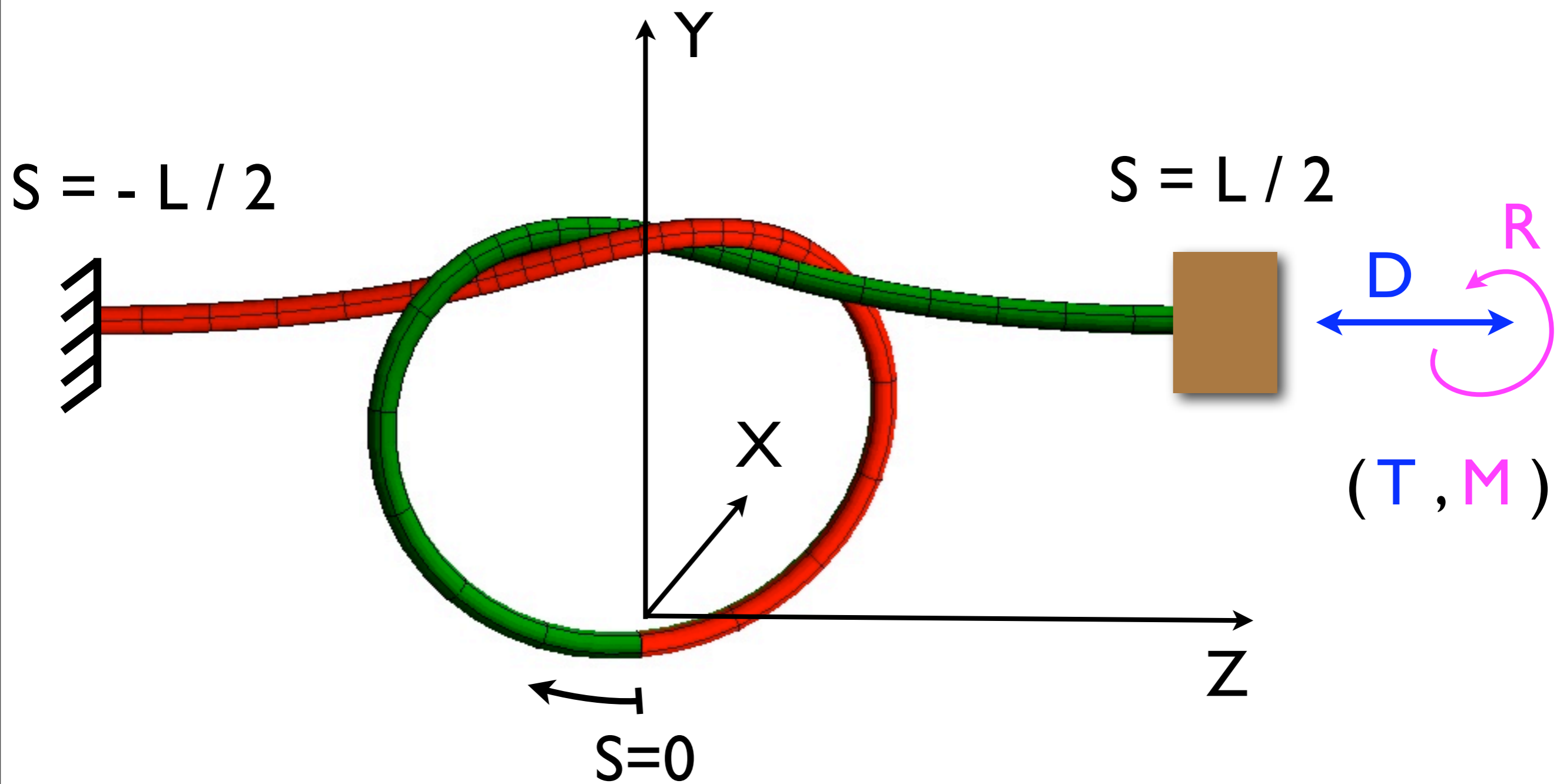


$$\vec{d}_3(A_1) = \vec{d}_3(A_2)$$

$$\vec{r}(A_2) - \vec{r}(A_1) = k \vec{d}_3(A_2)$$

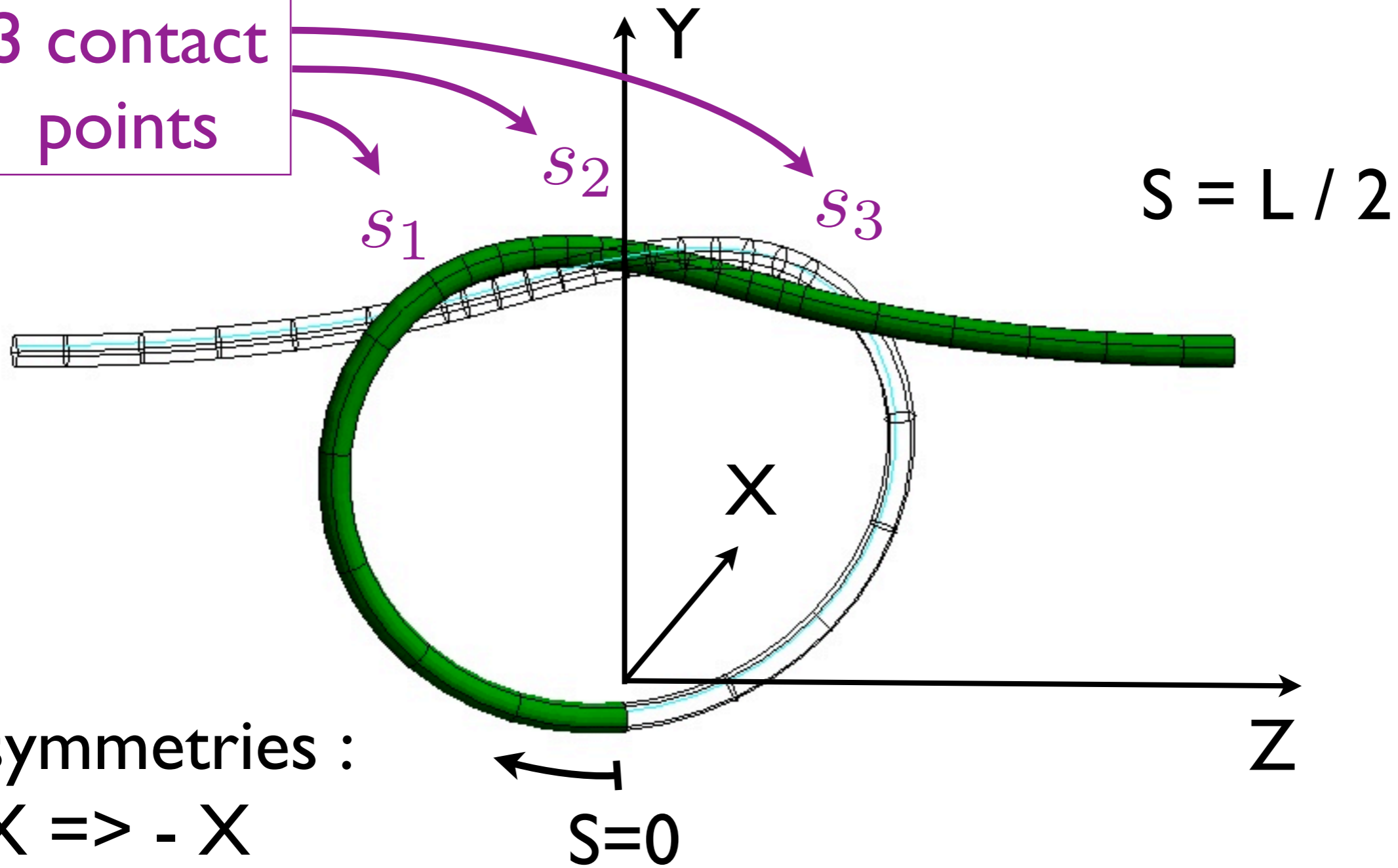
$$(D = L - k)$$

# Boundary value problem



# Boundary value problem

3 contact points



symmetries :

$$X \Rightarrow -X$$

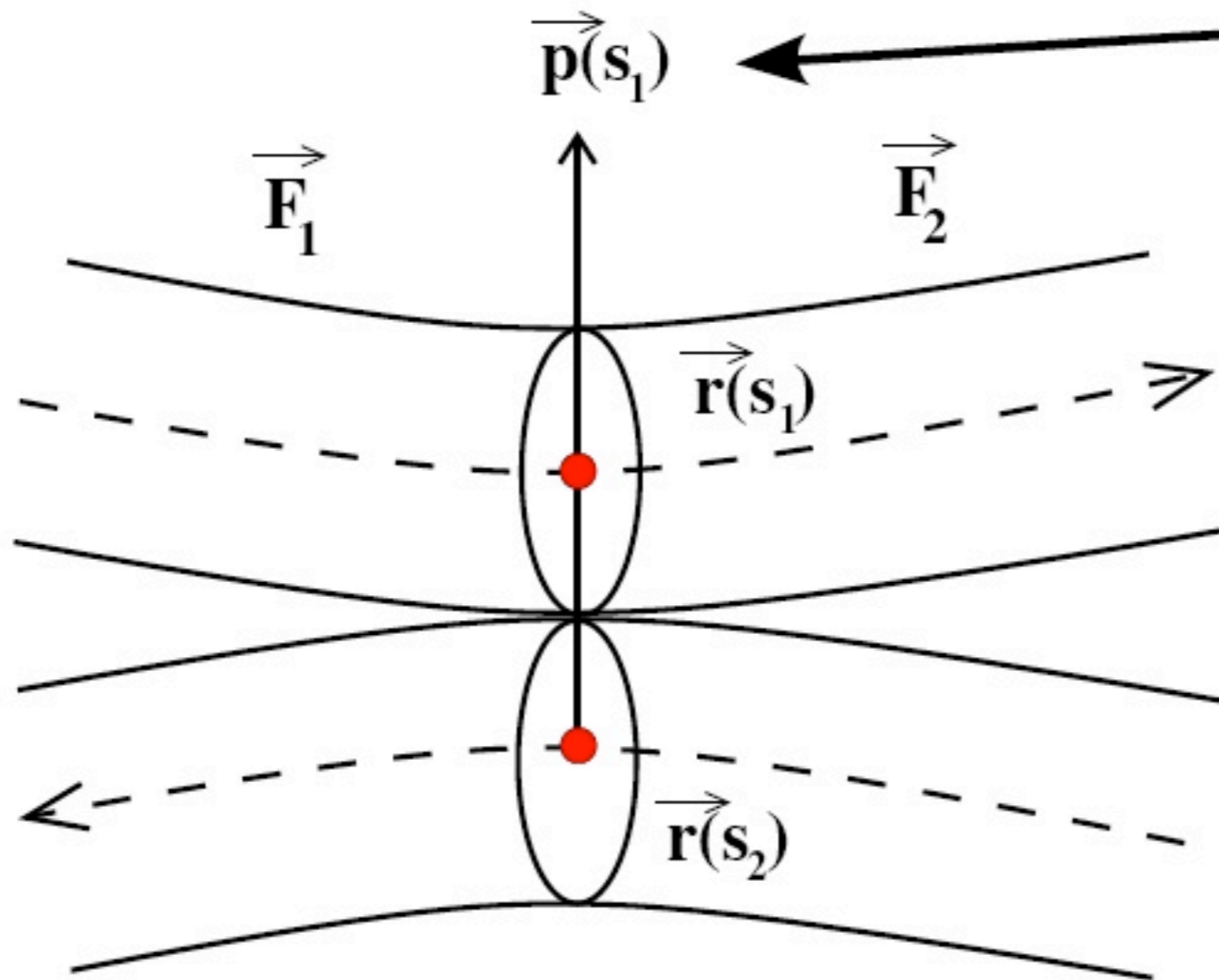
$$Y \Rightarrow Y$$

$$Z \Rightarrow -Z$$

- Shooting method (Mathematica)
- Gauss collocation (AUTO)

# Hard-wall contact, no friction

force from strand at  $s_2$   
acting on strand at  $s_1$



$$\vec{F}_1 = \vec{p} + \vec{F}_2$$

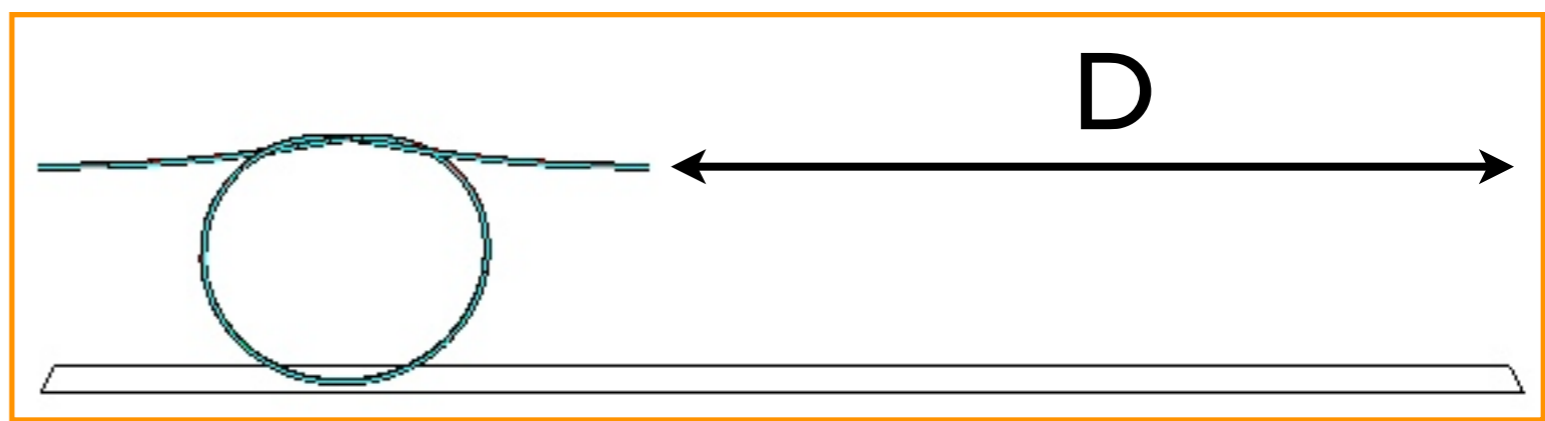
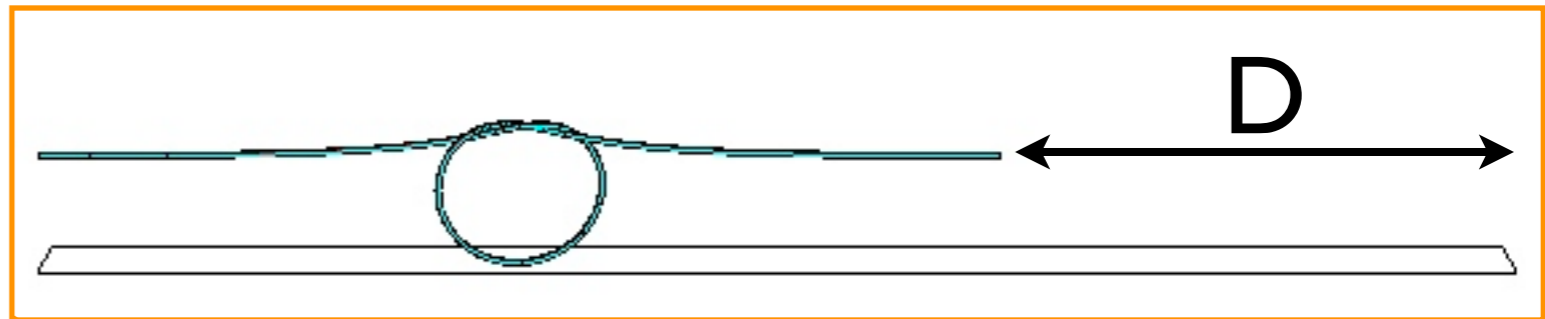
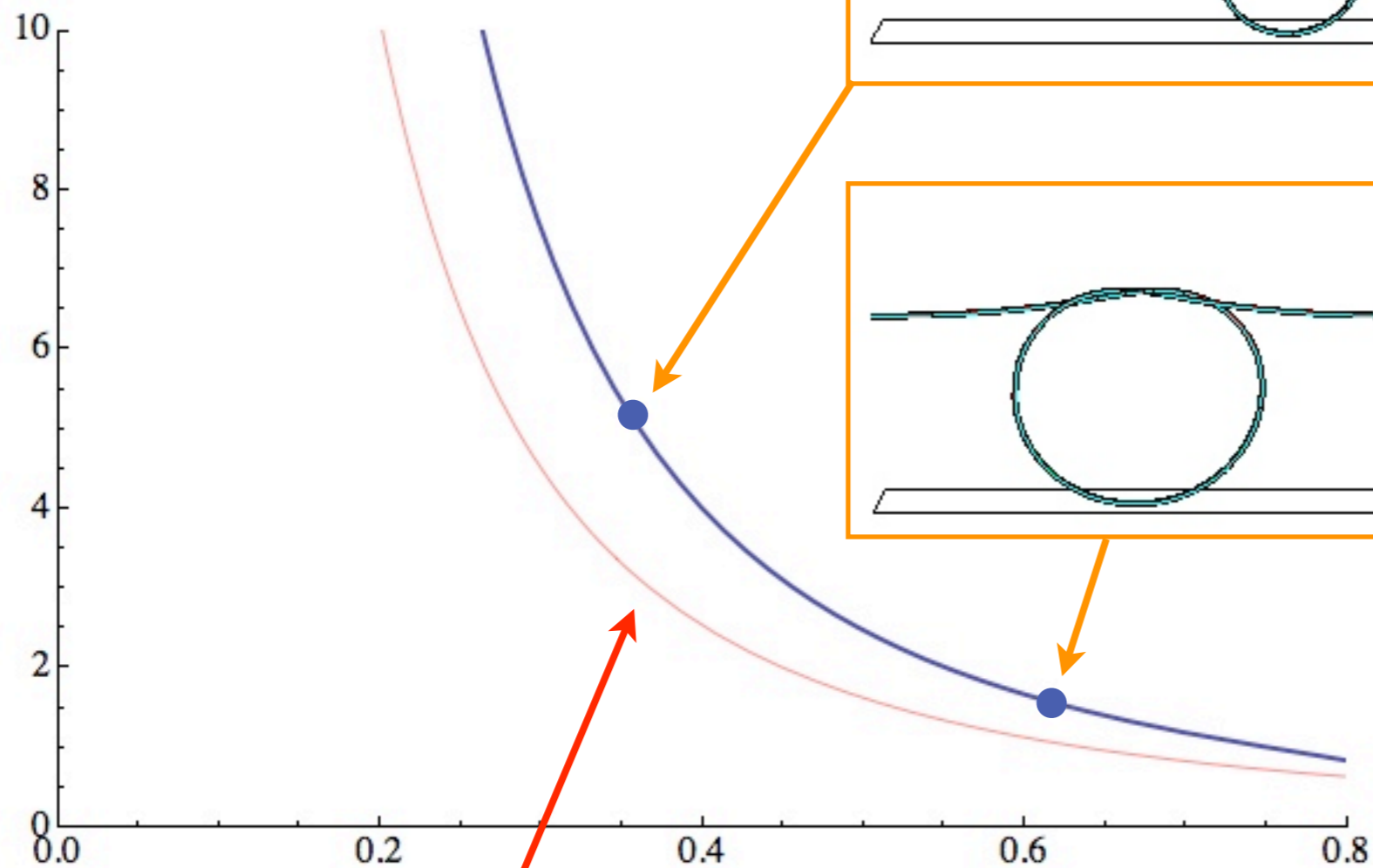
$$\vec{p} = p \frac{\vec{r}(s_1) - \vec{r}(s_2)}{|\vec{r}(s_1) - \vec{r}(s_2)|}$$

touching conditions :

$$\left\{ \begin{array}{l} |\vec{r}(s_1) - \vec{r}(s_2)| = \text{thickness} \\ (\vec{r}(s_1) - \vec{r}(s_2)) \perp \vec{d}_3(s_1) \\ (\vec{r}(s_1) - \vec{r}(s_2)) \perp \vec{d}_3(s_2) \end{array} \right.$$

# Numerical Path Following : Results

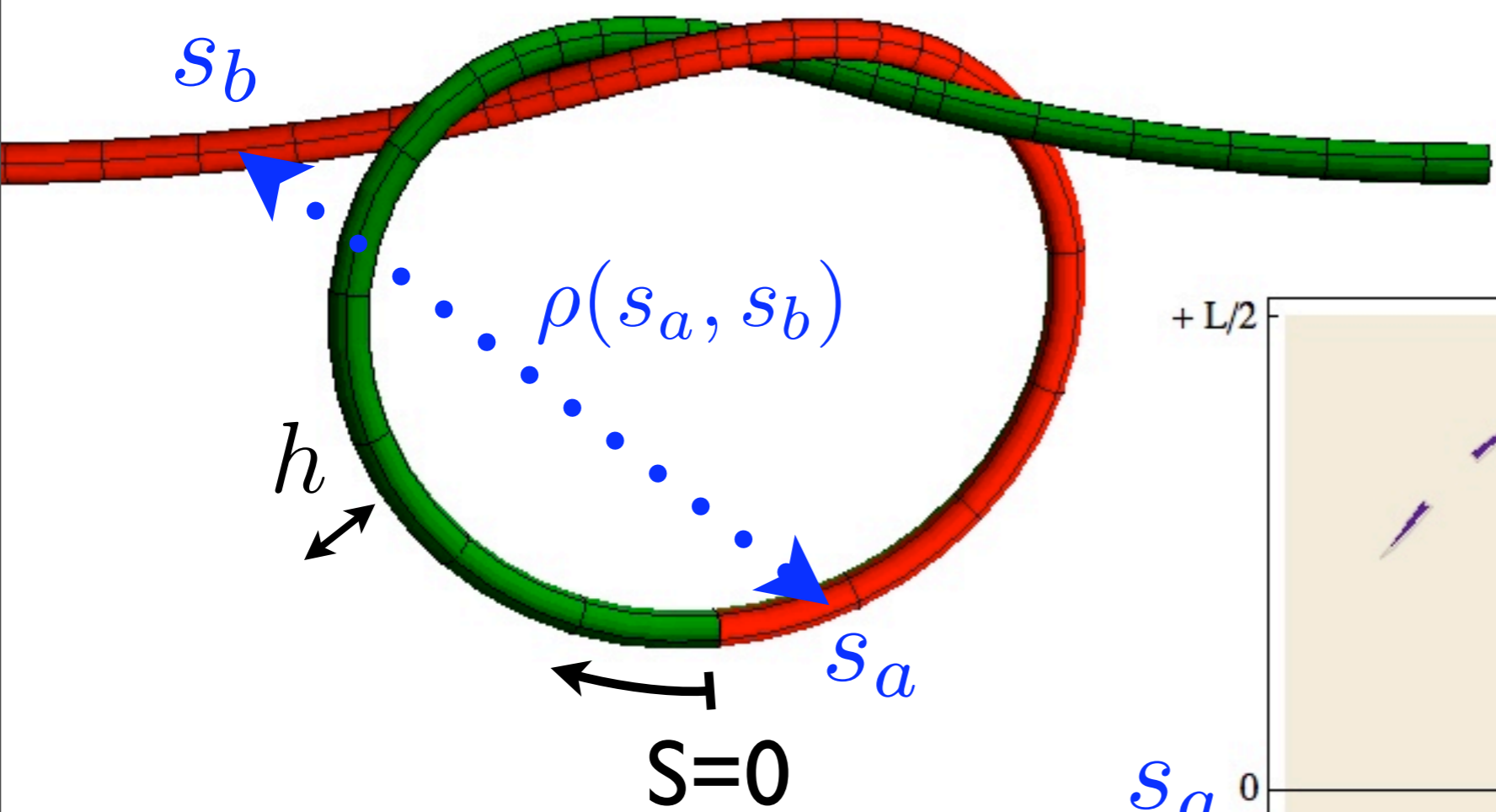
$$t = \frac{TL^2}{(2\pi)^2 EI}$$



Planar Elastica  $t = \left(\frac{2/\pi}{d}\right)^2$

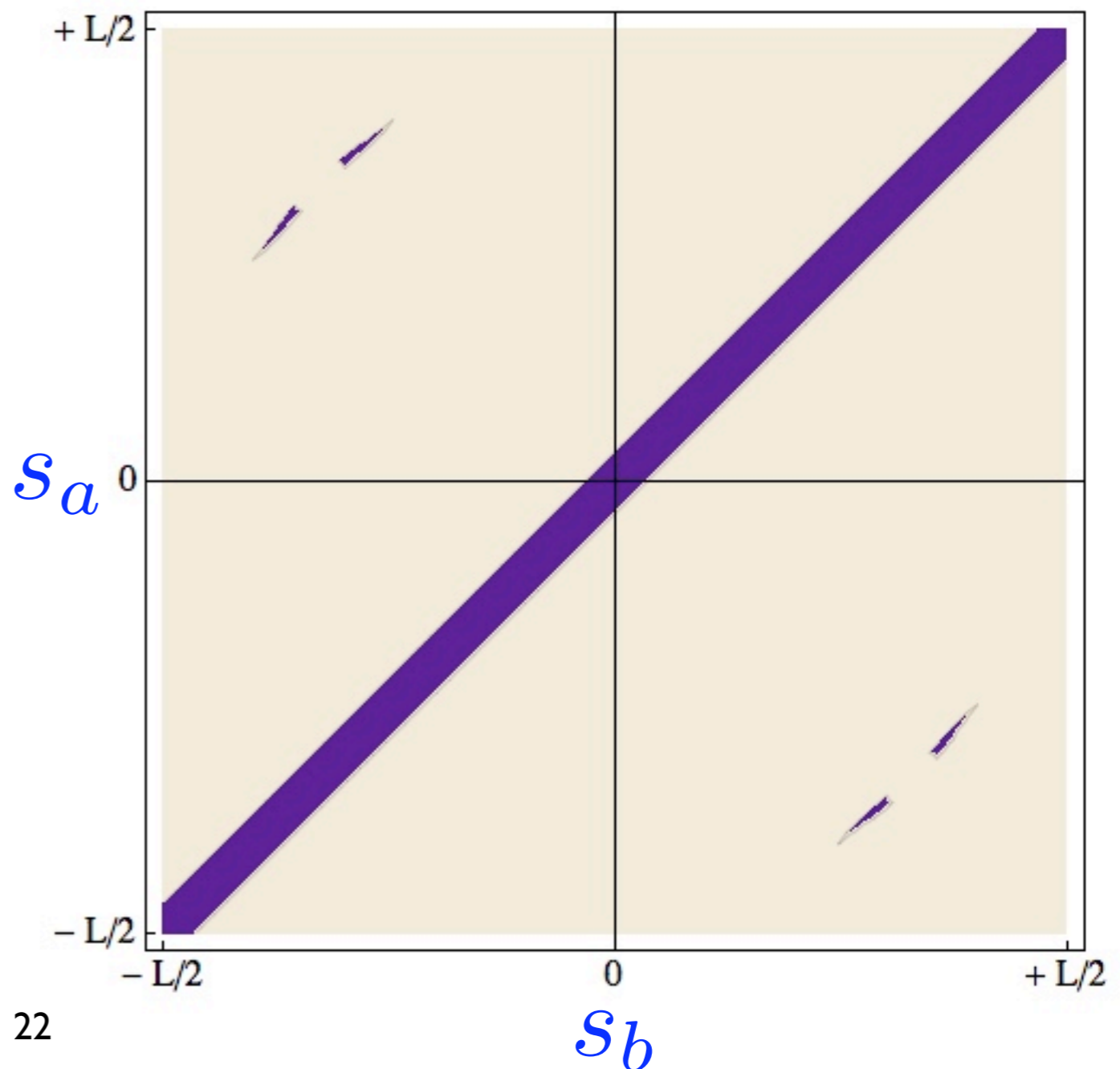
$$d = \frac{D}{L}$$

# Distance of self-approach

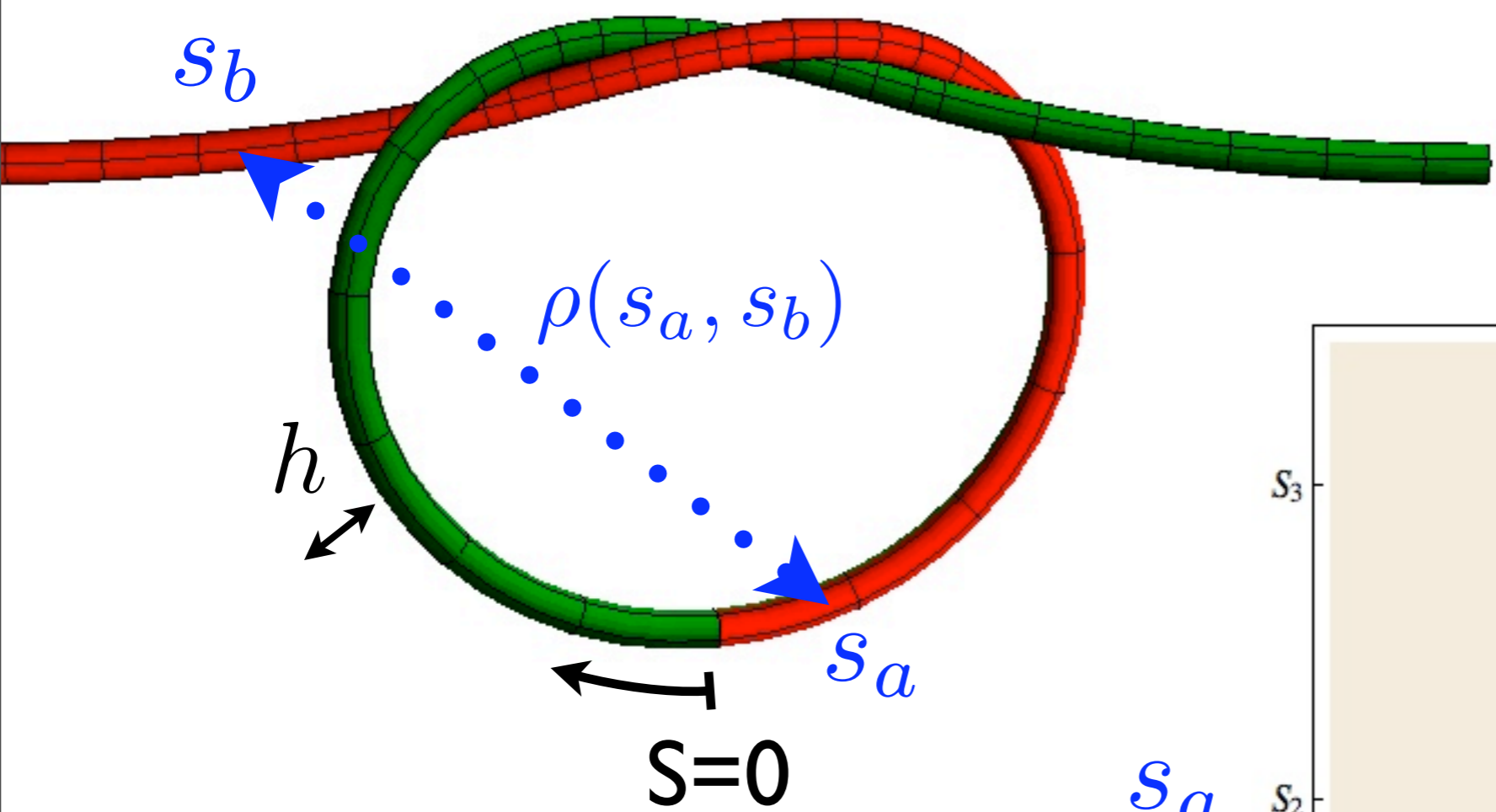


$$\rho(s_a, s_b) - 2h$$

$\rho(s_a, s_b) < 2h$

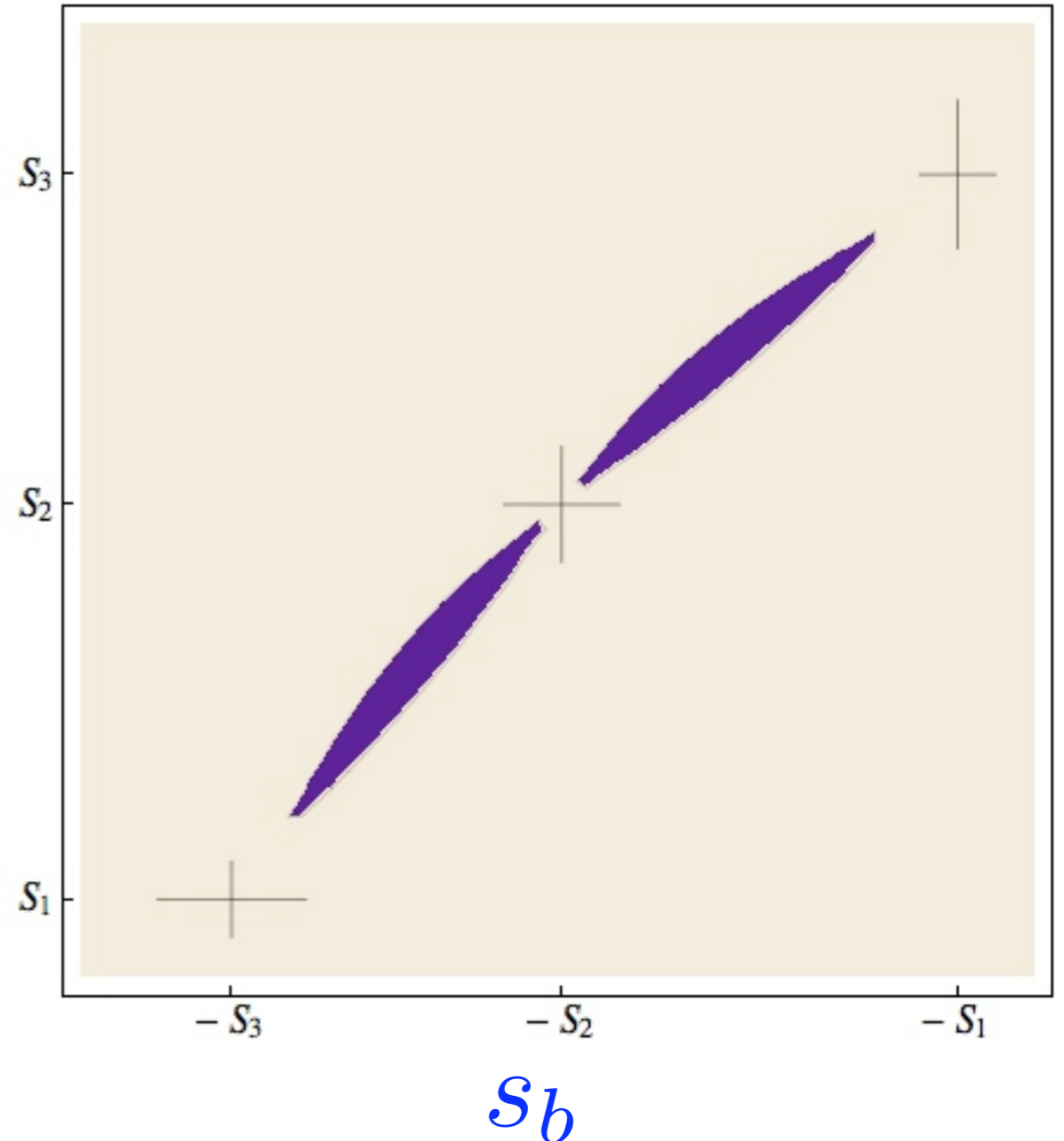


# Distance of self-approach

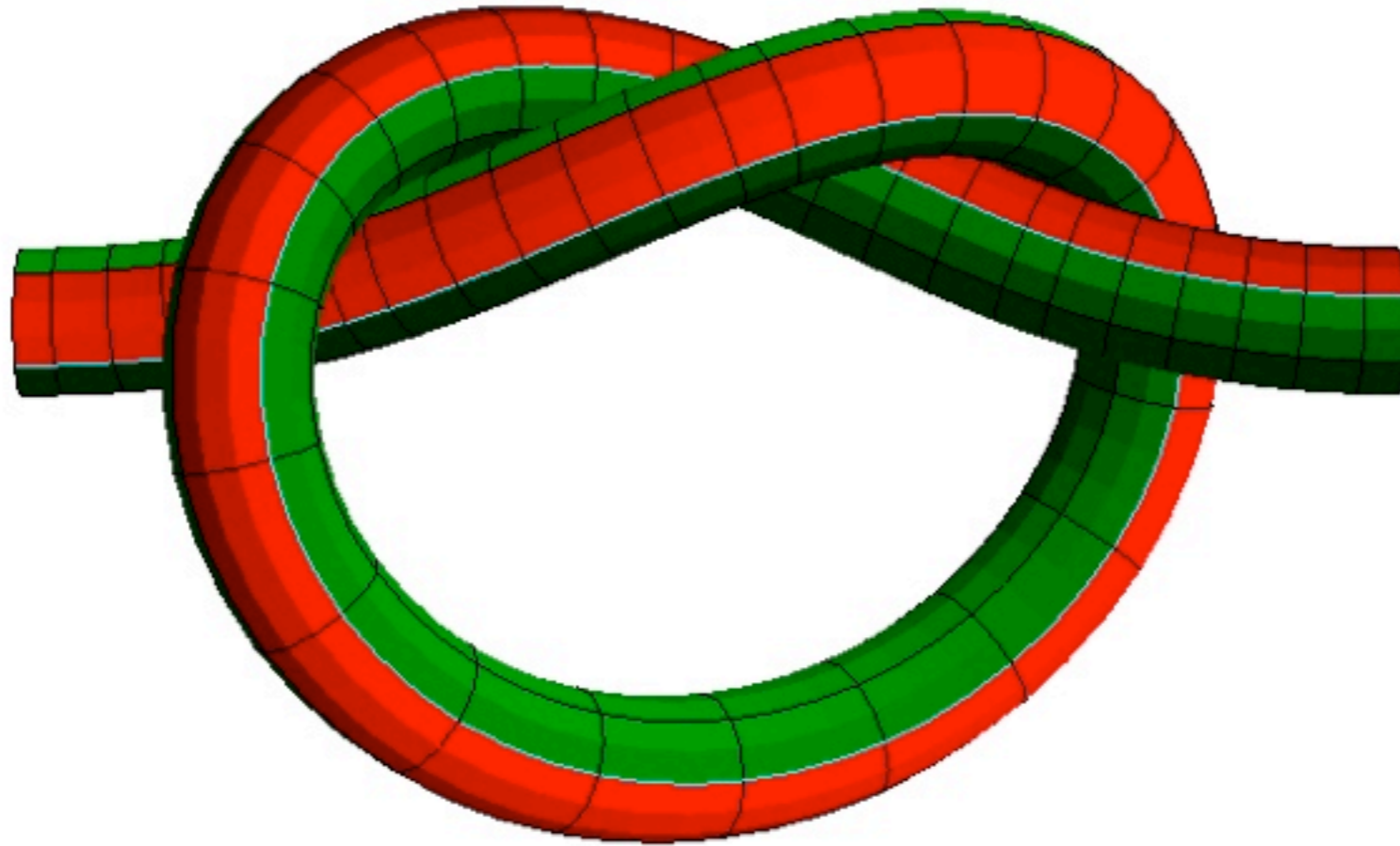


$$\rho(s_a, s_b) - 2h$$

$\rho(s_a, s_b) < 2h$

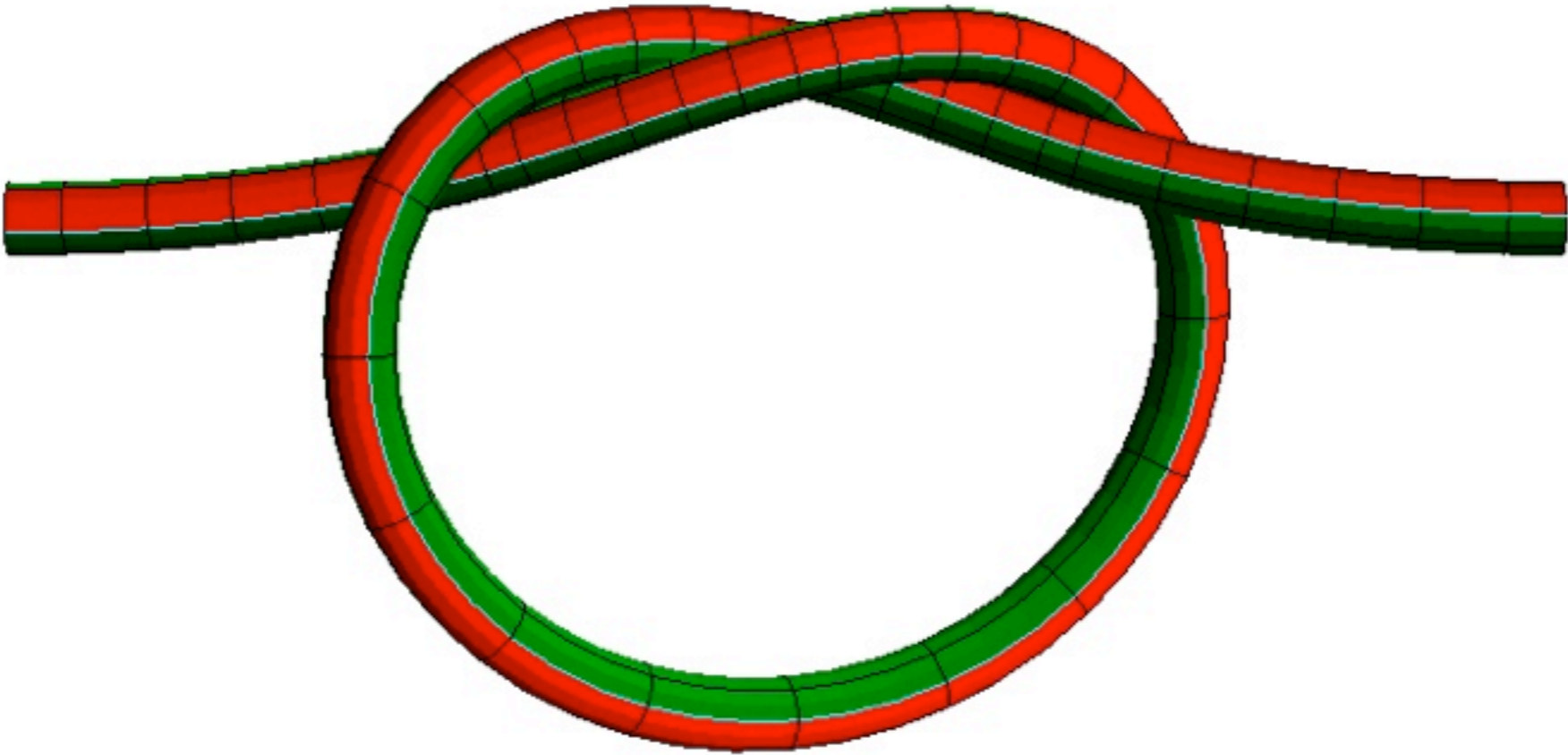


# Making the rod thinner

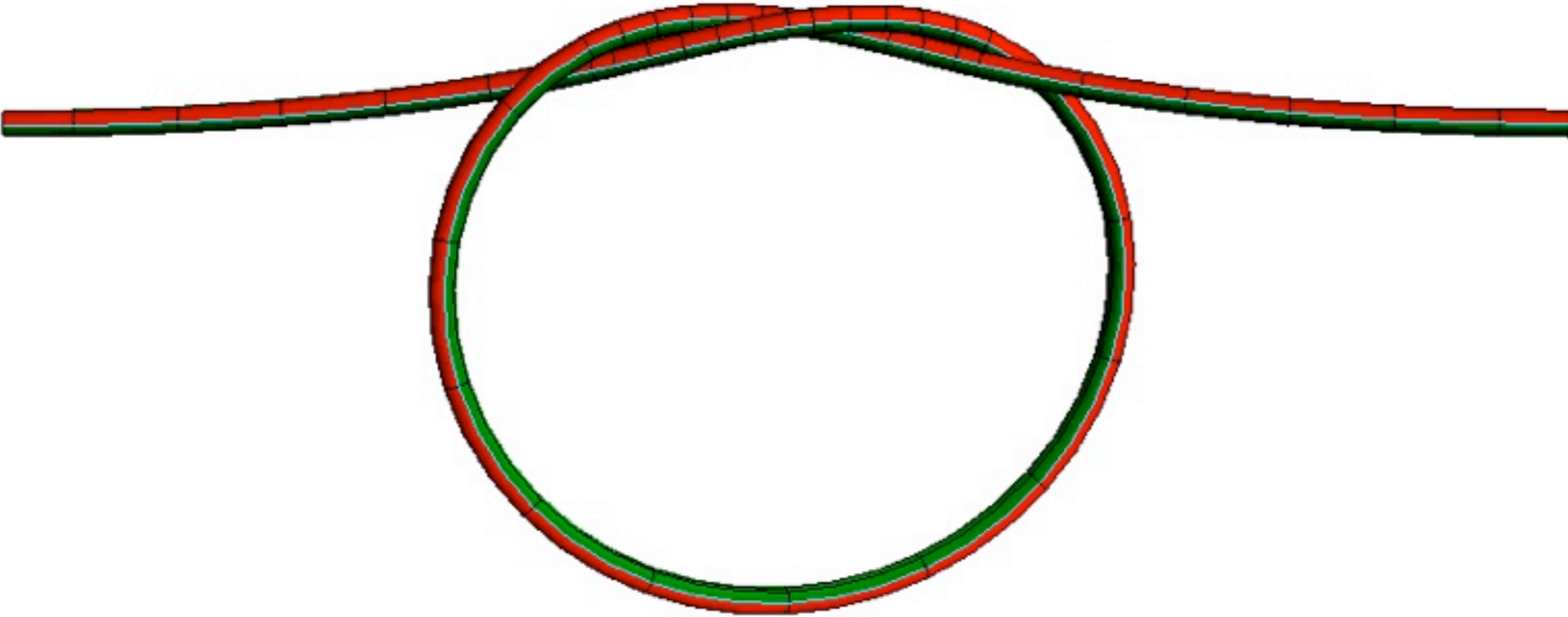




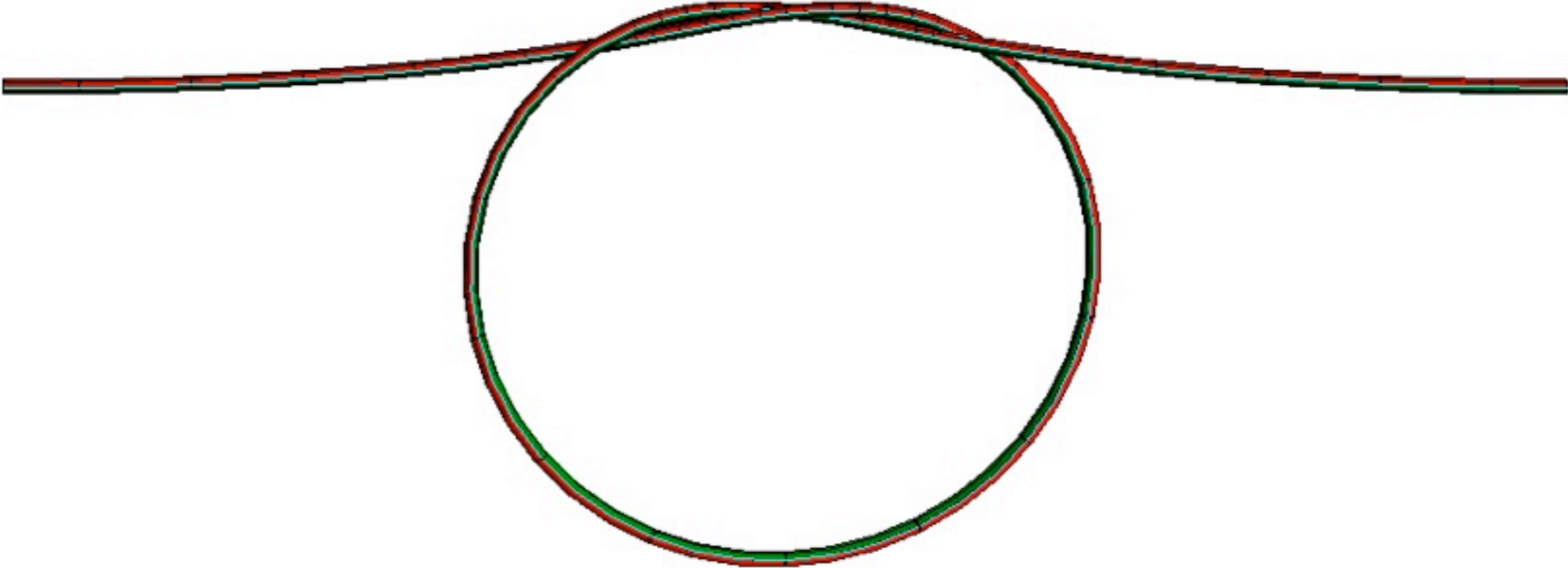
# Making the rod thinner



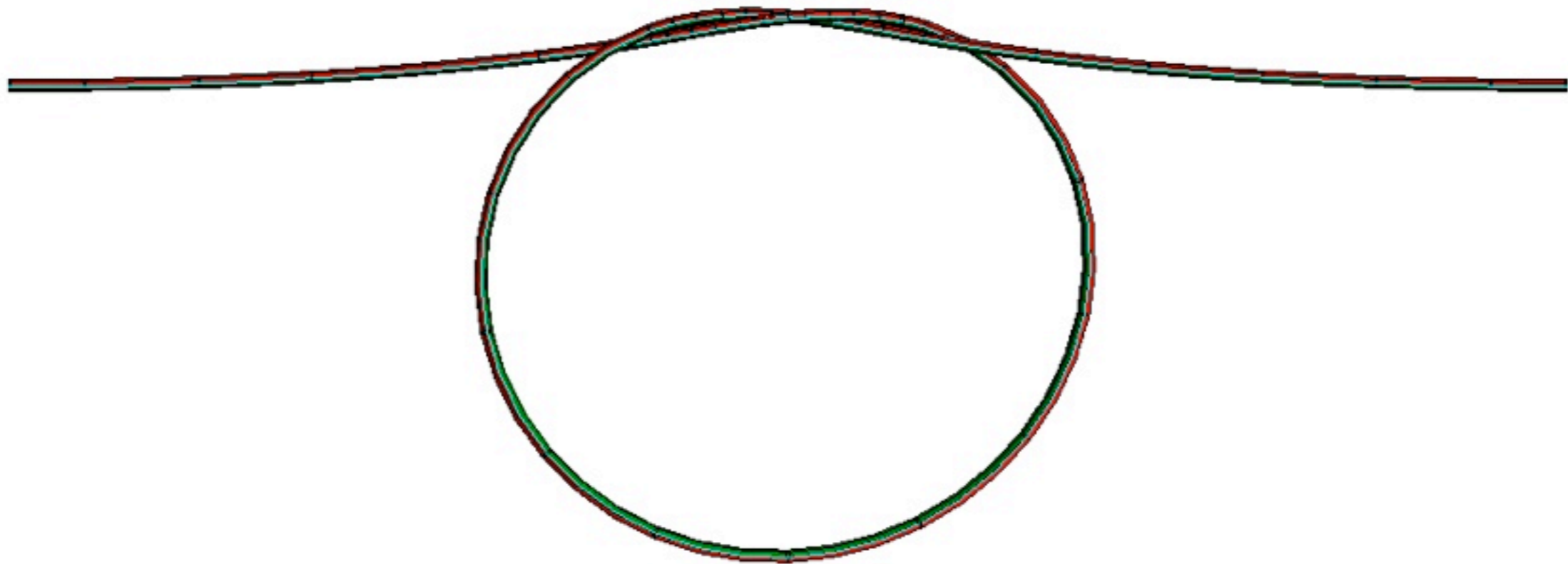
# Making the rod thinner



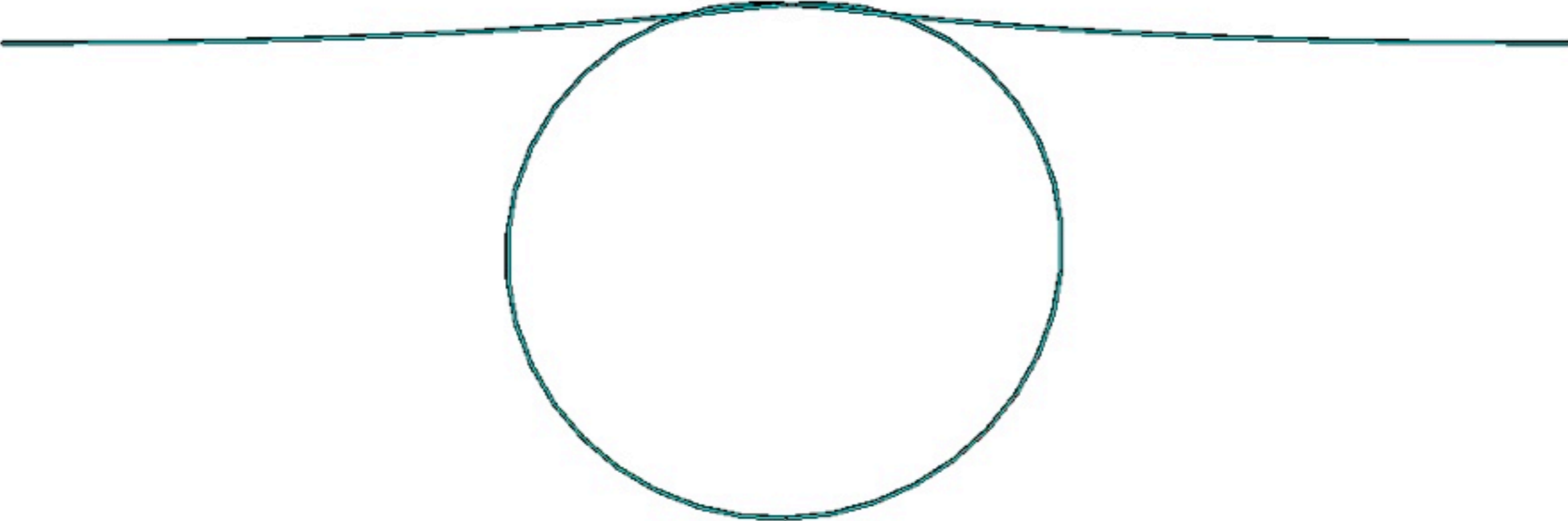
# Making the rod thinner



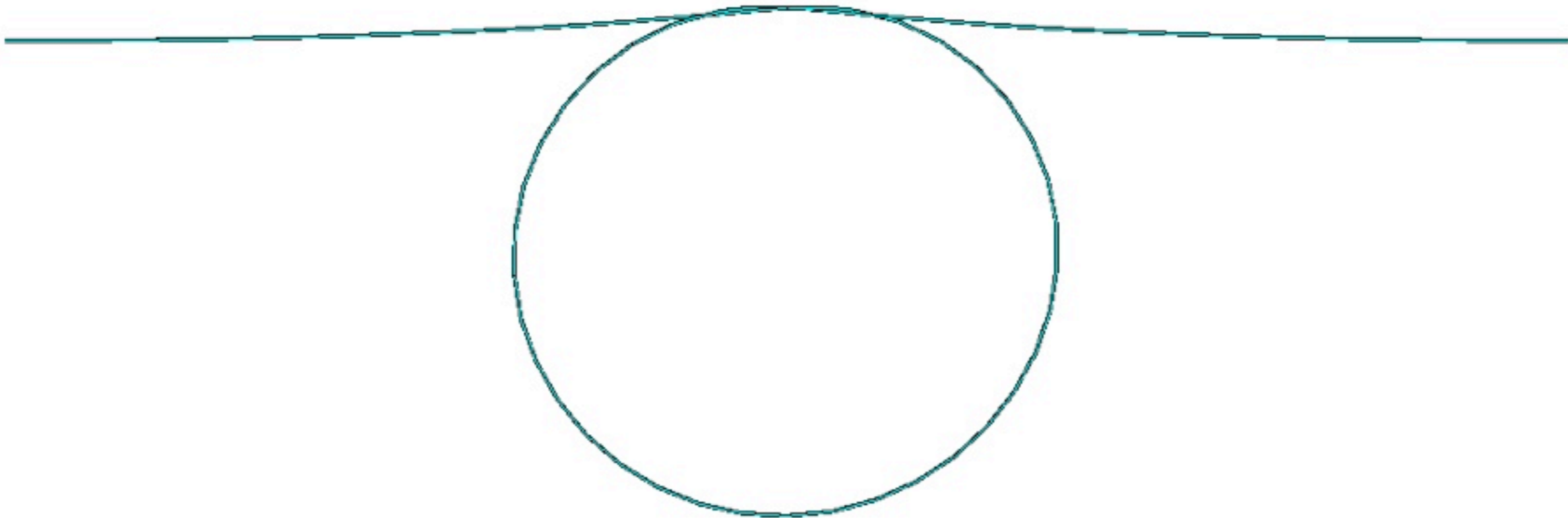
# Making the rod thinner



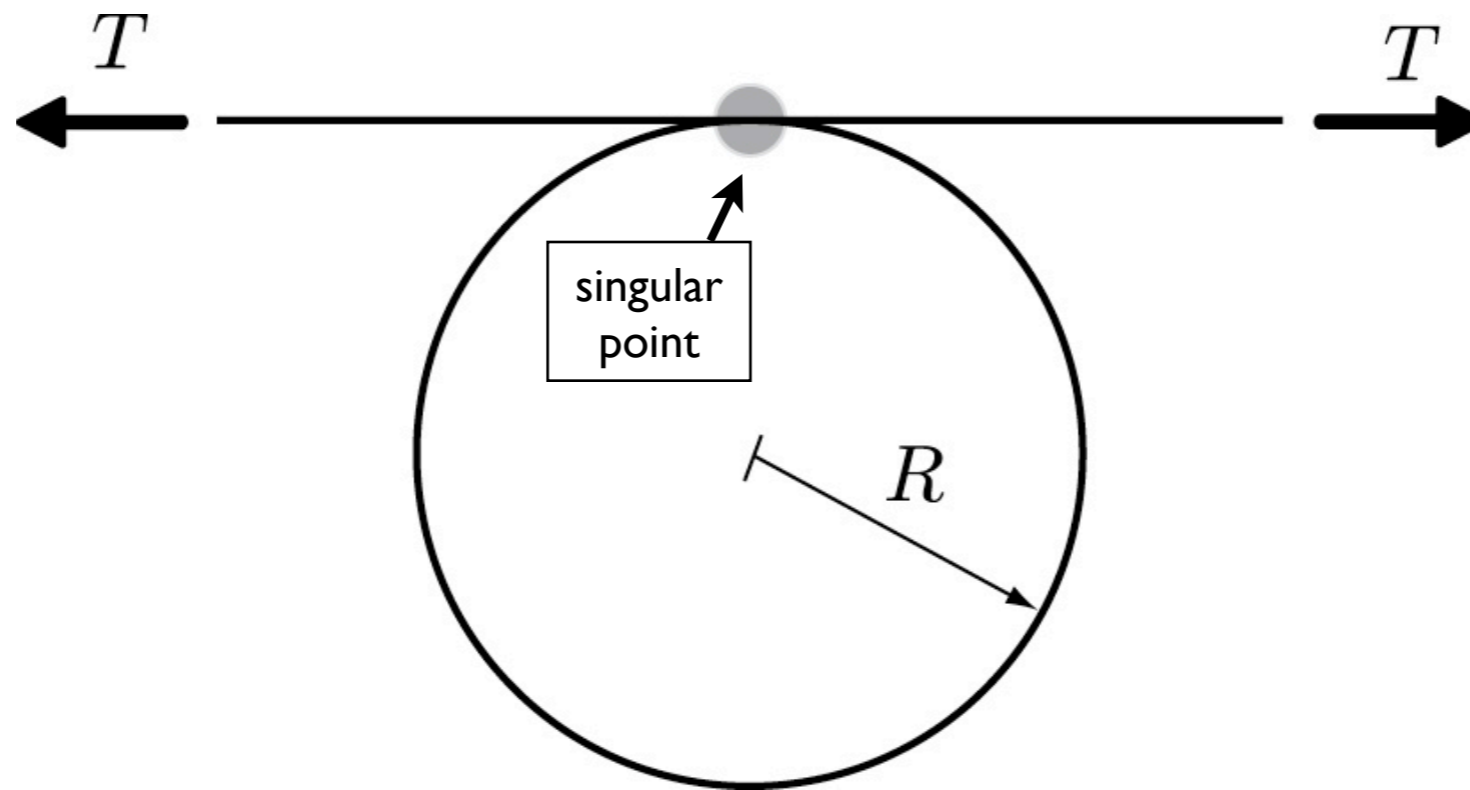
# Making the rod thinner



# Making the rod thinner

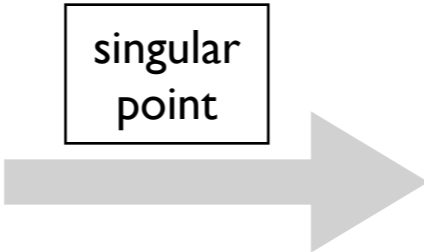


# Zero thickness limit

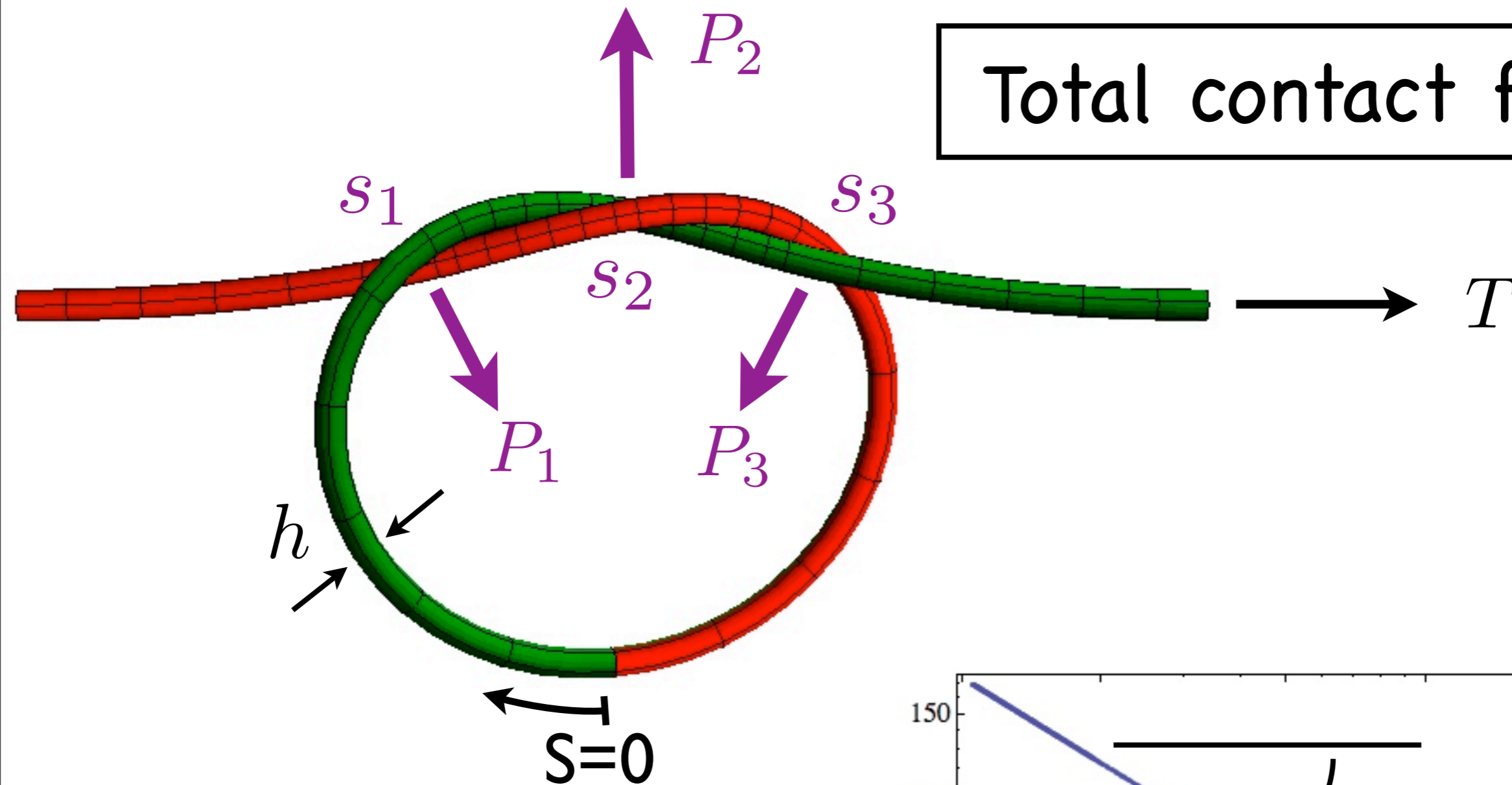


equilibrium :  $T = \frac{EI}{2R^2}$

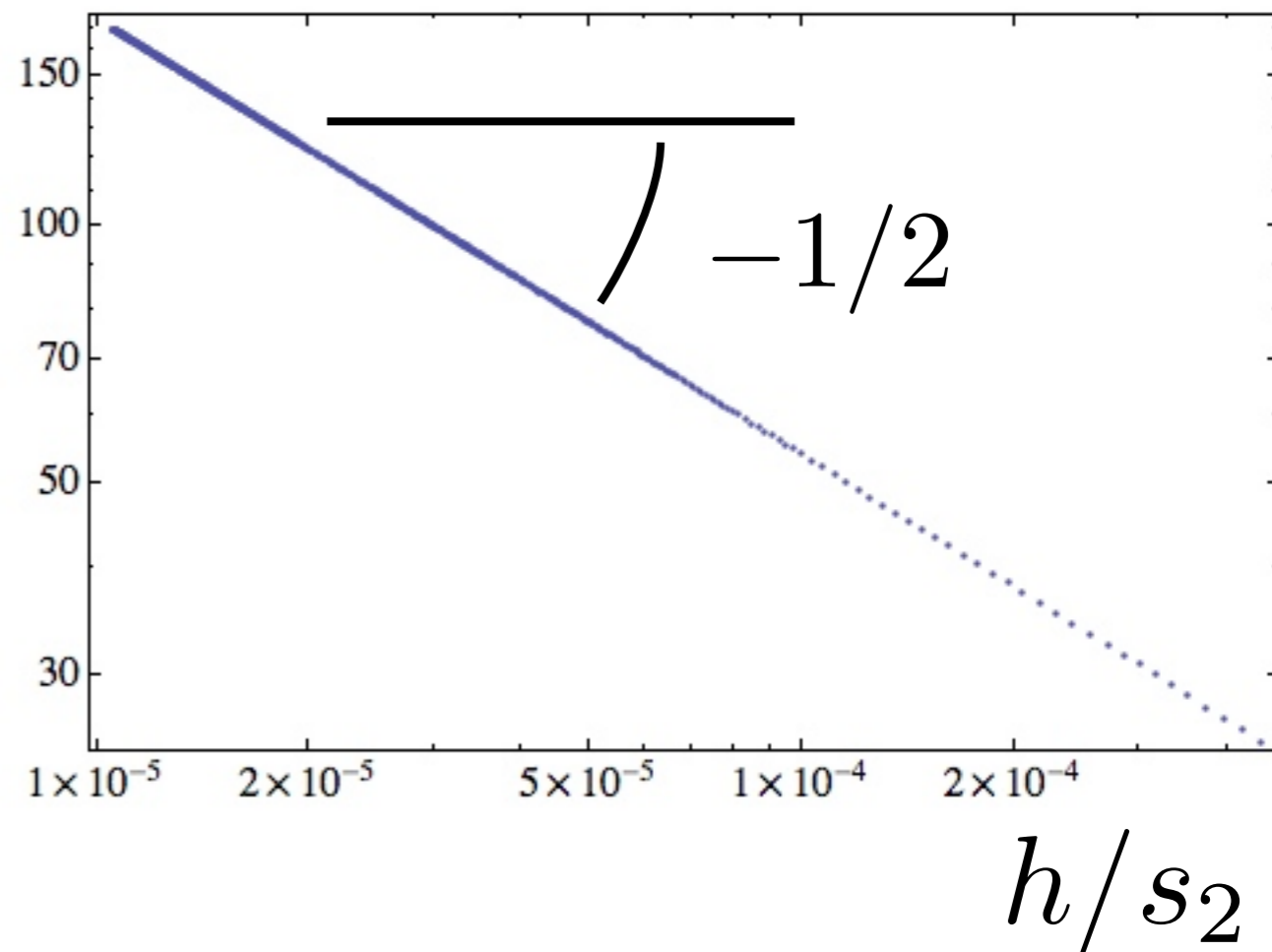
Arai et al (1999)

tensile force  $T$   bending moment  $\frac{EI}{R}$

Total contact force



$$\frac{1}{T} \sum_i P_i$$



$$\frac{1}{T} \sum_i P_i \simeq 0.55 (h/s_2)^{-1/2}$$



# Kirchhoff Equations

$$\left\{ \begin{array}{ll} \vec{F}' = -\vec{p} & \text{forces equil.} \\ \vec{M}' = \vec{F} \times \vec{t} & \text{moments equil.} \\ \vec{t}' = \frac{1}{EI} \vec{M} \times \vec{t} & \text{kinematics} \\ \vec{R}' = \vec{t} & \text{tangent def.} \end{array} \right.$$

$$' \equiv \frac{d}{ds}$$

---

$\vec{p}(s)$  ext. pressure

$\vec{M}(s)$  internal moment

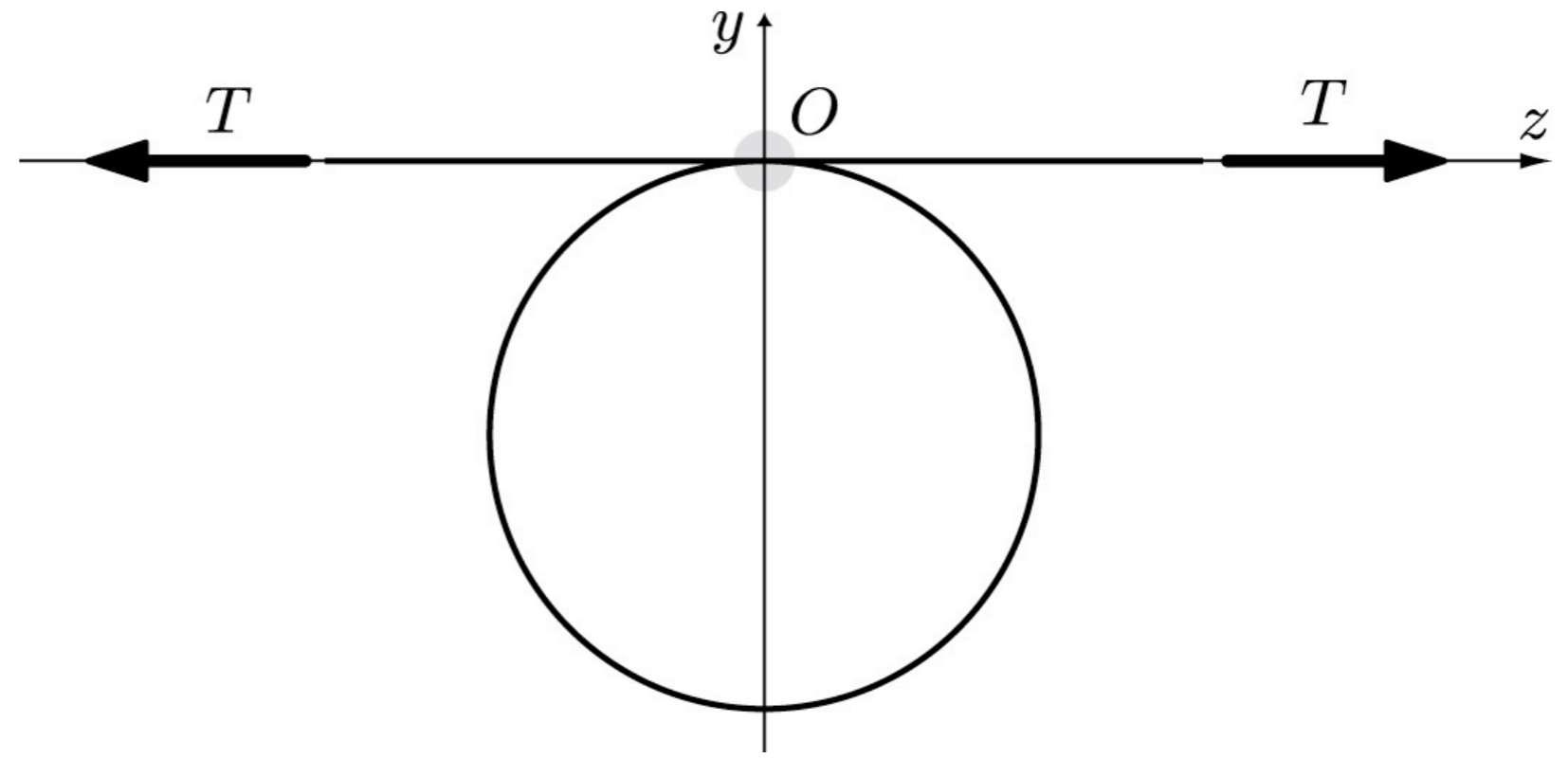
$\vec{F}(s)$  internal force

$\vec{R}(s)$  position

$\vec{t}(s)$  tangent

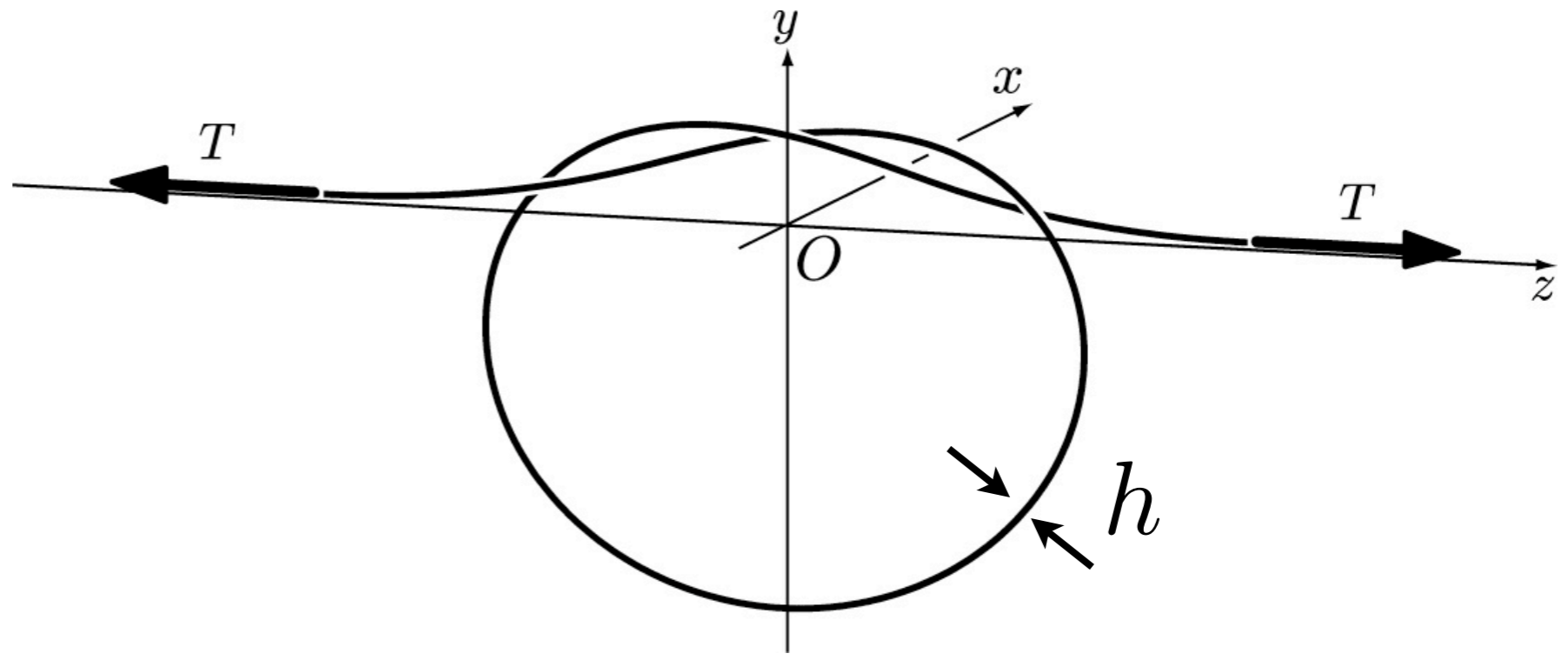
# Perturbative problem

$\epsilon = 0$   
 $(h = 0)$

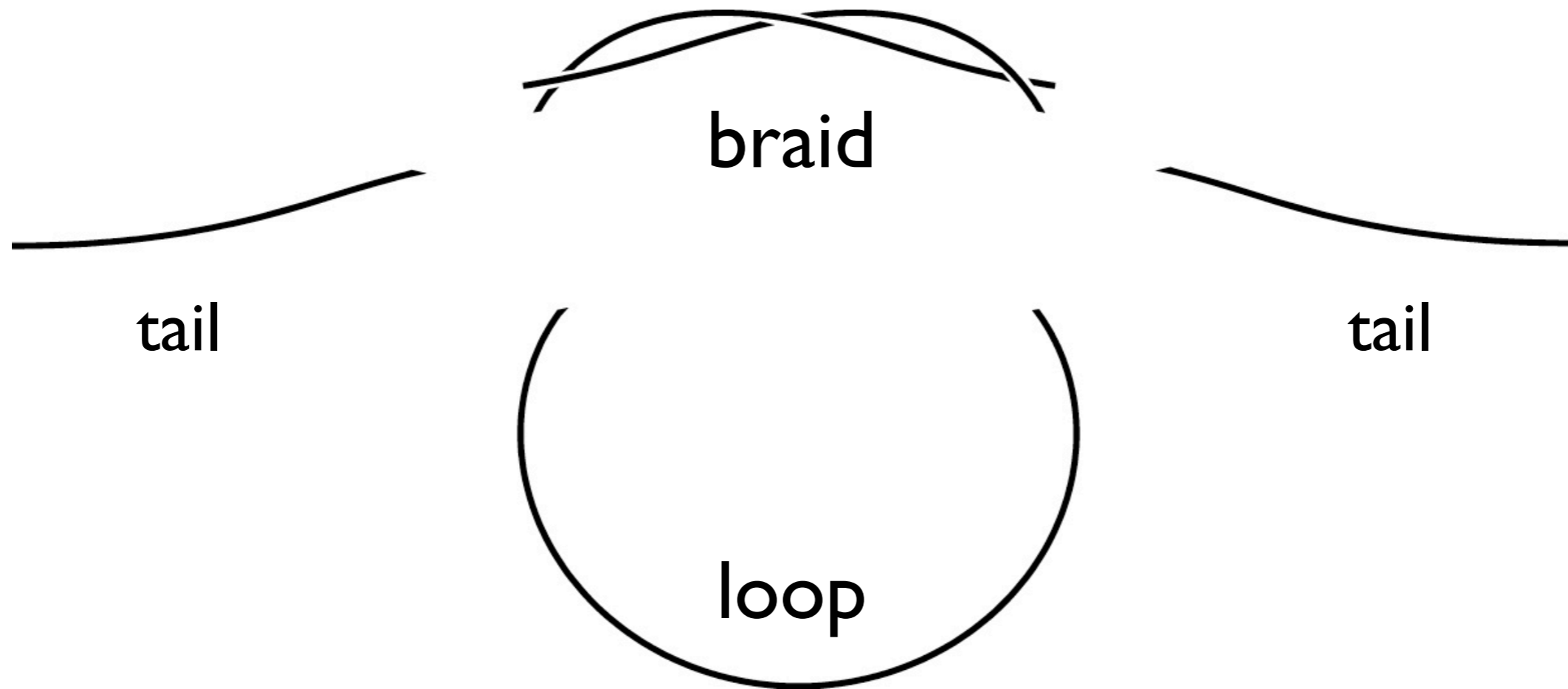


small parameter

$$\epsilon = \left( \frac{2h^2 T}{EI} \right)^{1/4} \ll 1$$

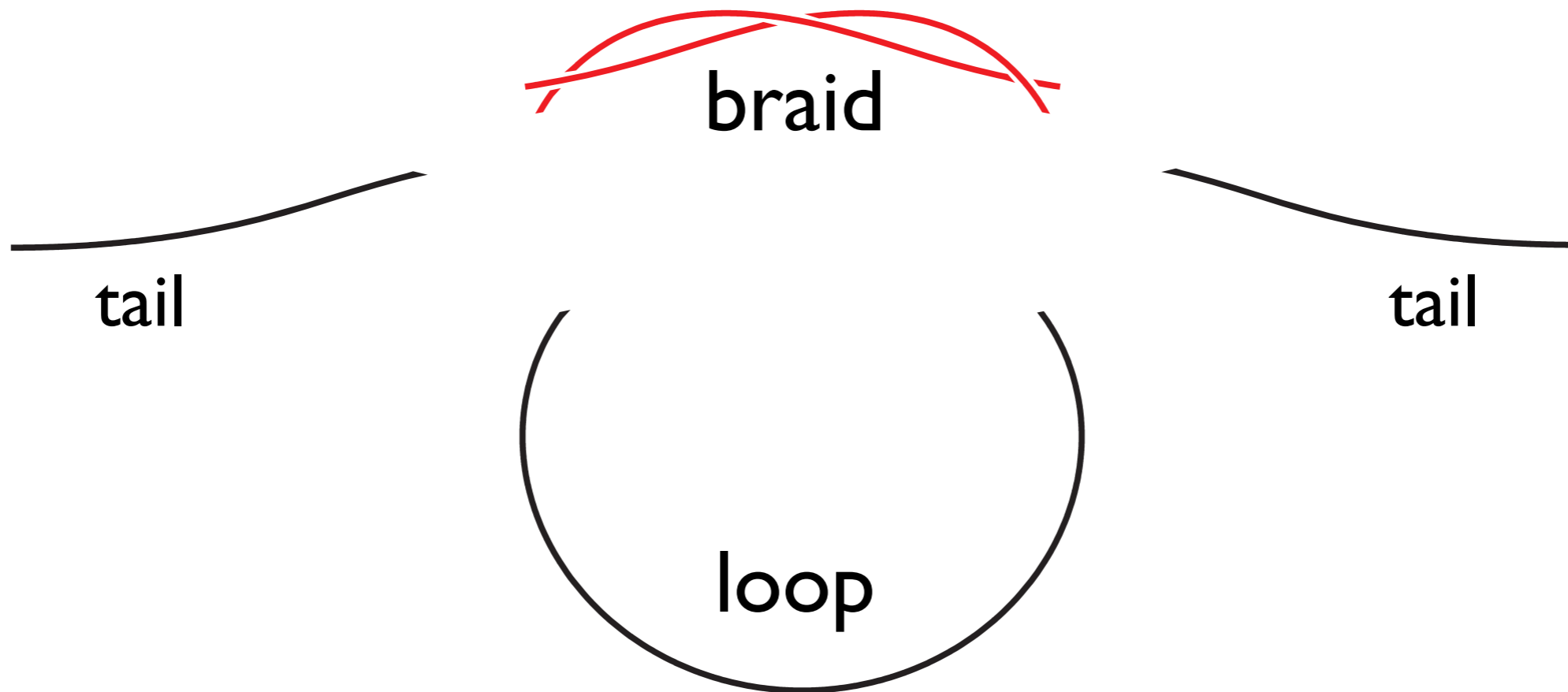


# Matched asymptotic expansions

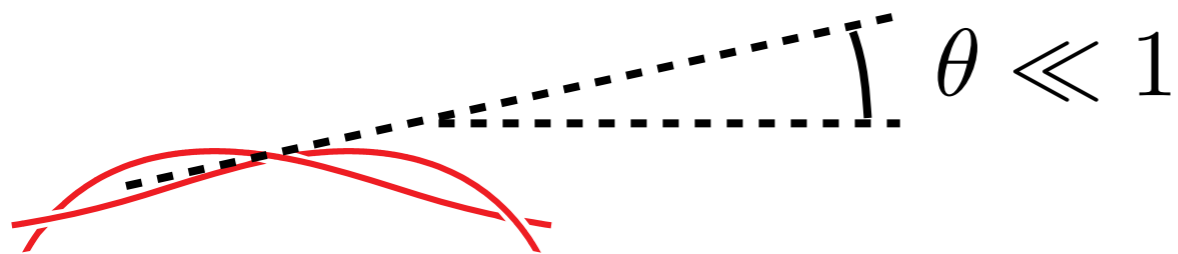


small parameter :  $\epsilon = \left( \frac{2h^2 T}{EI} \right)^{1/4} \ll 1$

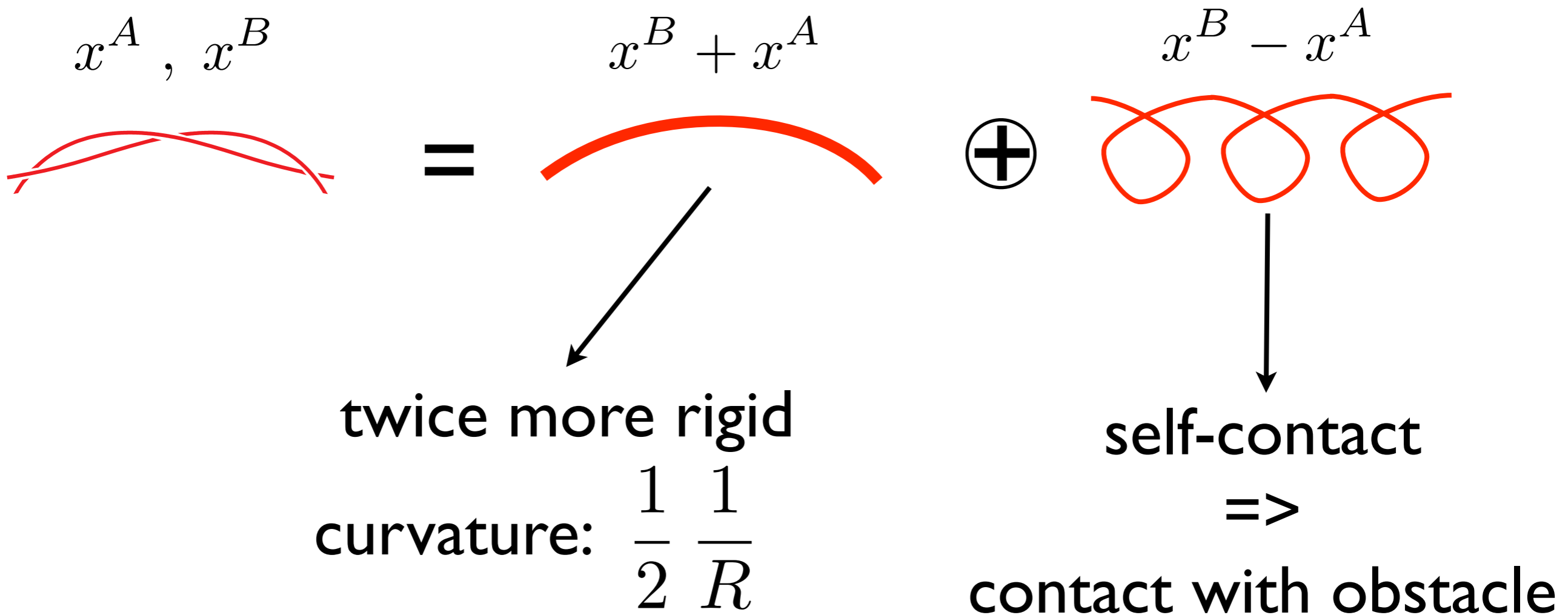
# Braid : self-contact zone



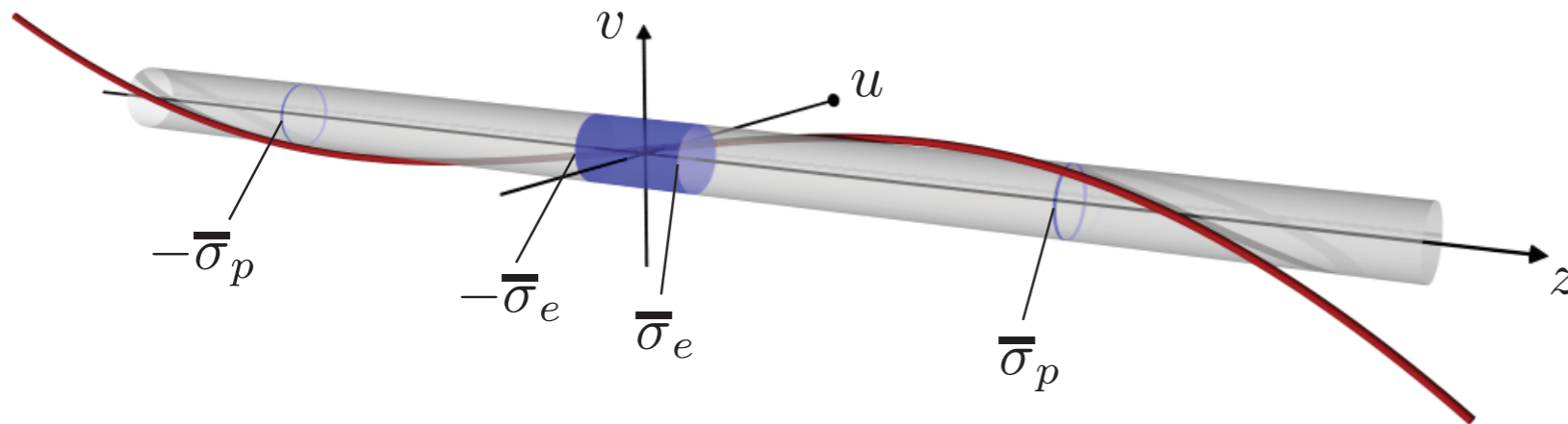
# Braid : linear superposition



small deflections  $\Rightarrow$  linear problem



# Braid : variational formulation



Kirchhoff equations  $\Rightarrow$  minimizing an energy

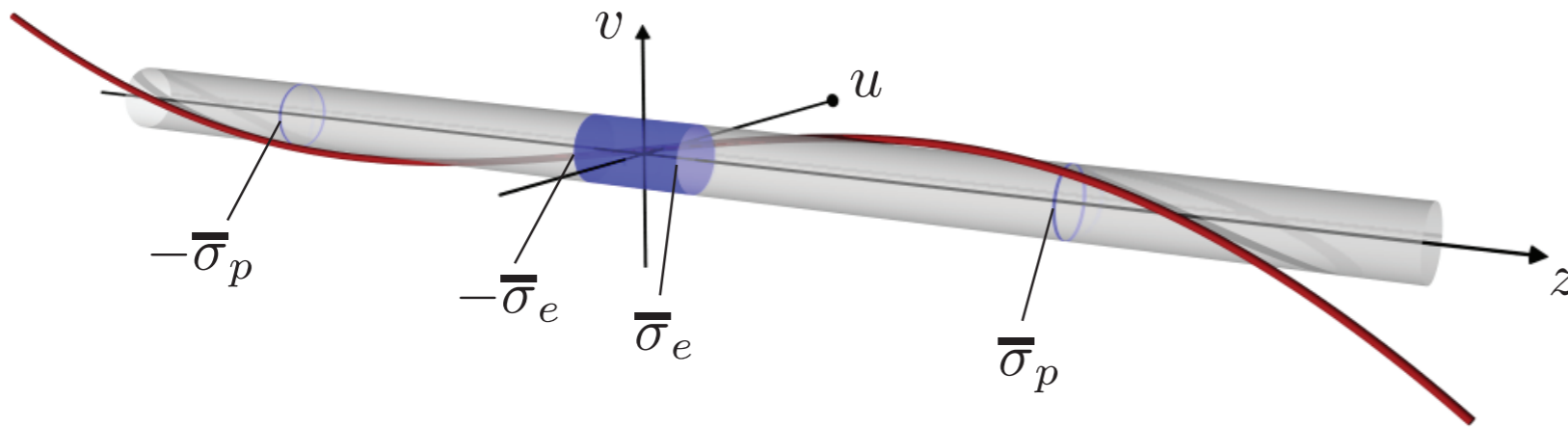
$$V = \frac{1}{2} \int_{-\infty}^{+\infty} \left( u''^2 + v''^2 \right) d\sigma + \underbrace{v'(+\infty) + v'(-\infty)}$$

work of external  
applied moments

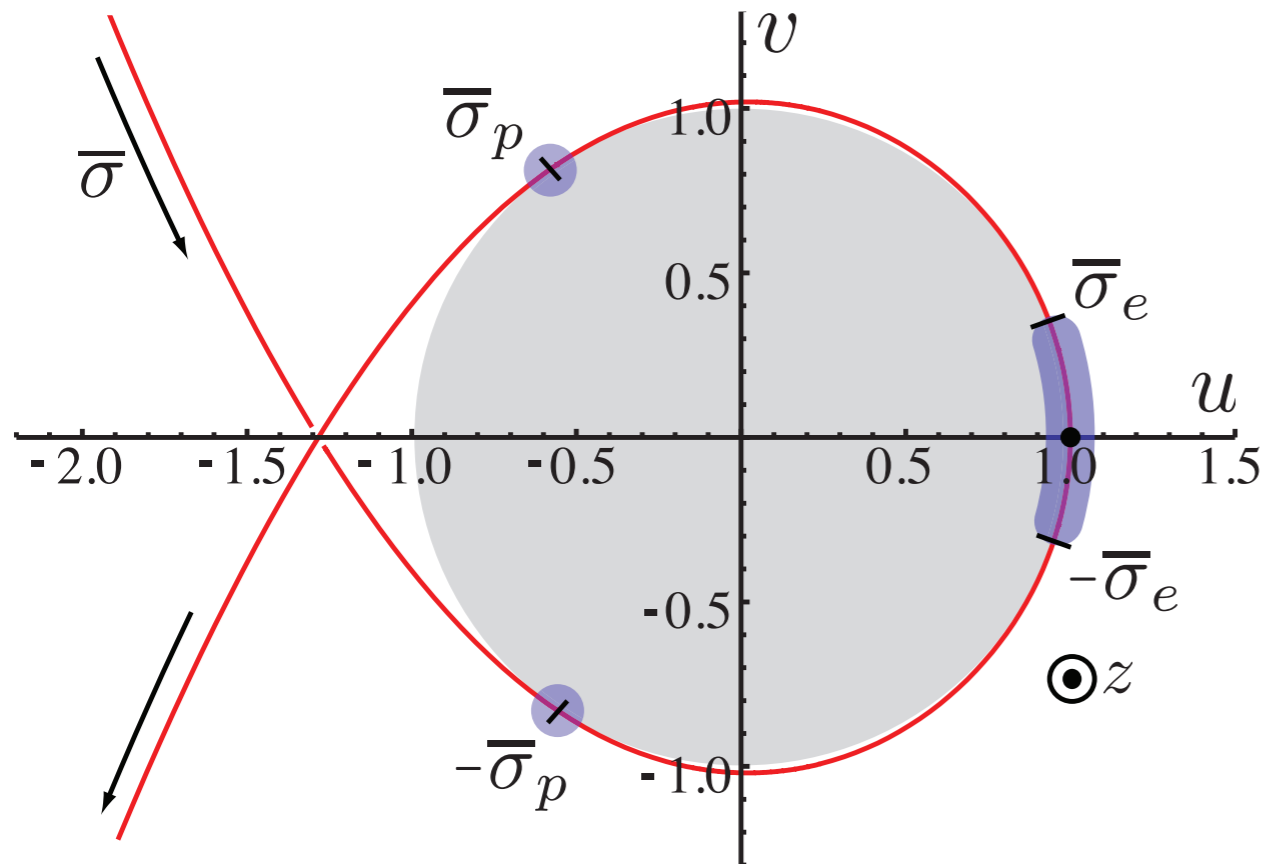
with constraint:

$$u^2(\sigma) + v^2(\sigma) \geq 1, \quad \forall \sigma$$

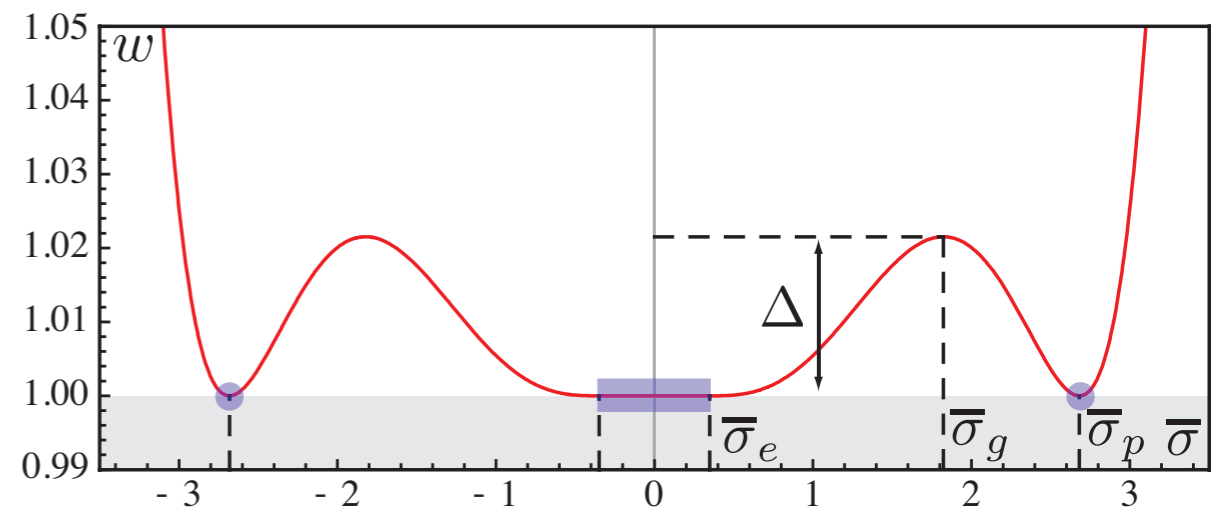
# Braid : contact topology



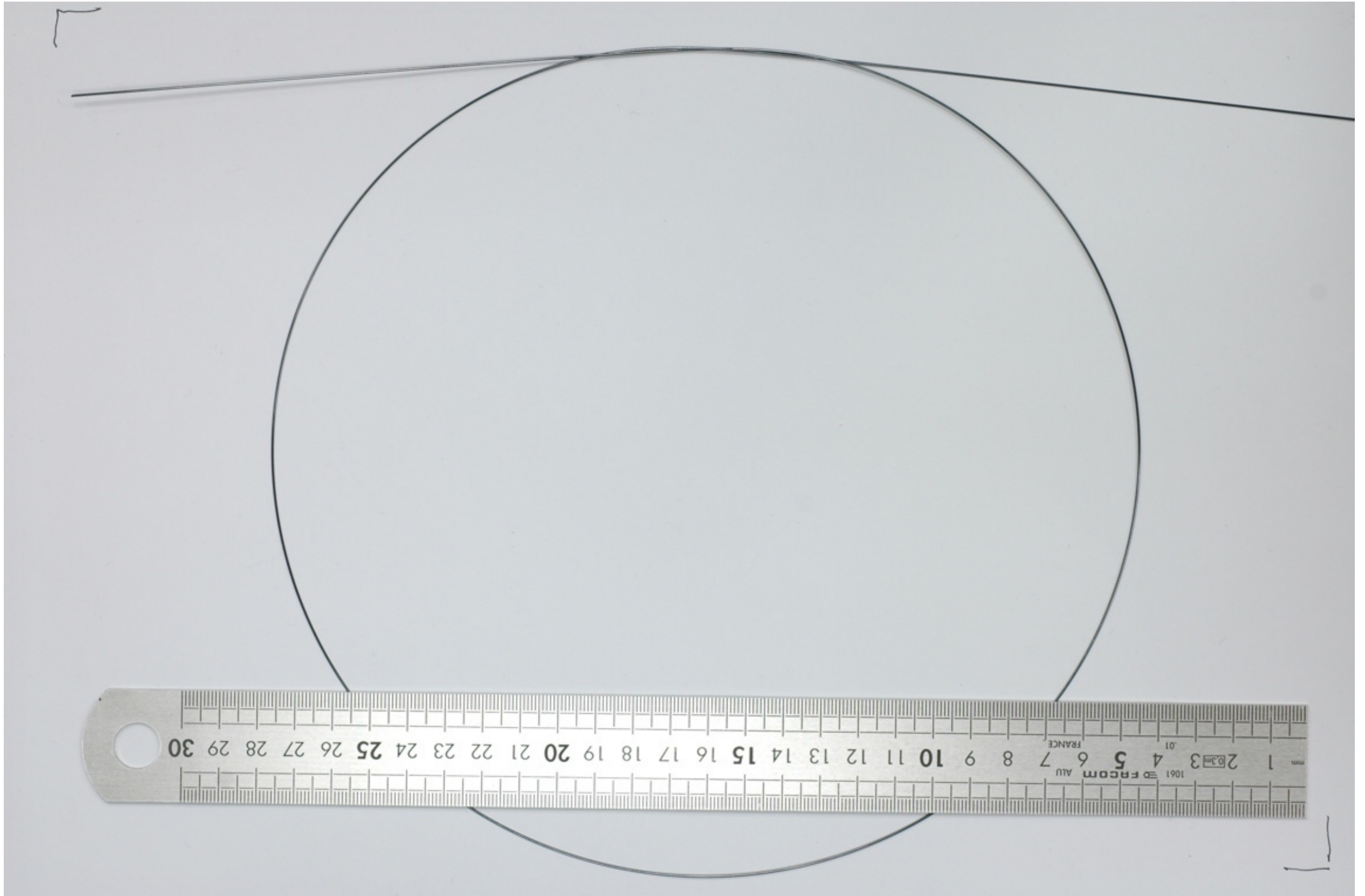
side view



inter-strand distance

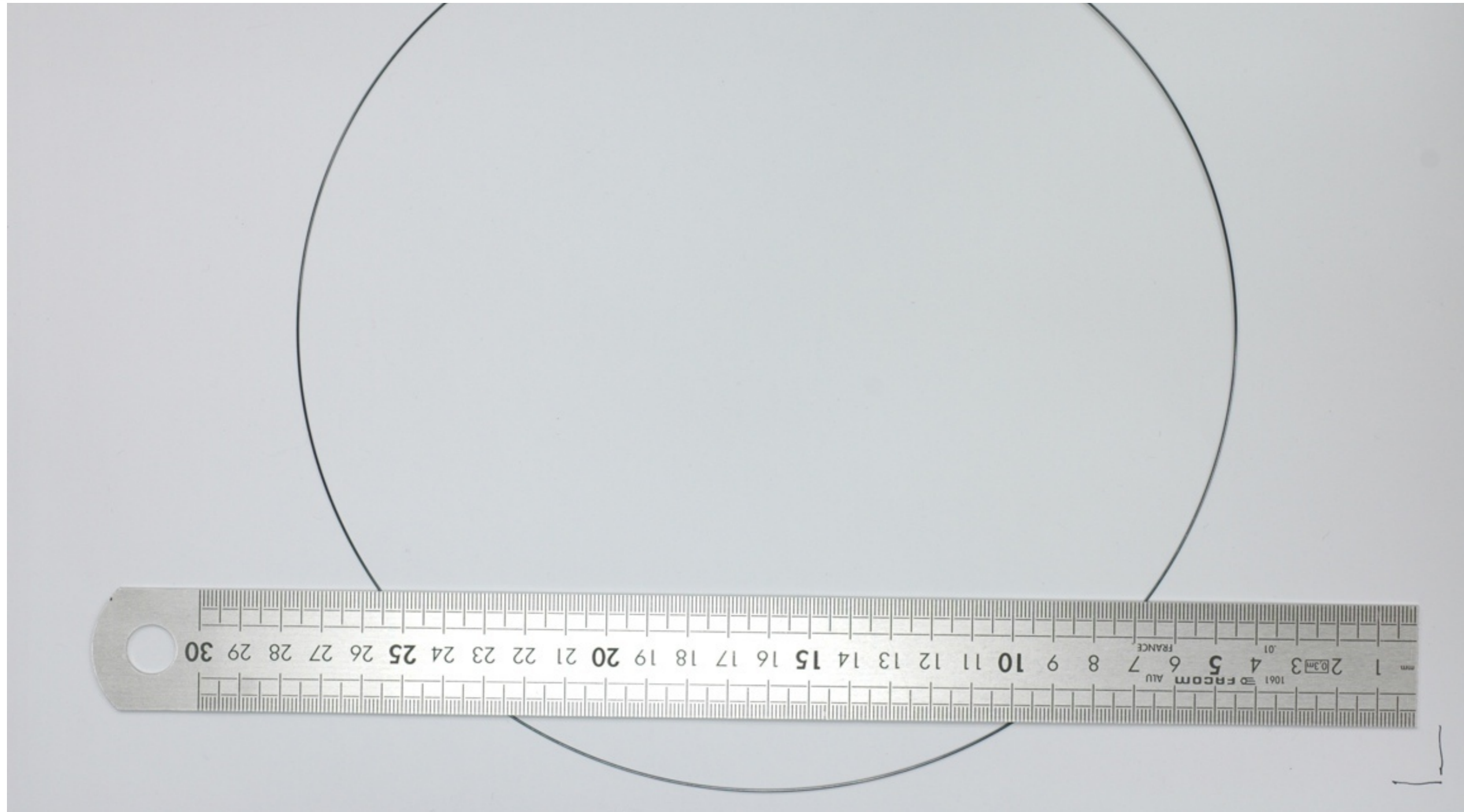


# Braid : contact topology

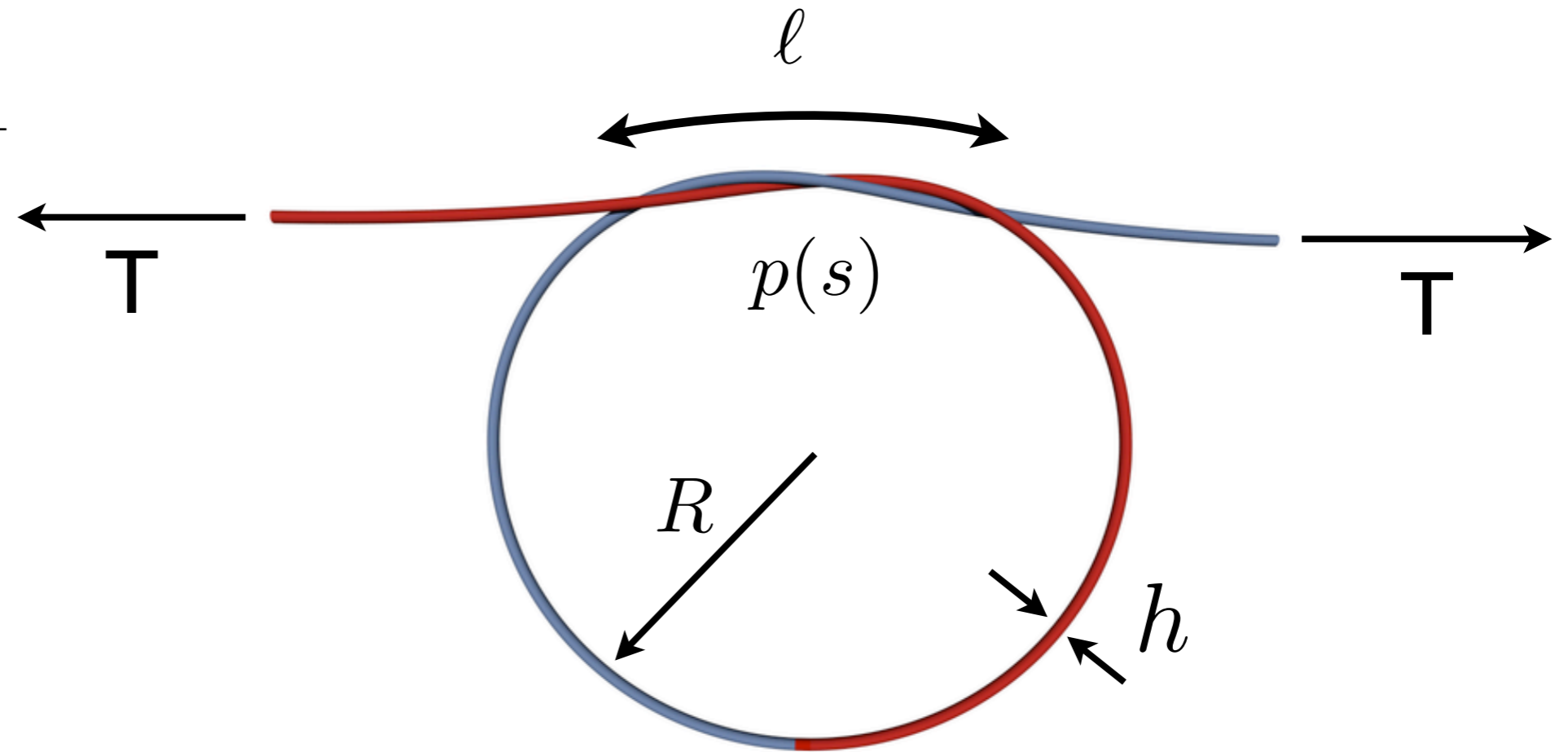




# Braid : contact topology



# Results



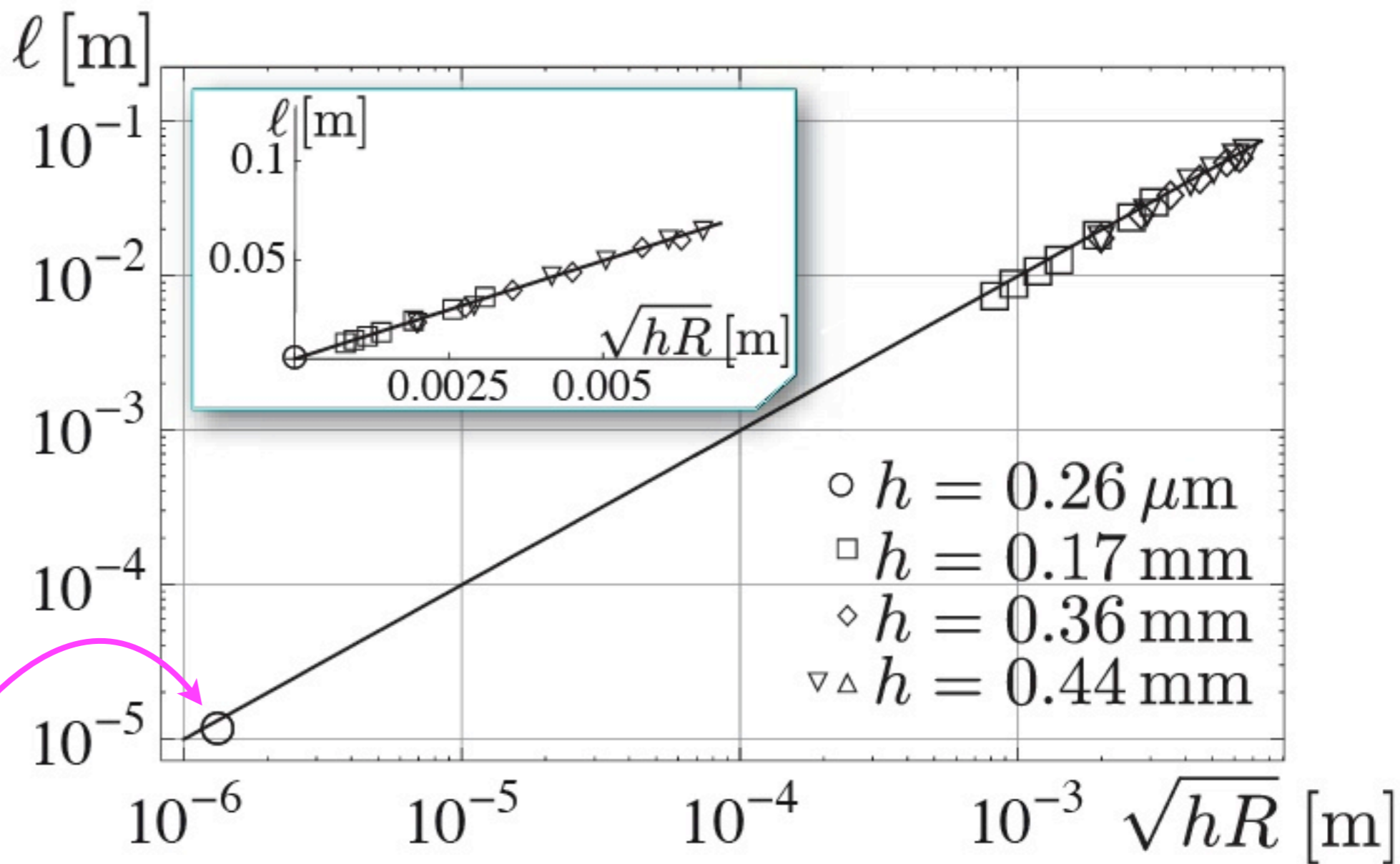
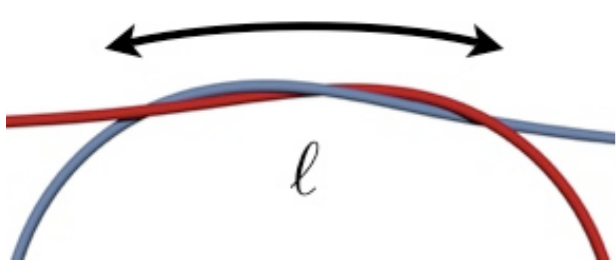
$$R = \sqrt{\frac{EI}{2T}}$$

$$\ell = 9.91 h^{1/2} (EI)^{1/4} T^{-1/4}$$

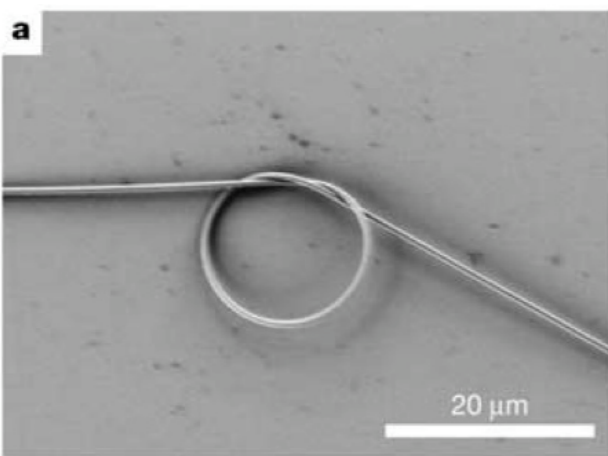
Contact pressure  $p(s)$

Total contact force  $P = \int_0^\ell p(s) ds = 0.82 h^{-1/2} (EI)^{1/4} T^{3/4}$

# Experiments

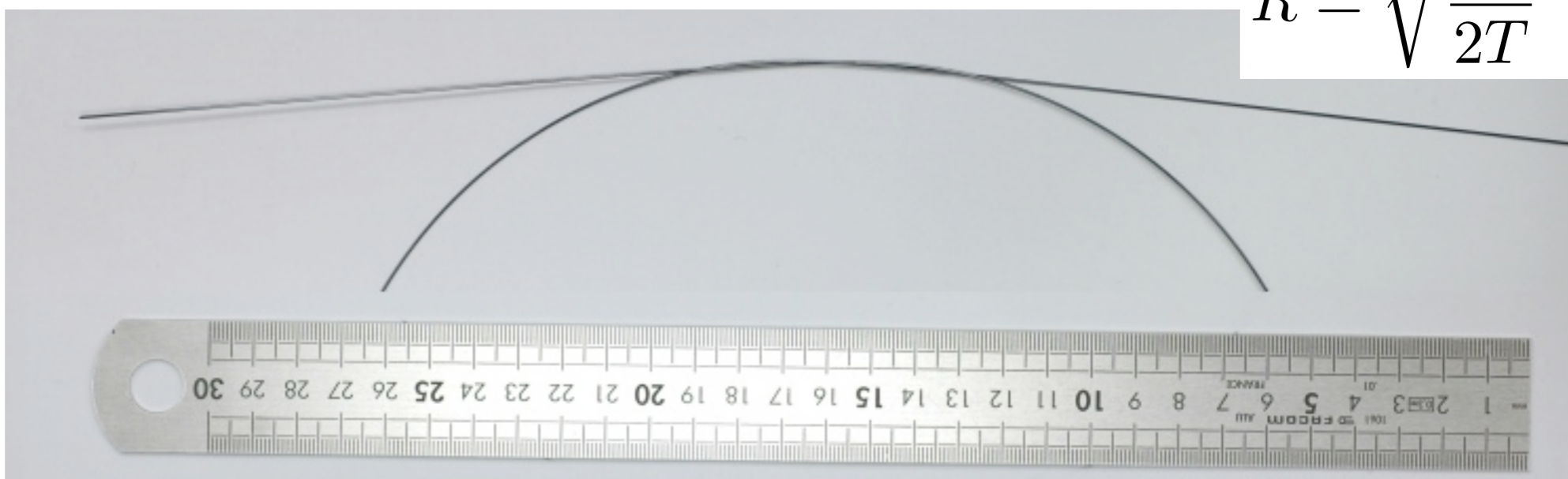


Tong et al., Nature 2003

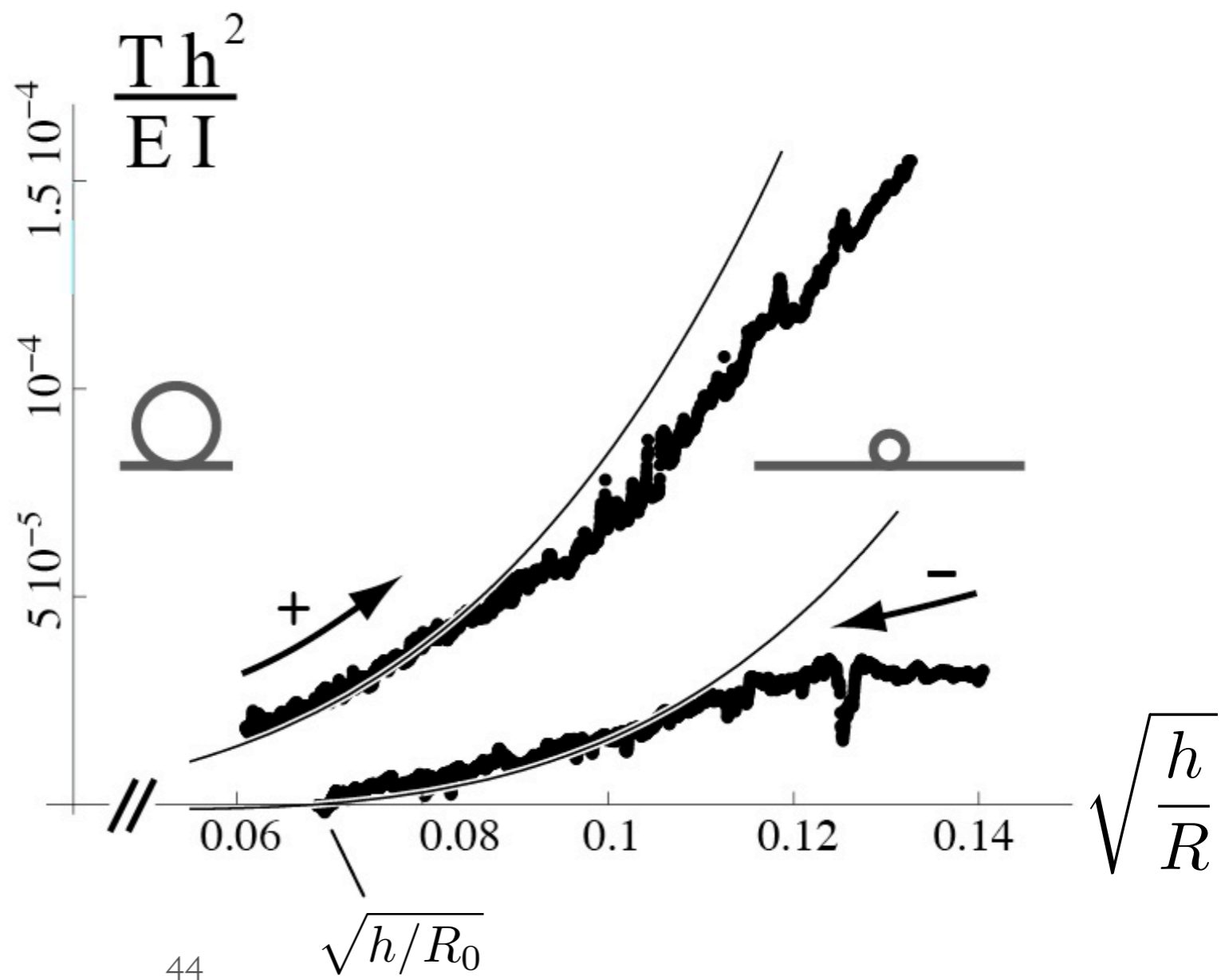
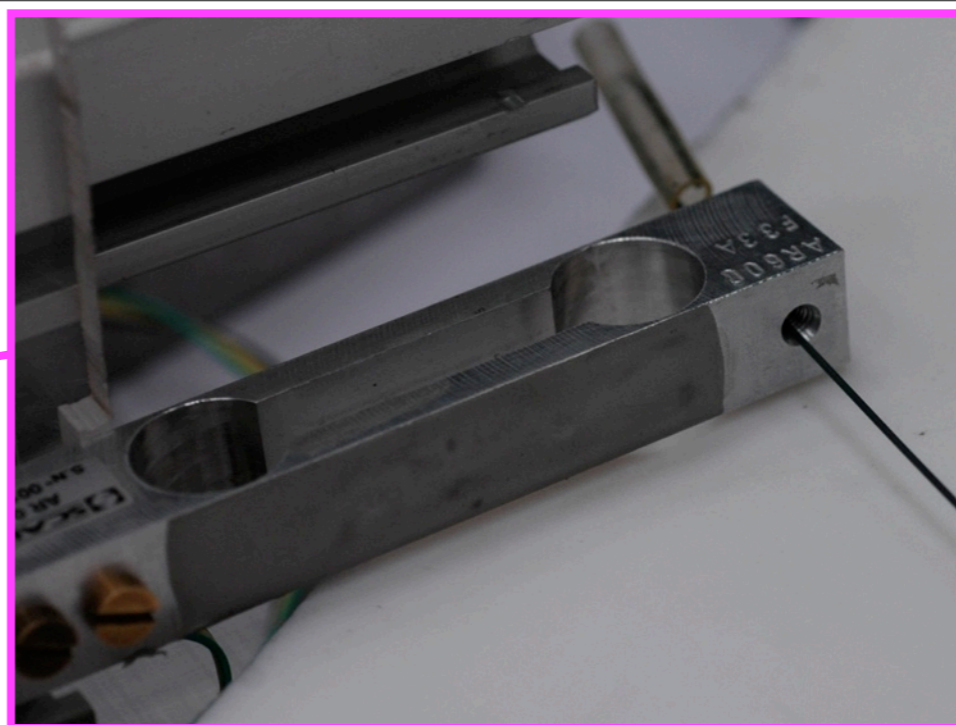
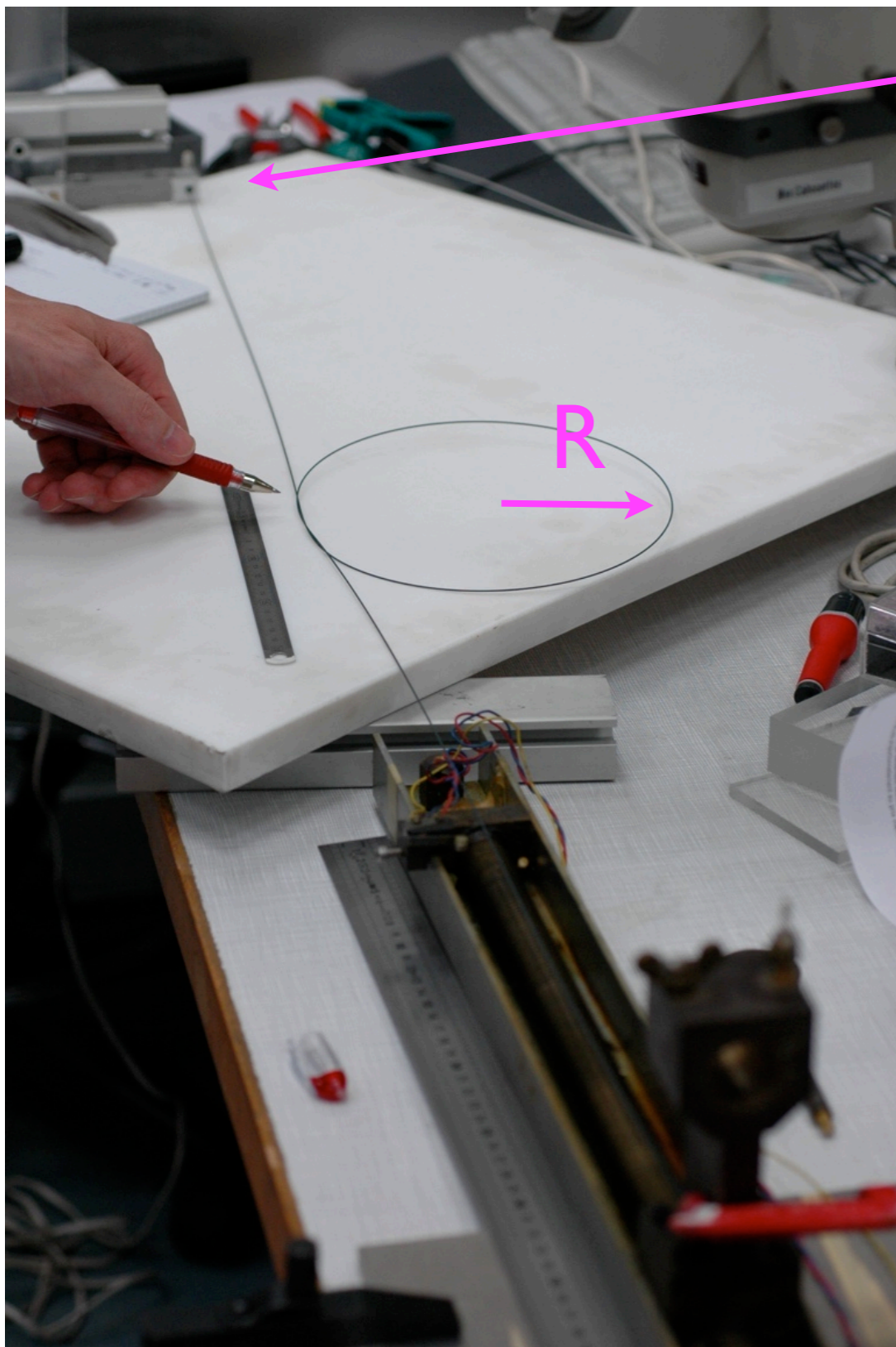


silica wire  
 $h = 1/2$  micron

$$R = \sqrt{\frac{EI}{2T}}$$

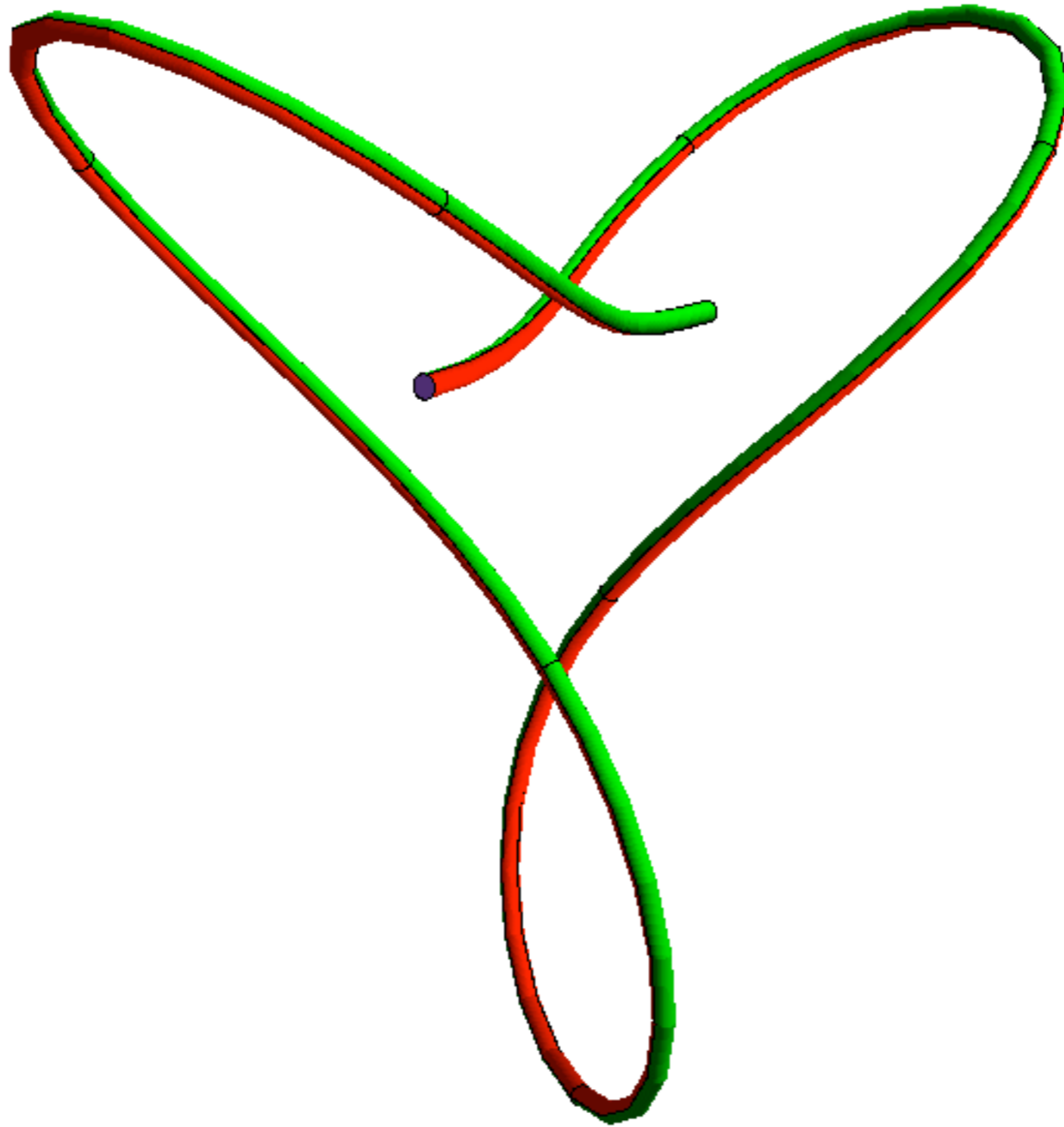


# Experiments



do stable open trefoil knotted configurations exist ?

Langer + & Singer (J. London Math. Soc) 1984 conjecture that no.  
(for closed configurations though)



do stable open trefoil knotted configurations exist ?

Langer + & Singer (J. London Math. Soc) 1984 conjecture that no.  
(for closed configurations though)

# Fin

[www.lmm.jussieu.fr/~neukirch](http://www.lmm.jussieu.fr/~neukirch)

B. Audoly, N. Clauvelin, and S. Neukirch. *Physical Review Letters*, 99 (2007) 164301.

N. Clauvelin, B. Audoly, and S. Neukirch. *Journal of the Mechanics and Physics of Solids*, 57 (2009) 1623–1656.

# Variational formulation

$$E = \int_{-\infty}^{+\infty} \left( \frac{B}{2} \kappa^2 + \frac{C}{2} \tau^2 \right) ds + TD_{\infty} - UR_{\infty},$$

where  $\kappa$  and  $\tau$  stand for the curvature  
and the twist of the rod.

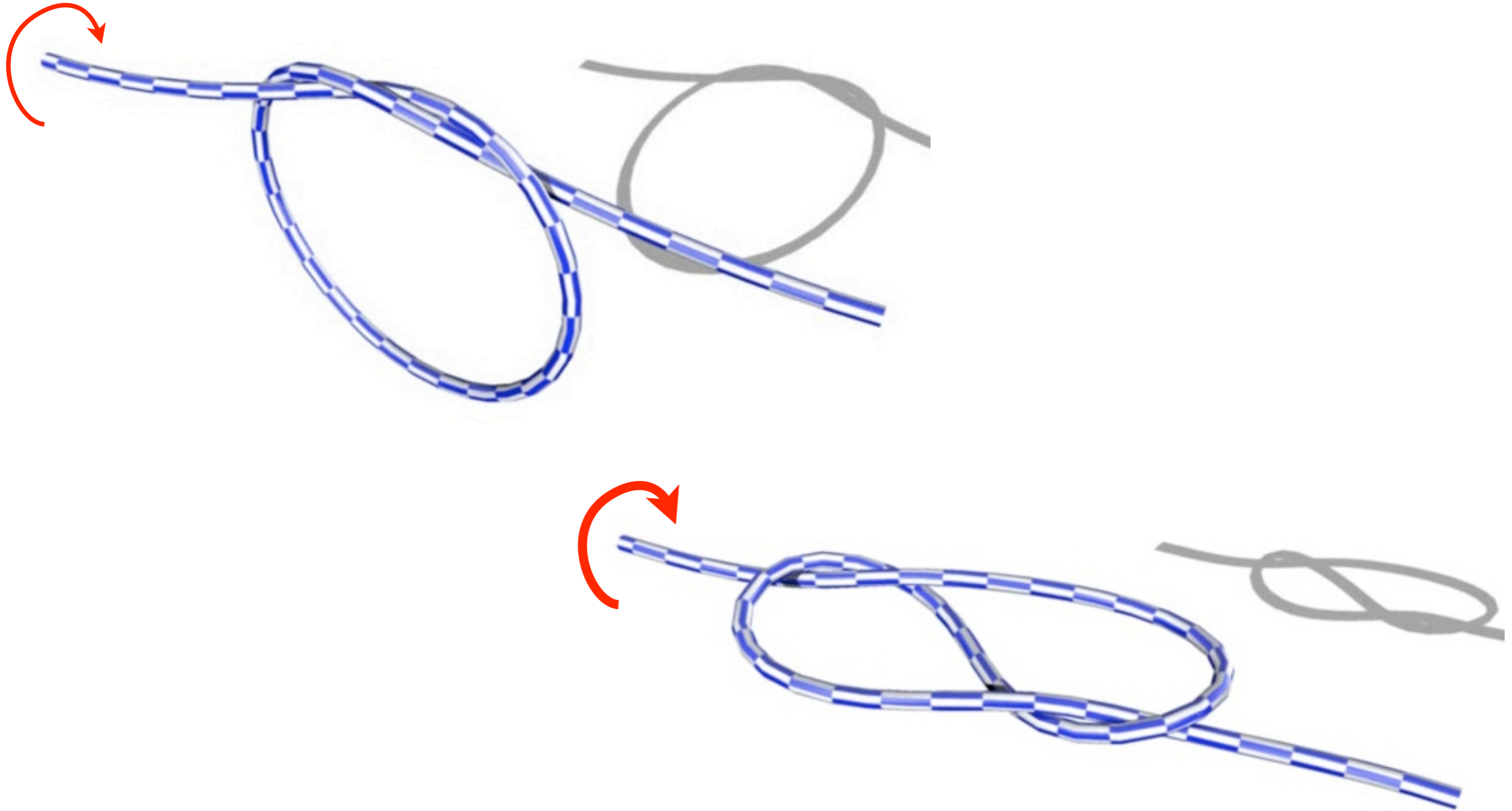
$$\kappa = |\mathbf{t}'(s)|.$$

$$|\mathbf{r}(s_1) - \mathbf{r}(s_2)| \geq 2h,$$

for any  $s_1$  and  $s_2$  such that  $|s_1 - s_2| > 4h$ .



# Twist Instability

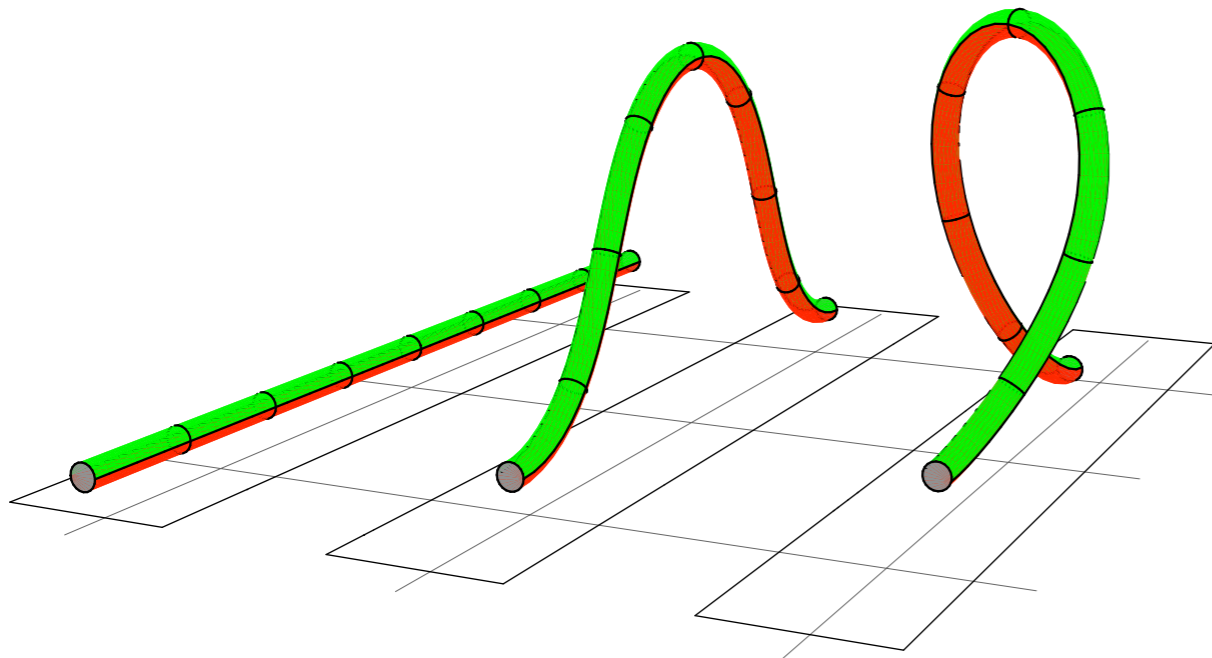


**numerical simulations** : M. Bergou, M. Wardetzky, S. Robinson, B. Audoly, and E. Grinspun.

*ACM Transactions on Graphics (SIGGRAPH), 2008*

# Twisted rods : the ideal case

if rod is uniform, isotropic, naturally straight

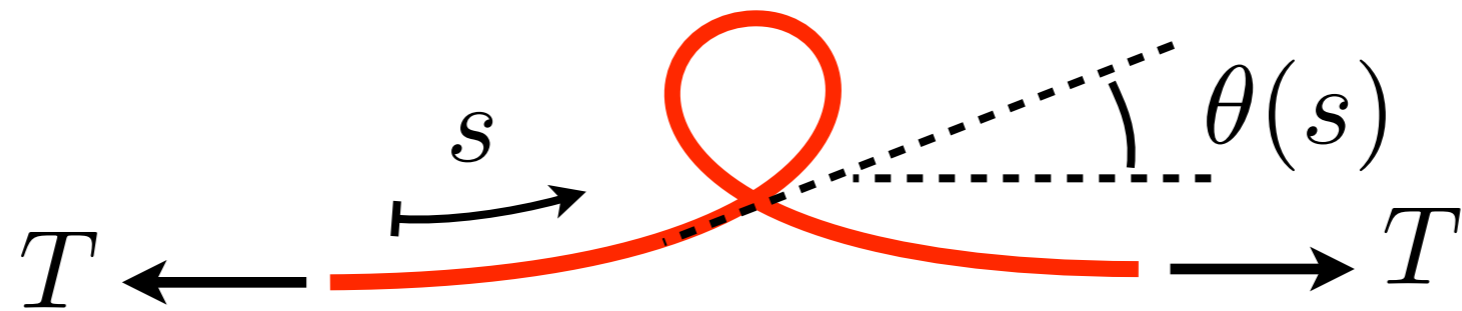


system reduction

$$21 \text{ D} \Rightarrow 6 \text{ D}$$

$$r' = d_3$$
$$d'_3 = (F \times r + M_0) \times d_3$$

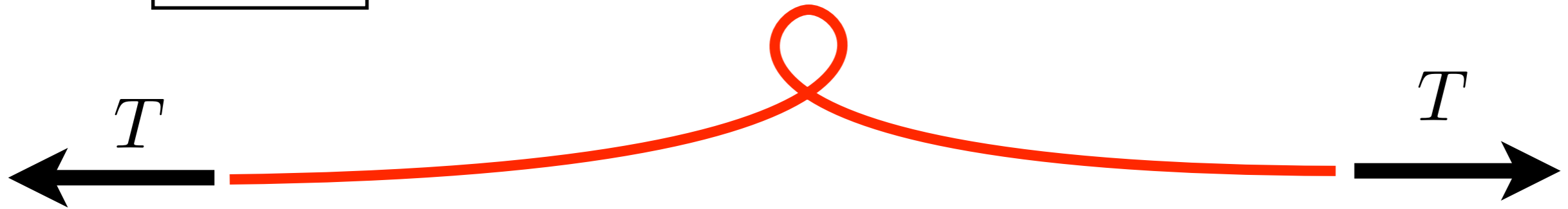
# Planar Elastica



$$EI\theta'' = T \sin \theta$$

# Planar Elastica

large  $T$

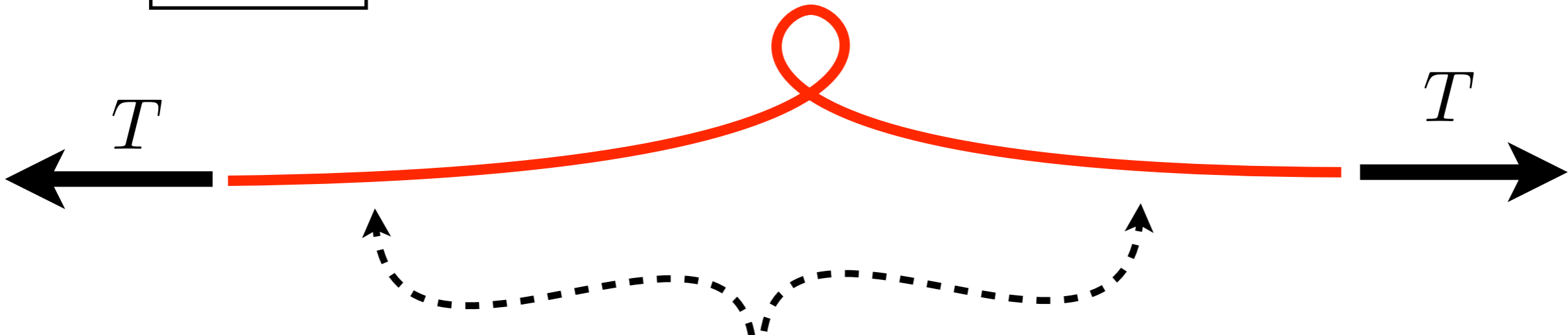


$$\frac{EI}{T} \theta'' = \sin \theta$$

singular  
perturbation

# Planar Elastica

large  $T$

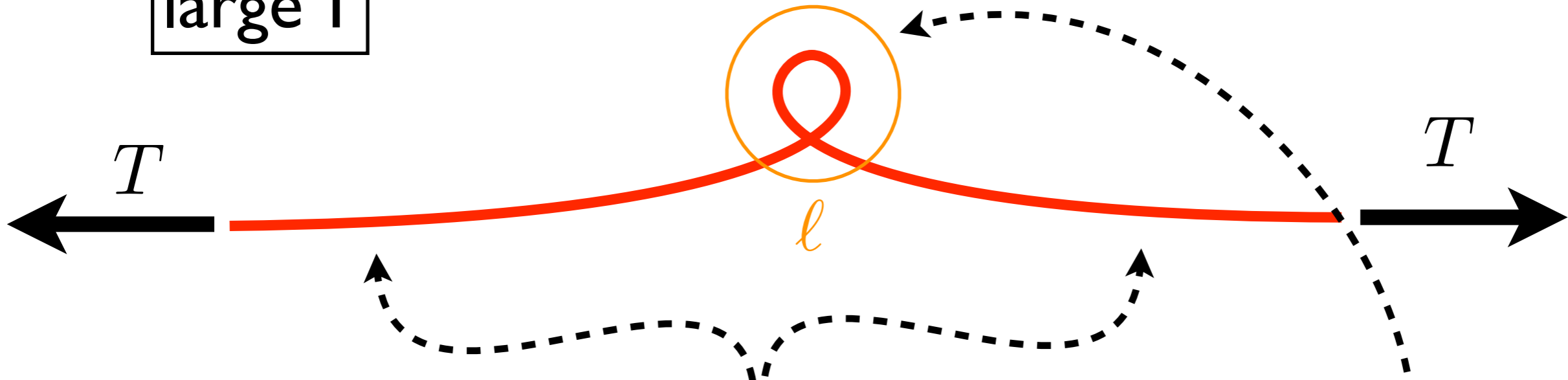


$$\frac{EI}{T} \theta'' = \sin \theta \quad \left\{ \begin{array}{l} \sin \theta \approx 0 \Rightarrow \theta(s) \approx 0 \end{array} \right.$$

singular  
perturbation

# Planar Elastica

large  $T$



$$\frac{EI}{T} \theta'' = \sin \theta \quad \left\{ \begin{array}{l} \sin \theta \approx 0 \Rightarrow \theta(s) \approx 0 \\ \theta(s) \text{ rapidly varying} \end{array} \right.$$

region size :  $l \sim \sqrt{\frac{EI}{T}}$

singular perturbation

inner layer

# Kirchhoff Equations

$$\left\{ \begin{array}{ll} \vec{F}' = -\vec{p} & \text{forces equil.} \\ \vec{M}' = \vec{F} \times \vec{t} & \text{moments equil.} \\ \vec{t}' = \frac{1}{EI} \vec{M} \times \vec{t} & \text{kinematics} \\ \vec{R}' = \vec{t} & \text{tangent def.} \end{array} \right.$$

$$' \equiv \frac{d}{ds}$$

constitutive relations:

$$M_{\kappa} = EI \kappa \quad \text{curvature} \quad \kappa$$

$$M_{\tau} = GJ \tau \quad \text{twist} \quad \tau$$

$\vec{p}(s)$  ext. pressure

$\vec{M}(s)$  internal moment

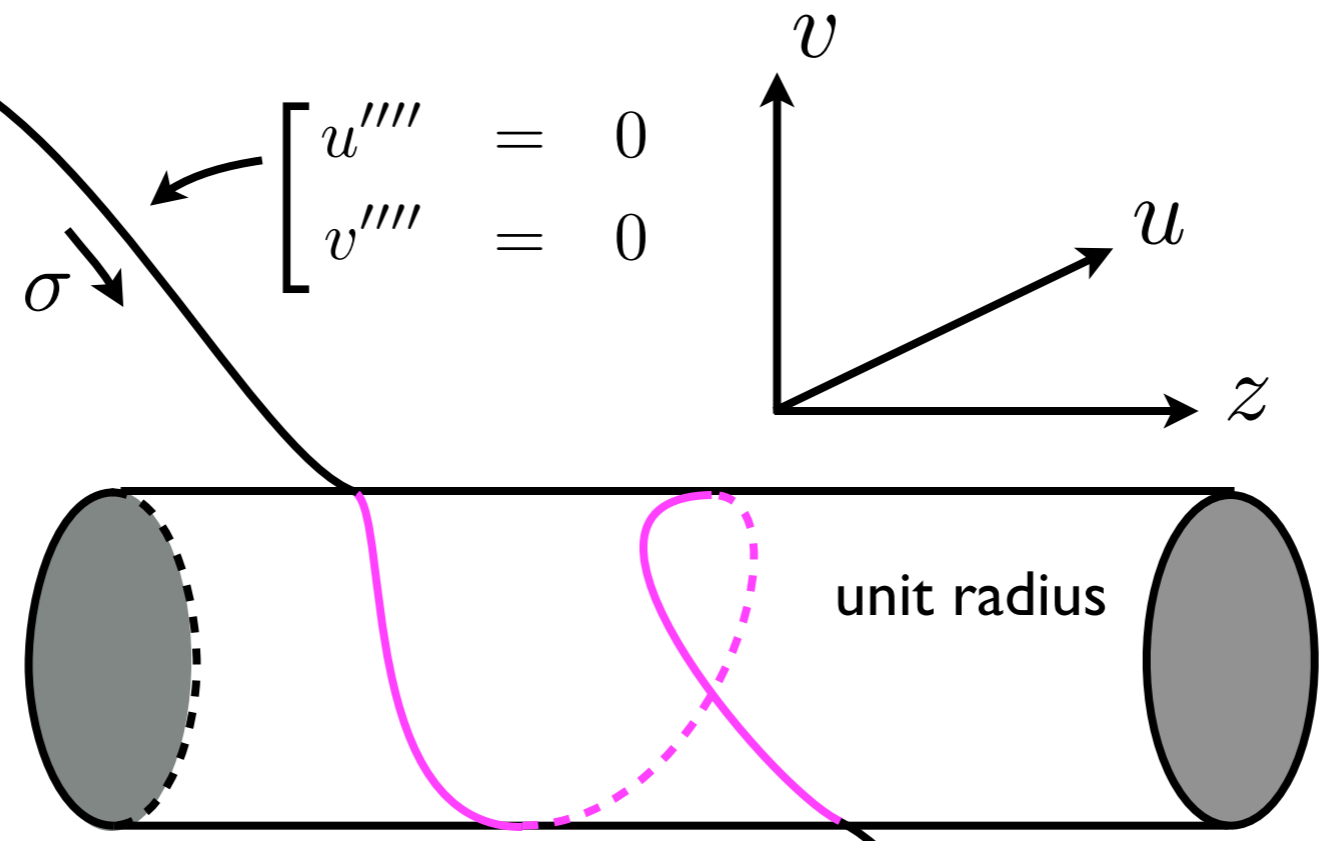
$\vec{F}(s)$  internal force

$\vec{R}(s)$  position

$\vec{t}(s)$  tangent

# Braid : boundary value problem (BVP)

$u''(-\infty)$	$=$	$0$
$v''(-\infty)$	$=$	$+1$
$u'''(-\infty)$	$=$	$0$
$v'''(-\infty)$	$=$	$0$
boundary conditions		



$$u = \frac{x^B - x^A}{\sqrt{2}}$$

$$v = \frac{y^B - y^A}{\sqrt{2}}$$

$$u^2(\sigma) + v^2(\sigma) = 1$$

$$\begin{cases} u'''' = \sqrt{2} p(\sigma) u(\sigma) \\ v'''' = \sqrt{2} p(\sigma) v(\sigma) \end{cases}$$

$$p(\sigma) = ?$$

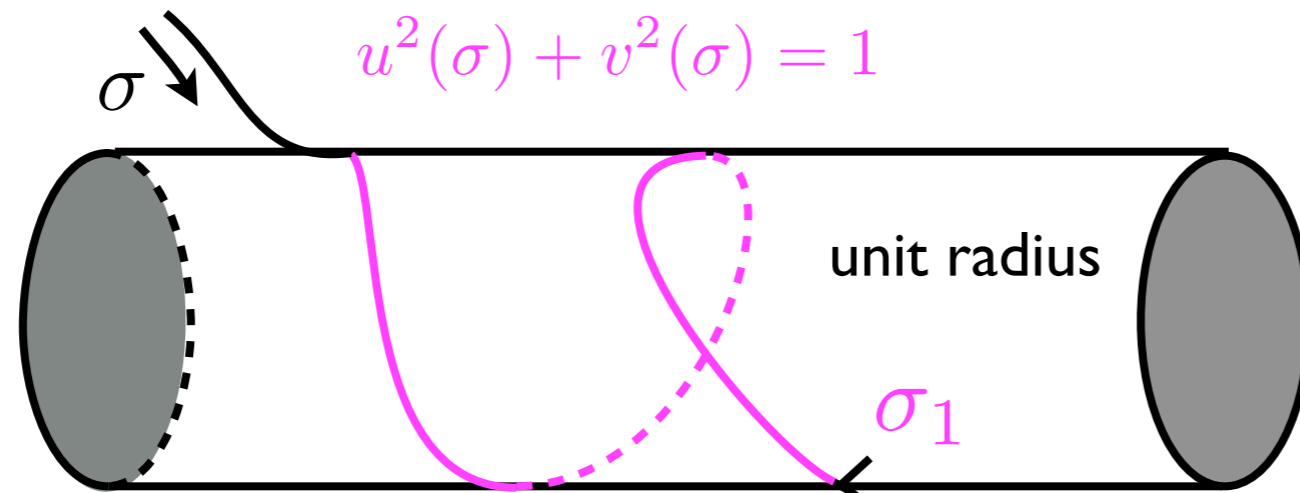
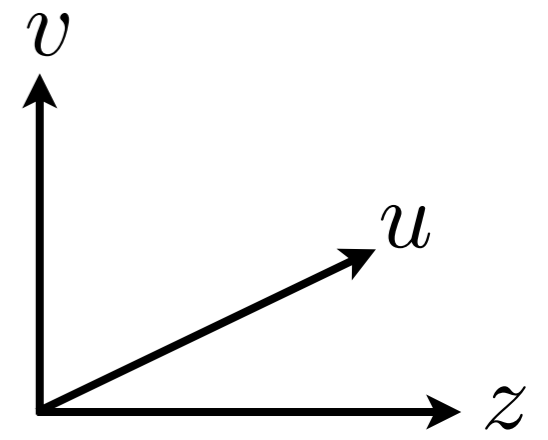
$$\begin{cases} u'''' = 0 \\ v'''' = 0 \end{cases}$$

**moments**

$u''(+\infty)$	$=$	$0$
$v''(+\infty)$	$=$	$-1$
$u'''(+\infty)$	$=$	$0$
$v'''(+\infty)$	$=$	$0$
<b>forces</b>		
boundary conditions		



# Braid : first kind of solutions



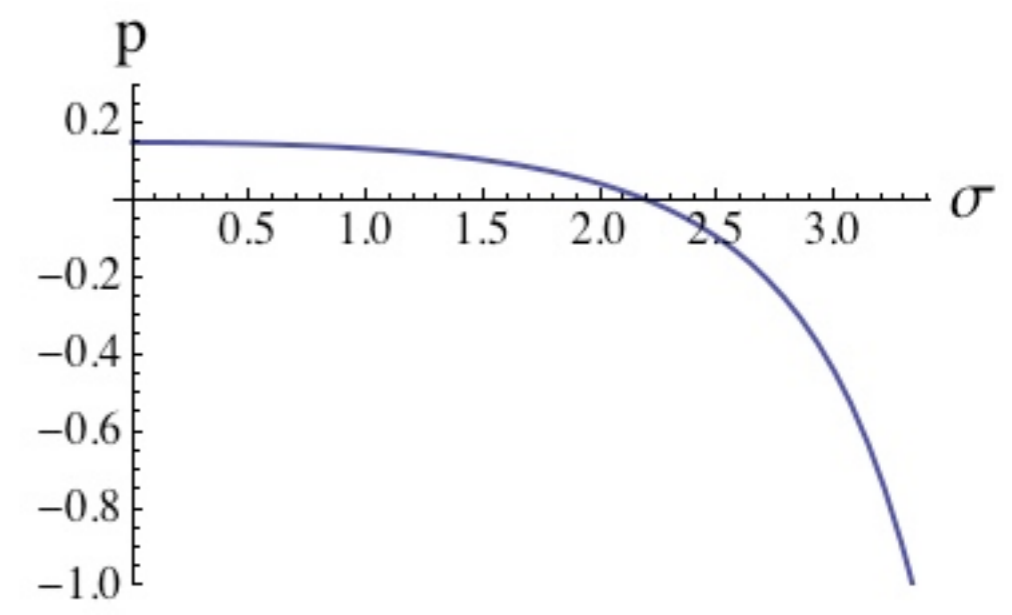
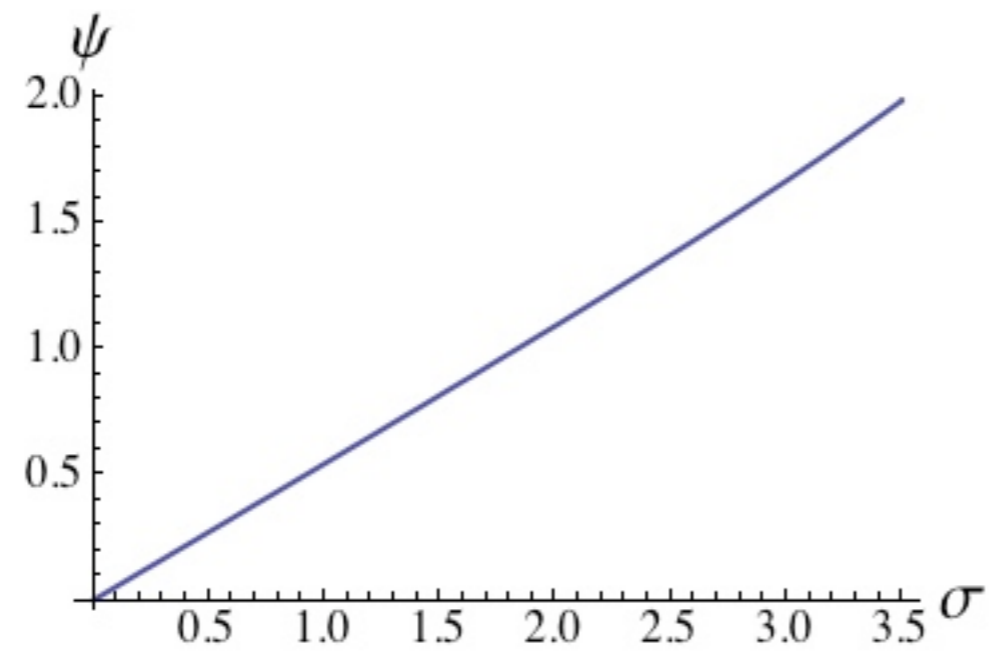
boundary conditions

$$\begin{aligned} u''(\sigma_1) &= 0 \\ v''(\sigma_1) &= -1 \\ u'''(\sigma_1) &= 0 \\ v'''(\sigma_1) &= 0 \end{aligned}$$

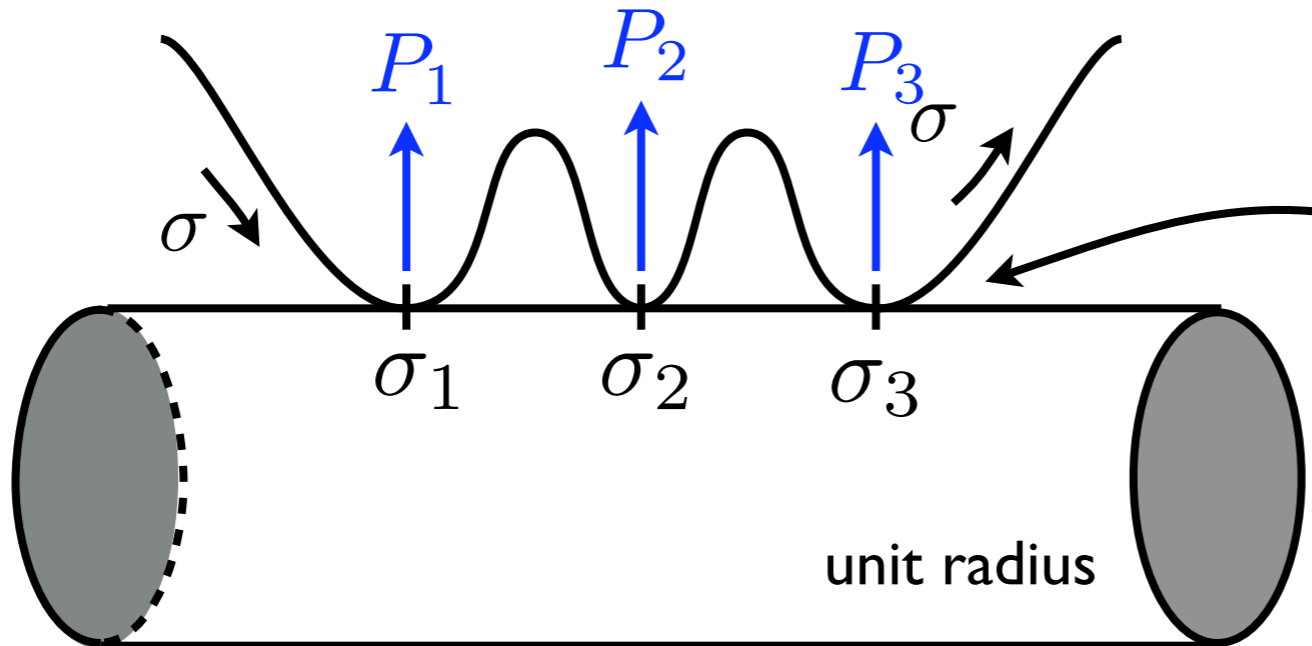
$$\begin{cases} u'''' = \sqrt{2} p(\sigma) u(\sigma) \\ v'''' = \sqrt{2} p(\sigma) v(\sigma) \end{cases} \quad \begin{cases} u = \cos(\psi(\sigma)) \\ v = \sin(\psi(\sigma)) \end{cases}$$

$$\begin{cases} \psi'''' = 6 \psi'' \psi'^2 \\ p(\sigma) = (\psi'^4 - 3\psi''^2 - 4\psi' \psi''') / \sqrt{2} \end{cases}$$

$$\begin{aligned} \psi(0) &= 0 \\ \psi'(0) &= 0.54 \\ \psi''(0) &= 0 \\ \psi'''(0) &= 0.004 \\ \sigma_1 &= 3.50 \end{aligned}$$



# Braid : second kind of solutions



boundary conditions

$$u''(+\sigma_3) = 0$$

$$v''(+\sigma_3) = -1$$

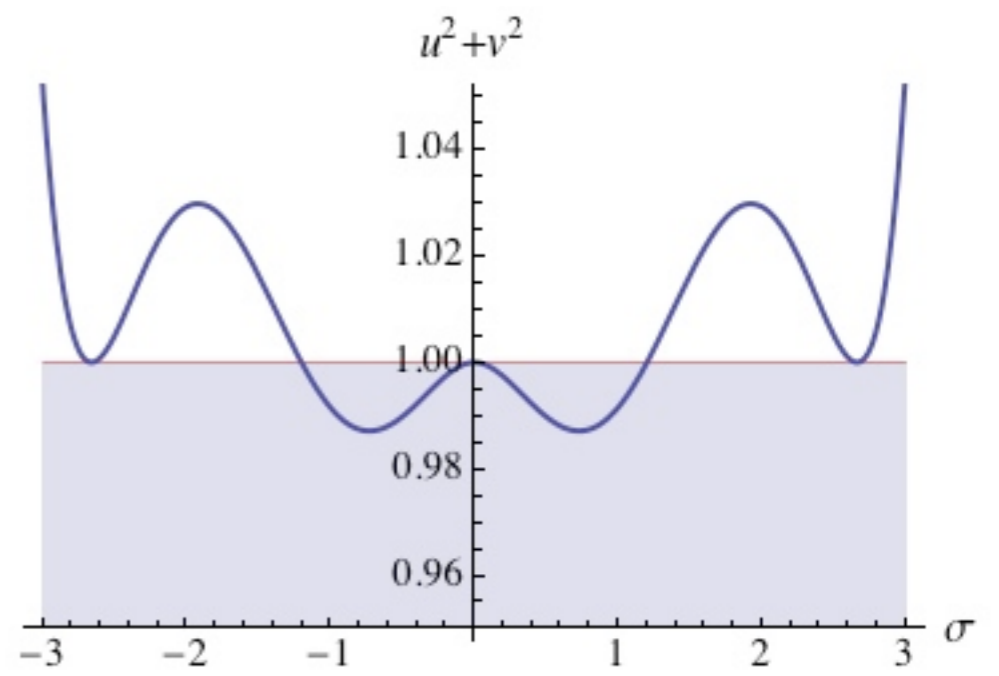
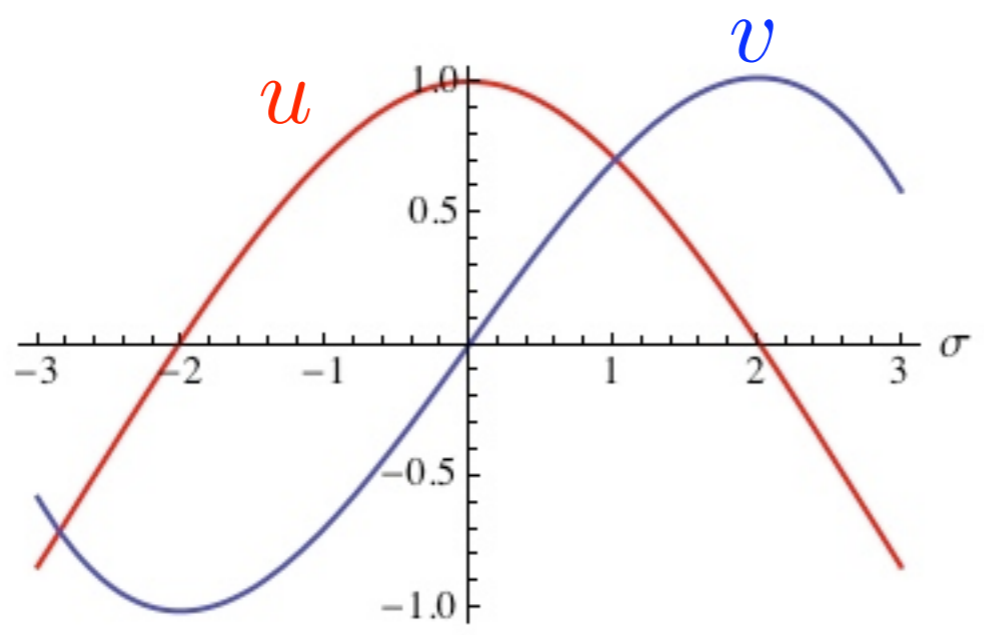
$$u'''(+\sigma_3) = 0$$

$$v'''(+\sigma_3) = 0$$

$$\begin{cases} u'''' = \sqrt{2} p(\sigma) u(\sigma) \\ v'''' = \sqrt{2} p(\sigma) v(\sigma) \end{cases} \quad \text{avec} \quad p(\sigma) = P_1 \delta(\sigma - \sigma_1) + P_2 \delta(\sigma - \sigma_2) + P_3 \delta(\sigma - \sigma_3)$$

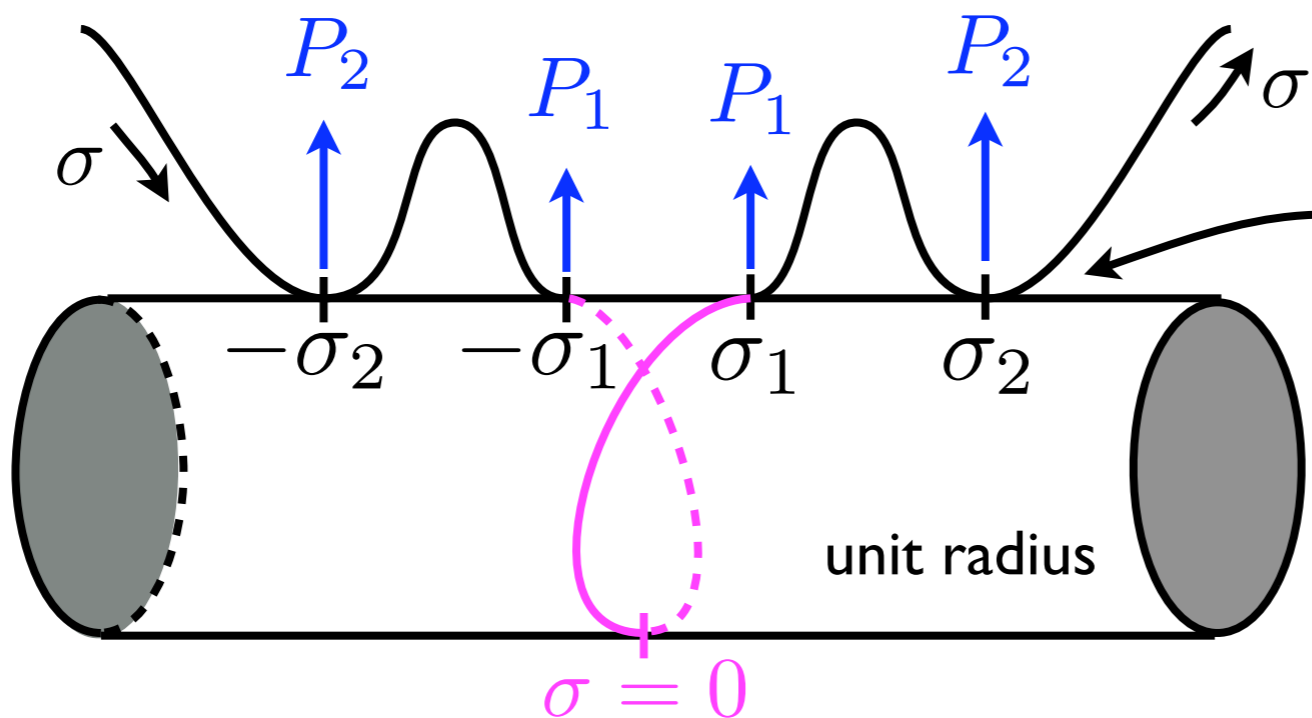
$$\begin{aligned} u(0) &= 1 \\ u'(0) &= 0 \\ u''(0) &= -0.66 \\ u'''(0) &= 0.25 \end{aligned}$$

$$\begin{aligned} v(0) &= 0 \\ v'(0) &= 0.76 \\ v''(0) &= 0 \\ v'''(0) &= -0.38 \end{aligned}$$



$$\sigma_3 = -\sigma_1 = 2.66 ; \sigma_2 = 0 ; P_1 = P_3 = 0.32 ; P_2 = 0.35$$

# Braid : third kind of solutions



boundary conditions

$$u''(+\sigma_2) = 0$$

$$v''(+\sigma_2) = -1$$

$$u'''(+\sigma_2) = 0$$

$$v'''(+\sigma_2) = 0$$

- $\sigma_1 = 0.35$
- $\sigma_2 = 2.68$
- $P_1 = 0.12$
- $P_2 = 0.31$

